



California Independent  
System Operator Corporation

July 30, 2007

**Via Federal Express**

Attn: Commission's Docket Office  
California Public Utilities Commission  
505 Van Ness Avenue  
San Francisco, CA 94102

RE: Docket No. R.07-01-041 - Order Instituting Rulemaking Regarding Policies and Protocols for Demand Response, Load Impact Estimates, Cost-Effectiveness Methodologies, Megawatt Goals and Alignment with California Independent System Operator Protocols

With this transmittal letter, the California Independent System Operator Corporation (CAISO) submits, by paper filing, its original and six copies of the Comments of the California System Operator Re: Loan Impact and Cost Effectiveness Straw Proposals. As indicated by our Proof of Service, the CAISO served the service list for the proceeding on July 27, 2007.

The filing date for comments was July 27, 2008. The CAISO has requested and received permission from the Assigned Administrative Law Judge, Jessica Hecht, to file its Comments by close of business Tuesday, July 31, 2007.

I discussed this filing with Mr. Darin Pratt of your office yesterday, July 30<sup>th</sup>. Mr. Pratt confirmed that the CAISO would be permitted to submit the filing by expedited courier delivery.

The CAISO apologizes for its delay in submitting the materials. We experienced some computer-technical problems when attempting to merge the Exhibit A document into one electronic document for electronic filing (the final document was not of PDF/A-Draft quality). As the 5:00 hour neared, we then submitted an electronic filing of the Comments document only (we inadvertently forgot to include the service list). This document posted after 5:00 and received a July 30, 2007 filing date, along with the confirmation number 7026.

For reference, I am also including two email print-outs representing (i) the CPUC Docket Office's Notice of Rejection of the Electronic filing; and (ii) ALJ Hecht's communication to the CAISO of her grant of extension to file the Comments.

Very truly yours,

Baldassaro "Bill" Di Capo  
Counsel - Regulatory

CAISO  
151 Blue Ravine Road  
Folsom, California 95630  
(916) 351-4400

## Di Capo, Baldassaro

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**From:** CPUC Electronic Filing System [CPUCElectronicFiling@cpuc.ca.gov]  
**Sent:** Monday, July 30, 2007 11:53 AM  
**To:** Di Capo, Baldassaro  
**Subject:** 0000007026 - California Public Utilities Commission Rejection of Filing

Your filing, submitted on 7/27/2007 with confirmation number 0000007026, has been rejected by the California Public Utilities Commission for the following reasons:

E-File #7026 / R.07-01-041 / Comments of the California Independent System Operator re: Load Impact and Cost Effectiveness Straw Proposals on the Service List for Proceeding R.07-01-041.

1. Document is submitted late. These comments were due July 27, 2007. Prior to re-submitting, please get permission from the involved ALJ to late file.
2. Service list is not attached. (Rule 1.9(d))

Thank You,

Darin Pratt  
Legal Analyst  
(415) 703-3852

If you have questions about this rejection, please contact the CPUC Docket Office at the address listed below.

Docket Office  
California Public Utilities Commission  
505 Van Ness Avenue, Room 2001  
San Francisco, CA 94102  
Voice: (415) 703-2121  
Fax: (415) 703-2446  
Email: dkt@cpuc.ca.gov

**Di Capo, Baldassaro**

**From:** Hecht, Jessica T. [JHE@cpuc.ca.gov]  
**Sent:** Monday, July 30, 2007 2:16 PM  
**To:** Di Capo, Baldassaro  
**Cc:** mpieniazek@ecsny.com; sdebroff@sasllp.com; keith.mccrea@sabl原因.com; klatt@energyattorney.com; douglass@energyattorney.com; janet.combs@sce.com; vthompson@sempra.com; liddell@energyattorney.com; jellis@energyconnectinc.com; marcel@turn.org; Salvacion, Lisa-Marie; nes@a-klaw.com; cbaskette@enernoc.com; rcounihan@enernoc.com; saw0@pge.com; l\_brown369@yahoo.com; Sherif, Linda; wbooth@booth-law.com; eric@strategyi.com; ewoychik@strategyi.com; ja\_boothe@yahoo.com; Mills, Karen; clark.pierce@us.landisgyr.com; gesmith@ecsny.com; stephen.baker@constellation.com; Carlson, Trent; Violette, Daniel; kcooney@summitblue.com; barrettlarry@comcast.net; david@nemtzow.com; Pelote, Roger; david.reed@sce.com; joyce.leung@sce.com; marian.brown@sce.com; mark.s.martinez@sce.com; andrea.horwatt@sce.com; carl.silsbee@sce.com; case.admin@sce.com; ka-wing.poon@sce.com; larry.cope@sce.com; garwacrd@sce.com; jyamagata@semprautilities.com; dwood8@cox.net; cfpena@sempra.com; jlaun@apogee.net; dbarker@semprautilities.com; ksmith2@semprautilities.com; lwilloughby@semprautilities.com; CentralFiles@semprautilities.com; gayres@energycoalition.org; imungi@energycoalition.org; wmittchellrunner@socal.rr.com; dwylie@aswengineering.com; hvidstenj@kindermorgan.com; King, Chris; sharon@emeter.com; Engel, Dan; filings@a-klaw.com; snuller@ethree.com; stephengeorge@fccgroup.com; Haubenstock, Arthur; abonds@thelen.com; Middlekauff, Charles; evk1@pge.com; Abreu, Ken; latd@pge.com; pxo2@pge.com; ahmad.faruqui@brattle.com; jeffgray@dwt.com; cpuccases@pge.com; ssmyers@att.net; jwwd@pge.com; LATc@pge.com; sem4@pge.com; rwalther@pacbell.net; Service@spurr.org; cpjoe@gepllc.com; pthompson@summitblue.com; philha@astound.net; ted@energy-solution.com; jody\_london\_consulting@earthlink.net; mrw@mrwassoc.com; rschmidt@bartlewells.com; adamb@greenlining.org; elvine@lbl.gov; GLBarbose@lbl.gov; janreid@coastecon.com; jshields@ssjid.com; joyw@mid.org; VanHoy, Roger; tomk@mid.org; Barkovich, Barbara; clark.bernier@rlw.com; stacia.okura@rlw.com; gayatri@jbsenergy.com; jeff@jbsenergy.com; jweil@aglet.org; rmccann@umich.edu; demorse@omsoft.com; e-recipient; Goodin, John; Brown, Andy; dhungerf@energy.state.ca.us; msherida@energy.state.ca.us; bernardo@braunlegal.com; vwood@smud.org; bboice02@yahoo.com; Lindh, Karen; sas@a-klaw.com; mike.messenger@powerauthority.on.ca; Campbell, Andrew; Kaneshiro, Bruce; Villarreal, Christopher; Lam, Dorris; Salmi Klotz, Jason R.; Como, Joe; Morgenstern, Joy; Lee, Rebecca Tsai-Wei; Gokhale, Sudheer; Drew, Tim G.; claufenb@energy.state.ca.us; aulmer@water.ca.gov

**Subject:** RE: CPUC R07-01-041; CAISO Request for Leave to Late File CAISO Comments Re LI and CE Straw Proposals

Mr. Di Capo,

I am granting your request to file CAISO's comments on the load impact and cost effectiveness straw proposals not later than close of business tomorrow. Since you were able to serve your comments (including the Attachment A) on the service list last Friday (the filing deadline), and did attempt to file the document Friday as directed, I do not believe that anyone is disadvantaged by your request to file this document late. I will inform the Commission's docket office that I am granting this request.

Please make sure that the document is properly filed by close of business tomorrow, Tuesday, July 31, 2007.

Please let me know if you have any questions.

Jessica T. Hecht  
 Administrative Law Judge  
 California Public Utilities Commission  
 (415) 703-2027  
 jhe@cpuc.ca.gov

7/30/2007

**From:** Di Capo, Baldassaro [mailto:BDiCapo@caiso.com]

**Sent:** Monday, July 30, 2007 12:19 PM

**To:** Hecht, Jessica T.

**Cc:** mpieniazek@ecsny.com; sdebroff@sasllp.com; keith.mccrea@sablaw.com; klatt@energyattorney.com; douglass@energyattorney.com; janet.combs@sce.com; vthompson@sempra.com; liddell@energyattorney.com; jellis@energyconnectinc.com; marcel@turn.org; Salvacion, Lisa-Marie; nes@a-klaw.com; cbasket@enernoc.com; rcounihan@enernoc.com; saw0@pge.com; l\_brown369@yahoo.com; Sherif, Linda; wbooth@booth-law.com; eric@strategyi.com; ewoychik@strategyi.com; ja\_boothe@yahoo.com; Di Capo, Baldassaro; Mills, Karen; clark.pierce@us.landisgyr.com; gesmith@ecsny.com; stephen.baker@constellation.com; Carlson, Trent; Violette, Daniel; kcooney@summitblue.com; barrettlarry@comcast.net; david@nemtzwow.com; Pelote, Roger; david.reed@sce.com; joyce.leung@sce.com; marian.brown@sce.com; mark.s.martinez@sce.com; andrea.horwatt@sce.com; carl.silsbee@sce.com; case.admin@sce.com; ka-wing.poon@sce.com; larry.cope@sce.com; garwacrd@sce.com; jyamagata@semprautilities.com; dwood8@cox.net; cfpenna@sempra.com; jlaun@apogee.net; dbarker@semprautilities.com; ksmith2@semprautilities.com; lwilloughby@semprautilities.com; CentralFiles@semprautilities.com; gayres@energycoalition.org; imungi@energycoalition.org; wmittchellrunner@socal.rr.com; dwylie@aswengineering.com; hvidstenj@kindermorgan.com; King, Chris; sharon@emeter.com; Engel, Dan; filings@a-klaw.com; snuller@ethree.com; stephengeorge@fccgroup.com; Haubenstock, Arthur; abonds@thelen.com; Middlekauff, Charles; evk1@pge.com; Abreu, Ken; latd@pge.com; pxo2@pge.com; ahmad.faruqui@brattle.com; jeffgray@dwt.com; cpuccases@pge.com; ssmyers@att.net; jwwd@pge.com; LATc@pge.com; sem4@pge.com; rwalther@pacbell.net; Service@spurr.org; cpjoe@gepllc.com; pthompson@summitblue.com; philha@astound.net; ted@energy-solution.com; jody\_london\_consulting@earthlink.net; mrw@mrwassoc.com; rschmidt@bartlewells.com; adamb@greenlining.org; elvine@lbl.gov; GLBarbose@lbl.gov; janreid@coastecon.com; jshields@ssjid.com; joyw@mid.org; VanHoy, Roger; tomk@mid.org; Barkovich, Barbara; clark.bernier@rlw.com; stacia.okura@rlw.com; gayatri@jbsenergy.com; jeff@jbsenergy.com; jweil@aglet.org; rmccann@umich.edu; demorse@omsoft.com; e-recipient; Di Capo, Baldassaro; Goodin, John; Brown, Andy; dhungerf@energy.state.ca.us; msherida@energy.state.ca.us; bernardo@braunlegal.com; vwood@smud.org; bboice02@yahoo.com; Lindh, Karen; sas@a-klaw.com; mike.messenger@powerauthority.on.ca; Campbell, Andrew; Kaneshiro, Bruce; Villarreal, Christopher; Lam, Dorris; Salmi Klotz, Jason R.; Hecht, Jessica T.; Como, Joe; Morgenstern, Joy; Lee, Rebecca Tsai-Wei; Gokhale, Sudheer K.; Drew, Tim G.; claufenb@energy.state.ca.us; aulmer@water.ca.gov

**Subject:** CPUC R07-01-041; CAISO Request for Leave to Late File CAISO Comments Re LI and CE Straw Proposals

Dear Judge Hecht:

By this email, the California ISO respectfully requests leave for late filing of its "Comments of the California Independent System Operator Re: Load Impact and Cost Effectiveness Straw Proposals," which were due July 27, 2007.

In this regard, the Cal ISO filing was delayed because we experienced problems in our attempt to create our Exhibit A document as a PDF document meeting the Docket Department's filing requirement that the document be a "PDF/A-Draft." Apparently, the electronic copy of the Exhibit A document that we had was not of sufficient electronic quality to meet this level, and we were ultimately unsuccessful in creating an Exhibit A of sufficient quality to file this exhibit electronically.

We were successful in serving Cal ISO's comments (with the Exhibit A) on all parties in the proceeding on Friday July 27<sup>th</sup>. Our intention is to hand file the Comments filing at the CPUC dockets office in its entirety no later than COB by Tuesday. In this regard, the Exhibit is over 150 pages in length and will take some time to copy, and we will need to have the document delivered to San Francisco for filing.

7/30/2007

**Baldassaro "Bill" Di Capo**

Counsel

California Independent System Operator Corp.

phone (916) 608-7157

email [bdicapo@caiso.com](mailto:bdicapo@caiso.com)

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California ISO  
Your Link to Power

California Independent  
System Operator Corporation

July 27, 2007

Attn: Commission's Docket Office  
California Public Utilities Commission  
505 Van Ness Avenue  
San Francisco, CA 94102

RE: Docket No. R.07-01-041 - Order Instituting Rulemaking Regarding Policies and Protocols for Demand Response, Load Impact Estimates, Cost-Effectiveness Methodologies, Megawatt Goals and Alignment with California Independent System Operator Protocols

Dear Clerk:

Enclosed for filing please find an original and five copies of the Comments Of The California Independent System Operator Re: Load Impact And Cost Effectiveness Straw Proposals in the above-referenced docket.

Please date stamp one copy and return to California ISO in the self-addressed stamped envelope provided.

Thank you.

Sincerely,

A handwritten signature in black ink that reads "Bill Di Capo".

Baldassaro "Bill" Di Capo  
Counsel - Regulatory

CAISO  
151 Blue Ravine Road  
Folsom, California 95630  
(916) 351-4400

**BEFORE THE PUBLIC UTILITIES COMMISSION OF  
THE STATE OF CALIFORNIA**

Order Instituting Rulemaking Regarding Policies  
and Protocols for Demand Response, Load Impact  
Estimates, Cost-Effectiveness Methodologies,  
Megawatt Goals and Alignment with California  
Independent System Operator Protocols

Rulemaking 07-01-041  
(January 25, 2007)

**COMMENTS OF  
THE CALIFORNIA INDEPENDENT SYSTEM OPERATOR  
RE: LOAD IMPACT AND COST EFFECTIVENESS STRAW PROPOSALS**

July 27, 2007

Nancy Saracino, General Counsel  
Baldassaro "Bill" Di Capo, Counsel  
California Independent System Operator  
151 Blue Ravine Road  
Folsom California 95630  
Telephone: (916) 351-4400  
Facsimile: (916) 608-7296

**BEFORE THE PUBLIC UTILITIES COMMISSION OF THE  
STATE OF CALIFORNIA**

Order Instituting Rulemaking Regarding Policies and Protocols for Demand Response, Load Impact Estimates, Cost-Effectiveness Methodologies, Megawatt Goals and Alignment with California Independent System Operator Protocols

Rulemaking 07-01-041  
(January 25, 2007)

**COMMENTS OF  
THE CALIFORNIA INDEPENDENT SYSTEM OPERATOR  
RE: LOAD IMPACT AND COST EFFECTIVENESS STRAW PROPOSALS**

The California Independent System Operator Corporation (“CAISO”) submits its comments regarding the Load Impact and Cost Effectiveness Straw Proposals submitted in this proceeding on July 16, 2007.

**Introduction**

The CAISO commends the efforts of the utilities and other parties for their efforts in preparing the Straw Proposals. Further, the CAISO appreciates the Commission’s support, in this proceeding, to better incorporate demand response programs into the CAISO’s wholesale market design.

The Federal Energy Regulatory Commission (“FERC”) is similarly interested in these topics, including the development of reasonable standards to measure compliance when demand resources are dispatched and whether ISOs should quantify the cost-effectiveness of demand response in their wholesale power markets. In addition, FERC is interested in the greater coordination between state and federal entities, in order to promote and integrate demand response into retail and wholesale markets and planning

and “to remove unnecessary obstacles to demand response participating in the wholesale power markets of RTOs and ISOs.”<sup>1</sup>

Responsive to these issues, on May 15, 2007, the CAISO, in collaboration with the CPUC, CEC, IOUs, convened a meeting with the objective of developing an informal process intended to advance the integration of demand resources into MRTU wholesale market design. In this regard, five key demand resource working groups have been formed to meet this objective. These five working groups are as follows:

1. Demand Response Participation in MRTU Release 1;
  - Lead agency- CAISO
2. Demand Response Participation in MRTU Post Release 1;
  - Lead agency- CAISO
3. Demand Resource Product Specification;
  - Lead agency- CEC
4. Infrastructure for Demand Resources;
  - Lead agency- CEC
5. Vision for Demand Resources;
  - Lead agency- CPUC<sup>2</sup>.

### **How Demand Resources Contribute to Grid Reliability**

Demand resources generally fall into one of three categories, in the context of their contributing to the reliability of the grid. Demand resources can:

1. Reduce the demand forecast;
2. Provide reliability services to the grid; and
3. Provide emergency response.

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<sup>1</sup> FERC Advanced Notice of Proposed Rulemaking, dated June 22, 2007 (issued in Docket Nos. RM07-19 and AD07-7), 119 FERC ¶61,603 (Accession No. 20070622-3049) at ¶41, p. 27 (hereafter, “ANOPR”). The ANOPR may be found through the FERC Internet Web Search Page at

[http://elibrary.ferc.gov/idmws/docket\\_search.asp](http://elibrary.ferc.gov/idmws/docket_search.asp), and entering “RM07-19” into the docket number field.

<sup>2</sup> Each working group has a lead sponsoring agency, as identified above. A summary of the objectives and deliverables for each working group can be found at: <http://www.caiso.com/1c0a/1c0a9dac6a660.pdf>

Demand resources can reduce the CAISO demand forecast in the day-ahead and day-of timeframe. In the day ahead, the CAISO can consider the contribution from demand resources in CAISO's determination of whether additional resources or capacity, not already bid into or scheduled in the Integrated Forward Market ("IFM"), needs to be committed. CAISO performs this determination through the CAISO's residual unit commitment ("RUC") process. Likewise, in the day-of timeframe, the contribution from demand resources could prevent the CAISO from having to start medium and/or quick start resources, based on system conditions and (the extent that demand response can contribute to a reduction in) the projected load forecast. Additionally, price-triggered demand resources can participate in the Integrated Forward Market ("IFM"), given a price-sensitive demand curve.

Demand resources can offer reliability services to the CAISO. Currently, reliability services offered by demand resources include imbalance energy and non-spinning reserve capacity for use by the CAISO in its real-time operations. In the future, demand resources could potentially be eligible to provide additional ancillary services, such as spinning reserve and regulation, to the CAISO. These services are generally considered higher quality in nature, given their inherent response times.

Finally, traditional interruptible/curtailable demand resources can provide emergency-load relief to the CAISO, either: i) after a system emergency is declared; or ii) for a local transmission emergency. Such emergency load relief aids in preventing the further degradation of the CAISO's operating reserves and/or to prevent firm load shedding, during the period of the emergency condition.

In each scenario, establishing, *ex ante*, and with a high degree of confidence, the load impacts of demand resources, is critical to the grid operator and its ability to maintain reliability. Since demand resources are most valuable to the CAISO as a supply side substitute (i.e. as a negative generator), foreknowledge of the load impact is equivalent to knowing the expected output of a generation resource. Thus, accurately

assessing the impact of, and mechanical reliability contribution from, demand resources is essential to the CAISO's ability to rely upon these resources to meet its operational needs.

### **Load Impact Protocols are Critical to Meeting the CAISO's Operational Needs**

Load impact protocols are important to the CAISO for understanding, for example, the basis on which the CAISO would be adjusting its demand forecast, to account for participation from demand resources in its RUC process. The accuracy of the load drop resulting from the call of demand resources is vital to the CAISO, as their incorporation into the forecast means that CAISO would use the demand resources in lieu of long-start resources, thus foregoing starting those long-start resources. If demand resources that were to be committed in the day-ahead timeframe and incorporated into the day ahead forecast, but were not to perform as CAISO reaches the day-of or real time, then CAISO would be resource short, at which point the long-start generation would be absolutely unavailable to make up the shortfall, because it would be physically impossible to timely start that generation to meet the need.

For these reasons, other ISOs, like the ISO New England, have developed their own set of measurement and verification ("M&V") protocols for application to demand resources participating in their organized markets. The CAISO briefly touched on the need to address baseline methodologies, and their importance, during a session of the demand response MRTU Release 1 Working Group, as it applies to integrating demand resources into the wholesale market and grid operations. The CAISO anticipates that suitable load impact protocols can be agreed to and ruled on in this proceeding that will serve both the CAISO's operational needs and the programmatic needs of demand resource providers. The CAISO understands that methodological refinements to the load impact protocols may be necessary over time. Therefore, we emphasize the need for

continual and close coordination between the CPUC, CEC, CAISO and demand resource providers on this issue.

### **Load Impacts Should Reflect Geographic Specificity**

The Joint IOU straw proposal correctly points out that “[r]esource planners may want to know DR impacts for different geographic regions that are dictated by the layout of generation, transmission and distribution resources.”<sup>3</sup> The CAISO’s RUC process assesses resource needs on a RUC zone basis, a subject that has been discussed in the Demand Response- MRTU Release 1 Working Group. In short, a RUC zone is a designated geographic area for which the CAISO has developed sufficient historical demand forecast and relevant weather data to perform a demand forecast for that zone. As such, demand resources must be identified by RUC zone, so that the CAISO can consider these resources in its RUC procurement process, through lowering the demand forecast, and therefore the RUC procurement target based on the level of participation from demand resources.

Moreover, for demand resources to qualify as local capacity for resource adequacy purposes, demand resources must likewise be identified and tied geographically to a local capacity area, which areas are identified in the CAISO’s Local Capacity Technical Analysis.<sup>4</sup>

### **The LI and CE Protocols Developed in this Proceeding Should Strive for Standardization and Glean From Work Already Performed**

The work product developed in this proceeding may have far-reaching implications, given the heightened interest in load impact and cost-effectiveness standards, both locally and nationally. Standardization of measurement and verification

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<sup>3</sup> IOU Joint Proposal, Section 3.2 [*Understanding What is Needed*], p.16.

<sup>4</sup> For details on local capacity areas, see the 2008 Local Capacity Technical Analysis Report and Study Results at: <http://www.caiso.com/1bb5/1bb5ed3d46430.pdf>.

(“M&V”) protocols and cost effectiveness screens, where appropriate, could be very helpful in meeting the objective of lowering barriers to entry for demand resources, particularly given the priority of demand resources in California’s loading order.<sup>5</sup>

Thus, the CAISO encourages the Commission, in its decision-making, to thoroughly consider the comprehensive and professional research being conducted by the Demand Response Research Center (“DRRC”) on these topics, along with important work already produced on these issues. One such significant work is the consultant report prepared by KEMA-Xenergy for the CEC in February 2003 on protocol development for demand response calculations (“KEMA-Xenergy Report”).<sup>6</sup> Much of this work could be instrumental in ultimately developing national standards. (A copy of the KEMA-Xenergy Report is attached to these Comments.)

Specifically, the five criteria for selecting a good baseline method that are identified and described in the KEMA-Xenergy Report are similar to those conveyed in the Joint Parties’ DR load impact protocols straw proposal<sup>7</sup> and, thus, are worthy of the Commissions’ attention. In general, the KEMA-Xenergy Report identified the following criteria:

1. Simplicity- ease of use, ease of understanding;
2. Accuracy- lack of bias, verifiable and flexible;
3. Minimization (or Integrity)- minimizes gaming opportunities;
4. Predictability- know baseline before committing to a response;
5. Consistency- similar results achieved when applied by different entities.<sup>8</sup>

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<sup>5</sup> The loading order is set forth in the Energy Action Plan II (EAP II), adopted by the CPUC and CEC on September 21, 2005. Legislative endorsement of the EAP II can be seen, for example, by reference to the EAP II in SB 1368, Section 1(h).

<sup>6</sup> *Consultant Report: Protocol Development for Demand Response Calculation- Findings and Recommendations*, prepared by KEMA-Xenergy, Miriam L. Goldberg and G. Kennedy Agnew, published by the California Energy Commission, February 2003 (CEC Document No. 400-02-017F) [hereafter, KEMA-Xenergy Report].

<sup>7</sup> See *Straw Proposals of Enernoc, Inc., Energy Connect, Comverge, Inc. Ancillary Services Coalition, and California Large Energy Consumers Association on Load Impact Protocols for Demand Response Resources*, July 16, 2007, p. 5.

<sup>8</sup> KEMA-Xenergy Report, CEC Report Summary forward to the report, at subsection entitled “Criteria for Selecting a Good Baseline Method.” [The CEC forward is not paginated.]

Before this process unfolds further, the CAISO encourages the Commission to adopt the same or similar criteria for use in guiding the evaluation and screening of various cost-effectiveness protocols and methodologies and should include these in its workshop report.

### **Load Impact Protocol Options Should be Explored**

The Commission should consider adopting an approach as outlined in the KEMA-Xenergy Report “that baseline calculation protocols should provide for alternatives based on customer load characteristics and operating practices.”<sup>9</sup> In other words, the Commission should clearly identify the best-fit load impact protocol by customer and/or building type, however, and with clear guidance and rules, provide the ability for the program administrator to approve alternative approaches on an exception basis and with justification.

### **Cost Effectiveness Protocols Should Consider Value Contribution for the Wholesale Power Market**

The Commission should consider and further explore and consider the value that demand resources can provide to the wholesale power market, a perspective broader than looking just at retail energy and capacity values. Certainly, these additional value streams are tied to resolving seams issues between retail programs and pricing and the wholesale market and planning. However, if addressed, other categories of value will contribute to the cost-effectiveness of demand resources. For instance, value from demand resources could be derived from, amongst other possibilities:

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<sup>9</sup> KEMA-Xenergy Report at Section X.5 [*Recommendations*], Subsection X5.1 [*Proposed Approaches by Accountant Type, Offering Options*] at p. X-11.

- Sales of reliability services to the CAISO, in the form of ancillary services and imbalance energy;
- Participation in the forward energy market;
- A reduction in transmission losses and congestion; and
- The deferral of investment in generation and transmission assets;

The Commission should consider in its workshop report a process to identify and monetize such values streams and how they might be incorporated, at some point, into its adopted cost-effectiveness protocols.

### **Conclusion**

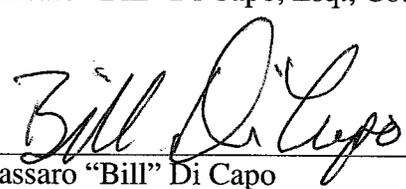
The CAISO looks forward to contributing to suitable outcomes that meet the respective needs of demand resource providers, regulators and the grid operator.

Dated: July 27, 2007

Respectfully submitted,

CALIFORNIA INDEPENDENT SYSTEM  
OPERATOR CORPORATION

Baldassaro "Bill" Di Capo, Esq., Counsel

By:   
Baldassaro "Bill" Di Capo

CALIFORNIA INDEPENDENT SYSTEM  
OPERATOR CORPORATION

151 Blue Ravine Road  
Folsom, CA 95630  
(916) 608-7157  
(916) 608-7222 (FAX)  
[bdicapo@caiso.com](mailto:bdicapo@caiso.com)

**CERTIFICATE OF SERVICE**

I hereby certify that i have served, by electronic and united states mail, a copy of the foregoing Comments Of The California Independent System Operator Re: Load Impact And Cost Effectiveness Straw Proposals to each party in docket no. A.07-01-041.

Executed On July 27, 2007 At Folsom, California.

A handwritten signature in black ink, appearing to read "Susan L. Montana", written over a horizontal line.

Susan L. Montana  
smontana@caiso.com

# Service List for Proceeding R. 07-01-041

ANDREW B. BROWN  
ELLISON, SCHNEIDER & HARRIS, LLP  
2015 H STREET  
SACRAMENTO, CA 95814abb@eslawfirm.com

AHMAD FARUQUI  
THE BATTLE GROUP  
353 SACRAMENTO STREET, SUITE 1140  
SAN FRANCISCO, CA  
94111ahmad.faruqui@battlle.com

LARRY B. BARRETT  
CONSULTING ASSOCIATES, INC.  
PO BOX 60429  
COLORADO SPRINGS, CO  
80960barrettlarry@comcast.net

RYAN BERNARDO  
BRAUN & BLAISING, P.C.  
915 L STREET, SUITE 1270  
SACRAMENTO, CA 95814bernardo@braunlegal.com

CASE ADMINISTRATION  
SOUTHERN CALIFORNIA EDISON COMPANY  
2244 WALNUT GROVE AVENUE  
ROSEMEAD, CA 91770case.admin@sce.com

CHRIS KING  
EMETER CORPORATION  
ONE TWIN DOLPHIN DRIVE  
REDWOOD CITY, CA 94065chris@emeter.com

JOE PRIJYANONDA  
GLOBAL ENERGY PARTNERS, LLC  
3569 MT. DIABLE BLVD., SUITE 200  
LAFAYETTE, CA 94549cpjoe@gepllc.com

DAVID REED  
SOUTHERN CALIFORNIA EDISON  
6060 IRWINDALE AVE., STE. J  
IRWINDALE, CA 91702david.reed@sce.com

DAVID MORSE  
1411 W. COVELL BLVD., SUITE 106-292  
DAVIS, CA 95616-5934demorse@omsoft.com

DANIEL M. VIOLETTE  
SUMMIT BLUE CONSULTING  
1722 14TH STREET, SUITE 230  
BOULDER, CO 80302dviolette@summitblue.com

CALIFORNIA ISO  
151 BLUE RAVINE ROAD  
FOLSOM, CA 95630e-recipient@caiso.com

KAREN TERRANOVA  
ALCANTAR & KAHL, LLP  
120 MONTGOMERY STREET, STE 2200  
SAN FRANCISCO, CA 94104filings@aklaw.com

GALEN BARBOSE  
LAWRENCE BERKELEY NATIONAL LAB  
1 CYCLOTRON RD.  
BERKELEY, CA 94720GLBarbose@LBL.gov

JANET COMBS  
SOUTHERN CALIFORNIA EDISON COMPANY  
2244 WALNUT GROVE AVENUE  
ROSEMEAD, CA 91770janet.combs@sce.com

JACK ELLIS  
ENERGY CONNECT, INC.  
490 RAQUEL COURT  
LOS ALTOS, CA 94022jellis@energyconnectinc.com

JOHN LAUN  
APOGEE INTERACTIVE, INC.  
1220 ROSECRANS ST., SUITE 308  
SAN DIEGO, CA 92106jlaun@apogee.net

JOY A. WARREN  
MODESTO IRRIGATION DISTRICT  
1231 11TH STREET  
MODESTO, CA 95354joyw@mid.org

JOY C. YAMAGATA  
SAN DIEGO GAS & ELECTRIC/SOCALGAS  
8330 CENTURY PARK COURT  
SAN DIEGO, CA 91910yamagata@semprautilities.com

KEVIN COONEY  
SUMMIT BLUE CORPORATION  
1722 14TH STREET  
BOULDER, CO 80302kcooney@summitblue.com

KAREN N. MILLS  
CALIFORNIA FARM BUREAU FEDERATION  
2300 RIVER PLAZA DRIVE  
SACRAMENTO, CA 95833kmills@cfbf.com

ASHLEE M. BONDS  
THELEN REID BROWN RAYSMAN&STEINER LLP  
101 SECOND STREET  
SAN FRANCISCO, CA 94105abonds@thelen.com

ARTHUR HAUBENSTOCK  
PACIFIC GAS AND ELECTRIC COMPANY  
77 BEALE STREET, B30A  
SAN FRANCISCO, CA 94105ahj@pge.com

BARB BOICE  
4309 NORWOOD AVENUE, APT. 160  
SACRAMENTO, CA 95838bboice02@yahoo.com

BARBARA R. BARKOVICH  
BARKOVICH & YAP, INC.  
44810 ROSEWOOD TERRACE  
MENDOCINO, CA 95460brbarkovich@earthlink.net

CARMEN BASKETTE  
ENERNOC, INC.  
594 HOWARD STREET, SUITE 400  
SAN FRANCISCO, CA 94105cbaskette@enernoc.com

CLARK BERNIER  
RLW ANALYTICS  
1055 BROADWAY, SUITE G  
SONOMA, CA 95476clark.bernier@rlw.com

LAW DEPARTMENT FILE ROOM  
PACIFIC GAS AND ELECTRIC COMPANY  
PO BOX 7442  
SAN FRANCISCO, CA 94120-7442cpucases@pge.com

DAVID NEMTZOW  
1254 9TH STREET, NO. 6  
SANTA MONICA, CA 90401david@nemtzow.com

DAVID HUNGERFORD  
CALIFORNIA ENERGY COMMISSION  
1516 NINTH STREET, MS-22  
SACRAMENTO, CA 95814dhungerf@energy.state.ca.us

DON WOOD  
PACIFIC ENERGY POLICY CENTER  
4539 LEE AVENUE  
LA MESA, CA 91941dwood8@cox.net

ERIC C. WOYCHIK  
STRATEGY INTEGRATION LLC  
9901 CALODEN LANE  
OAKLAND, CA 94605eric@strategyi.com

RUSS GARWACRD  
SOUTHERN CALIFORNIA EDISON COMPANY  
2244 WALNUT GROVE  
ROSEMEAD, CA 91770garwacrd@sce.com

JOEL M. HVIDSTEN  
KINDER MORGAN ENERGY PARTNERS  
1100 TOWN & COUNTRY ROAD, SUITE 700  
ORANGE, CA 92868hvidsten@kindermorgan.com

L. JAN REID  
COAST ECONOMIC CONSULTING  
3185 GROSS ROAD  
SANTA CRUZ, CA 95062janreid@coastecon.com

JOHN GOODIN  
CALIFORNIA ISO  
151 BLUE RAVINE RD.  
FOLSOM, CA 95630jgoodin@caiso.com

Joe Como  
CALIF PUBLIC UTILITIES COMMISSION  
505 VAN NESS AVENUE  
SAN FRANCISCO, CA 94102-3214joc@cpuc.ca.gov

JEFF SHIELDS  
SOUTH SAN JOAQUIN IRRIGATION DISTRICT  
11011 E. HWY 120  
MANTECA, CA 95336jshields@ssjid.com

Joy Morgenstern  
CALIF PUBLIC UTILITIES COMMISSION  
505 VAN NESS AVENUE  
SAN FRANCISCO, CA 94102-3214jym@cpuc.ca.gov

KEN ABREN  
245 MARKET STREET  
SAN FRANCISCO, CA 94105kea3@pge.com

KATHRYN SMITH  
SAN DIEGO GAS AND ELECTRIC COMPANY  
8306 CENTURY PARK COURT  
SAN DIEGO, CA 92123ksmith2@semprautilities.com

ADAM BRIONES  
THE GREENLINING INSTITUTE  
1918 UNIVERSITY AVENUE, 2ND FLOOR  
BERKELEY, CA 94704adamb@greenfining.org

ANDREA HORWATT  
SOUTHERN CALIFORNIA EDISON COMPANY  
2244 WALNUT GROVE AVENUE  
ROSEMEAD, CA 91770andrea.horwatt@sce.com

BALDASSARO DI CAPO, ESQ.  
CALIFORNIA ISO  
151 BLUE RAVINE ROAD  
FOLSOM, CA 95630bdcap@caiso.com

Bruce Kaneshiro  
CALIF PUBLIC UTILITIES COMMISSION  
505 VAN NESS AVENUE  
SAN FRANCISCO, CA 94102-3214bsk@cpuc.ca.gov

CENTRAL FILES  
SAN DIEGO GAS & ELECTRIC CO.  
8330 CENTURY PARK COURT-CP31E  
SAN DIEGO, CA 92123-  
1530CentralFiles@semprautilities.com

CLARK E. PIERCE  
LANDIS & GYR  
246 WINDING WAY  
STRATFORD, NJ 8084clark.pierce@us.landisgyr.com

CHARLES MIDDLEKAUFF  
PACIFIC GAS AND ELECTRIC COMPANY  
77 BEALE STREET  
SAN FRANCISCO, CA 94105crmd@pge.com

DAVID BARKER  
SAN DIEGO GAS & ELECTRIC COMPANY  
8306 CENTURY PARK COURT  
SAN DIEGO, CA 92123dbarker@semprautilities.com

Dorris Lam  
CALIF PUBLIC UTILITIES COMMISSION  
505 VAN NESS AVENUE  
SAN FRANCISCO, CA 94102-3214dnl@cpuc.ca.gov

DAVID M. WYLIE, PE  
ASW ENGINEERING  
2512 CHAMBERS ROAD, SUITE 103  
TUSTIN, CA 92780dwylie@aswengineering.com

EDWARD V. KURZ  
PACIFIC GAS AND ELECTRIC COMPANY  
77 BEALE STREET  
SAN FRANCISCO, CA 94105evk1@pge.com

GAYATRI SCHILBERG  
JBS ENERGY  
311 D STREET, SUITE A  
WEST SACRAMENTO, CA  
95605gayatri@jbsenergy.com

MWIRIGI IMUNGI  
THE ENERGY COALITION  
15615 ALTON PARKWAY, SUITE 245  
IRVINE, CA 92618imungi@energycoalition.org

JEFF NAHIGIAN  
JBS ENERGY, INC.  
311 D STREET  
WEST SACRAMENTO, CA 95605jeff@jbsenergy.com

Jessica T. Hecht  
CALIF PUBLIC UTILITIES COMMISSION  
505 VAN NESS AVENUE  
SAN FRANCISCO, CA 94102-3214jhe@cpuc.ca.gov

JODY S. LONDON  
JODY LONDON CONSULTING  
PO BOX 3629  
OAKLAND, CA  
94609jody\_london\_consulting@earthlink.net

JAMES WEIL  
AGLET CONSUMER ALLIANCE  
PO BOX 37  
COOL, CA 95614jweil@aglet.org

KAREN LINDH  
LINDH & ASSOCIATES  
7909 WALERGA ROAD, NO. 112, PMB 119  
ANTELOPE, CA 95843karen@klindh.com

KEITH R. MCCREA  
SUTHERLAND, ASBILL & BRENNAN, LLP  
1275 PENNSYLVANIA AVE., N.W.  
WASHINGTON, DC 20004-  
2415keith.mccrea@sablaw.com

LYNNE BROWN  
CALIFORNIANS FOR RENEWABLE ENERGY, INC.  
24 HARBOR ROAD  
SAN FRANCISCO, CA 94124\_lbrown369@yahoo.com

Andrew Campbell  
CALIF PUBLIC UTILITIES COMMISSION  
505 VAN NESS AVENUE  
SAN FRANCISCO, CA 94102-3214agc@cpuc.ca.gov

ANDREW ULMER  
CALIFORNIA DEPARTMENT OF WATER  
RESOURCES  
3310 EL CAMINO AVENUE, SUITE 120  
SACRAMENTO, CA 95821aulmer@water.ca.gov

DI CAPO BALDASSARO  
CALIFORNIA ISO  
151 BLUE RAVINE ROAD  
FOLSOM, CA 95630bdcap@caiso.com

CARL SILSBEE  
SOUTHERN CALIFORNIA EDISON  
2244 WALNUT GROVE AVENUE  
ROSEMEAD, CA 91770carl.silsbee@sce.com

CARLOS F. PENA  
SEMPRA ENERGY LAW DEPARTMENT  
101 ASH STREET  
SAN DIEGO, CA 92101cfpena@sempra.com

CLARE LAUFENBERG  
CALIFORNIA ENERGY COMMISSION  
1516 NINTH STREET, MS 46  
SACRAMENTO, CA 95814claufenb@energy.state.ca.us

Christopher R Villarreal  
CALIF PUBLIC UTILITIES COMMISSION  
505 VAN NESS AVENUE  
SAN FRANCISCO, CA 94102-3214crv@cpuc.ca.gov

DANIEL C. ENGEL  
FREEMAN, SULLIVAN & CO.  
101 MONTGOMERY STREET, 15TH FLOOR  
SAN FRANCISCO, CA 94104dengel@fiscgroup.com

DANIEL W. DOUGLASS  
DOUGLASS & LIDDELL  
21700 OXNARD STREET, SUITE 1030  
WOODLAND HILLS, CA  
91367dougllass@energyattorney.com

EDWARD VINE  
LAWRENCE BERKELEY NATIONAL LABORATORY  
BUILDING 90-4000  
BERKELEY, CA 94720elvine@lbl.gov

ERIC WOYCHIK  
COMVERGE, INC.  
9901 CALODEN LANE, STE 1  
OAKLAND, CA 94605ewoychik@strategyi.com

GEOFF AYRES  
THE ENERGY COALITION  
15615 ALTON PARKWAY, SUITE 245  
IRVINE, CA 92618gayres@energycoalition.org

JAMES BOOTHE  
THE ENERGY COALITION  
9 REBELO LANE  
NOVATO, CA 94947ja\_boothe@yahoo.com

JEFFREY P. GRAY  
DAVIS WRIGHT TREMAINE, LLP  
505 MONTGOMERY STREET, SUITE 800  
SAN FRANCISCO, CA 94111-6533jeffgray@dwt.com

Jason R. Salmi Klotz  
CALIF PUBLIC UTILITIES COMMISSION  
505 VAN NESS AVENUE  
SAN FRANCISCO, CA 94102-3214jk1@cpuc.ca.gov

JOYCE LEUNG  
SOUTHERN CALIFORNIA EDISON COMPANY  
6060 J IRWINDALE AVE.  
IRWINDALE, CA 91702joyce.leung@sce.com

JOSEPHINE WU  
PACIFIC GAS AND ELECTRIC COMPANY  
PO BOX 770000, MAIL CODE B9A  
SAN FRANCISCO, CA 94177jwud@pge.com

KA-WING MAGGIE POON  
2244 WALNUT GROVE AVE.  
ROSEMEAD, CA 91770ka-wing.poon@sce.com

GREGORY KLATT  
DOUGLASS & LIDDELL  
411 E. HUNTINGTON DRIVE, STE. 107-356  
ARCADIA, CA 91006klatt@energyattorney.com

LARRY R. COPE  
SOUTHERN CALIFORNIA EDISON  
2244 WALNUT GROVE AVENUE  
ROSEMEAD, CA 91770larry.cope@sce.com

## Service List for Proceeding R. 07-01-041

LUKE TOUGAS  
PACIFIC GAS AND ELECTRIC COMPANY  
PO BOX 770000, MC B9A  
SAN FRANCISCO, CA 94177LATc@pge.com

LESLIE WILLOUGHBY  
SAN DIEGO GAS AND ELECTRIC COMPANY  
8305 CENTURY PARK CT.  
SAN DIEGO, CA 92123willoughby@semprautilities.com

MIKE MESSENGER  
CALIFORNIA ENERGY COMMISSION  
120 ADELAIDE STREET WEST SUITE 1600  
TORONTO, ON M5H  
IT1mike.messenger@powerauthority.on.ca

PHILIPPE AUCLAIR  
11 RUSSELL COURT  
WALNUT CREEK, CA 94598philha@astound.net

RICHARD MCCANN  
M.CUBED  
2655 PORTAGE BAY ROAD, SUITE 3  
DAVIS, CA 95616mccann@umich.edu

ROBIN J. WALTHER, PH.D.  
1380 OAK CREEK DRIVE., 316  
PALO ALTO, CA 94305rwalther@pacbell.net

SUSAN MCNEILL  
PACIFIC GAS AND ELECTRIC COMPANY  
PO BOX 770000, B8M  
SAN FRANCISCO, CA 94177-0001sem4@pge.com

Sudheer Gokhale  
CALIF PUBLIC UTILITIES COMMISSION  
505 VAN NESS AVENUE  
SAN FRANCISCO, CA 94102-3214skg@cpuc.ca.gov

STEPHEN D. BAKER  
FELLON-MCCORD AND ASSOCIATES  
9960 CORPORATE CAMPUS DRIVE, STE. 2000  
LOUISVILLE, KY  
40223stephen.baker@constellation.com

TOM KIMBALL  
MODESTO IRRIGATION DISTRICT  
1231 11TH STREET  
MODESTO, CA 95354tomk@mid.org

WARREN MITCHELL  
THE ENERGY COALITION  
15615 ALTON PARKWAY, SUITE 245  
IRVINE, CA 92618wmitchellrunner@socal.rr.com

GRAYSON HEFFNER  
15525 AMBIANCE DRIVE  
N. POTOMAC, MD 20878

LISA TAKEUCHI  
PACIFIC GAS AND ELECTRIC COMPANY  
77 BEALE STREET  
SAN FRANCISCO, CA 94105latd@pge.com

MARCEL HAWIGER  
THE UTILITY REFORM NETWORK  
711 VAN NESS AVENUE, SUITE 350  
SAN FRANCISCO, CA 94102marcel@turn.org

MRW & ASSOCIATES, INC.  
1814 FRANKLIN STREET, SUITE 720  
OAKLAND, CA 94612mrw@mrwassoc.com

PATRICIA THOMPSON  
SUMMIT BLUE CONSULTING  
2920 CAMINO DIABLO, SUITE 210  
WALNUT CREEK, CA  
94597pthompson@summitblue.com

ROGER PELOTE  
WILLIAMS POWER COMPANY  
12736 CALIFA STREET  
VALLEY VILLAGE, CA  
91607roger.pelote@williams.com

ANNIE STANGE  
ALCANTAR & KAHL  
1300 SW FIFTH AVE., SUITE 1750  
PORTLAND, OR 97201sas@a-klaw.com

MICHAEL ROCHMAN  
SPURR  
1430 WILLOW PASS ROAD, SUITE 240  
CONCORD, CA 94520service@spurr.org

SNULLER PRICE  
ENERGY AND ENVIRONMENTAL ECONOMICS  
101 MONTGOMERY, SUITE 1600  
SAN FRANCISCO, CA 94104snuller@ethree.com

STEVE GEORGE  
GSC GROUP  
101 MONTGOMERY STREET, 15TH FLOOR  
SAN FRANCISCO, CA  
94104stephengorge@fcgroup.com

VICKI L. THOMPSON  
SAN DIEGO GAS & ELECTRIC COMPANY  
101 ASH STREET  
SAN DIEGO, CA 92101vthompson@sempra.com

Rebecca Tsai-Wei Lee  
CALIF PUBLIC UTILITIES COMMISSION  
505 VAN NESS AVENUE  
SAN FRANCISCO, CA 94102-3214wtr@cpuc.ca.gov

BRUCE PERLSTEIN  
PACIFIC GAS AND ELECTRIC COMPANY  
245 MARKET STREET  
SAN FRANCISCO, CA 94105

DONALD C. LIDDELL  
DOUGLASS & LIDDELL  
2928 2ND AVENUE  
SAN DIEGO, CA 92103liddell@energyattorney.com

MARIAN BROWN  
SOUTHERN CALIFORNIA EDISON  
6040A IRWINDALE AVE.  
IRWINDALE, CA 91702marian.brown@sce.com

MARGARET SHERIDAN  
CALIFORNIA ENERGY COMMISSION  
1516 NINTH STREET, MS-22  
SACRAMENTO, CA 95814msherida@energy.state.ca.us

PETER OUBORG  
PACIFIC GAS AND ELECTRIC COMPANY  
77 BEALE STREET, B30A  
SAN FRANCISCO, CA 94105pxo2@pge.com

ROGER VAN HOY  
MODESTO IRRIGATION DISTRICT  
1231 11TH STREET  
MODESTO, CA 95354rogerv@mid.org

SHIRLEY WOO  
PACIFIC GAS AND ELECTRIC COMPANY  
77 BEALE STREET, B30A  
SAN FRANCISCO, CA 94105saw0@pge.com

SHARON TALBOTT  
EMETER CORPORATION  
ONE TWIN DOLPHIN DRIVE  
REDWOOD CITY, CA 94065sharon@emeter.com

SARA STECK MYERS  
122 28TH AVENUE  
SAN FRANCISCO, CA 94121ssmyers@att.net

TRENT A. CARLSON  
RELIANT ENERGY  
1000 MAIN STREET  
HOUSTON, TX 77001tcarlson@reliant.com

VIKKI WOOD  
SACRAMENTO MUNICIPAL UTILITY DISTRICT  
6301 S STREET, MS A204  
SACRAMENTO, CA 95817-1899vwood@smud.org

Tim G. Drew  
CALIF PUBLIC UTILITIES COMMISSION  
505 VAN NESS AVENUE  
SAN FRANCISCO, CA 94102-3214zap@cpuc.ca.gov

CALIFORNIA ISO  
151 BLUE RAVINE ROAD  
FOLSOM, CA 95630

Lisa-Marie Salvacion  
CALIF PUBLIC UTILITIES COMMISSION  
505 VAN NESS AVENUE  
SAN FRANCISCO, CA 94102-3214lms@cpuc.ca.gov

MARK S. MARTINEZ  
SOUTHERN CALIFORNIA EDISON  
6060 IRWINDALE AVE., SUITE J  
IRWINDALE, CA 91702mark.s.martinez@sce.com

NORA SHERIFF  
ALCANTAR & KAHL, LLP  
120 MONTGOMERY STREET, SUITE 2200  
SAN FRANCISCO, CA 94104nes@a-klaw.com

RICHARD H. COUNIHAN  
ENERNOC, INC.  
45 FREMONT STREET, SUITE 1400  
SAN FRANCISCO, CA 94105rcounihan@enernoc.com

REED V. SCHMIDT  
BARTLE WELLS ASSOCIATES  
1889 ALCATRAZ AVENUE  
BERKELEY, CA 94703rschmidt@bartlewells.com

SCOTT H. DEBROFF  
SMIGEL, ANDERSON & SACKS  
4431 NORTH FRONT STREET  
HARRISBURG, PA 17110sdebloff@sasllp.com

LINDA Y. SHERIF  
CALPINE CORPORATION  
3875 HOPYARD ROAD, SUITE 345  
PLEASANTON, CA 94588sherif@calpine.com

STACIA OKURA  
RLW ANALYTICS, INC.  
1055 BROADWAY, SUITE G  
SONOMA, CA 95476stacia.okura@rlw.com

TED POPE  
ENERGY SOLUTIONS  
1738 EXCELSIOR AVE.  
OAKLAND, CA 94602ted@energy-solution.com

WILLIAM H. BOOTH  
LAW OFFICES OF WILLIAM H. BOOTH  
1500 NEWELL AVENUE, 5TH FLOOR  
WALNUT CREEK, CA 94596wbooth@booth-law.com

KEN SKINNER  
INTEGRAL ANALYTICS, INC  
312 WALNUT STREET, SUITE 1600  
CINCINNATI, OH 45202

## **Attachment A**

CALIFORNIA  
ENERGY  
COMMISSION

**PROTOCOL DEVELOPMENT FOR  
DEMAND RESPONSE CALCULATION —  
FINDINGS AND RECOMMENDATIONS**

**CONSULTANT REPORT**

February 2003  
400-02-017F



Gray Davis, *Governor*

# CALIFORNIA ENERGY COMMISSION

***Prepared By:***

KEMA-XENERGY

Miriam L. Goldberg and G. Kennedy Agnew  
Madison, Wisconsin

***Prepared For:***

Michael Messenger,

***Contract Manager***

Michael Messenger,

***Project Manager***

Scott W. Matthews,

***Deputy Director***

**Energy Efficiency and Demand Analysis**

Robert L. Therkelsen,

***Executive Director***

## **DISCLAIMER**

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# ***Report Summary***

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## ***Protocol Development for Demand Response Calculation***

The California Energy Commission has sponsored the development of a standardized measurement and verification protocol for use in calculating demand reductions by participants in Demand Response programs<sup>1</sup>. The protocol provides different methods to estimate the baseline electricity load profile for different types of customer load, against which peak load reductions can be calculated. The baseline electricity load profile is estimated using historical and current meter data, and represents the load that would be expected to occur in the absence of a curtailment request. The protocol may be used for price or emergency based programs that require customer-specific load reduction estimates as a basis for determining payments or incentives. Completion of the protocol is aimed at increasing small and medium-sized customer participation in demand response programs by (1) reducing the barriers related to inconsistency and confusion about how peak savings will be calculated and (2) ensuring that only real and verifiable peak load reductions receive payments.

The development of this standard peak savings protocol was based on interviews with stakeholders in several different jurisdictions and states and statistical testing of several alternative protocols for baseline load estimation. The analysis process used hourly load data from several hundred commercial and industrial customers. The study also proposes terminology for describing baseline calculation methods.

This work is intended to provide the foundation for a revised protocol that may be adopted as part of the International Performance Measurement and Verification Protocol. The IPMVP organization has participated in the development of this report and recommendations. The goal of this report is to establish a clear vocabulary for use in describing the methods used to estimate peak load reductions delivered in response to emergency or price conditions for use in future state or regional protocols. The report also offers guidelines on good estimation practice and the pros and cons of alternative peak savings calculation methods.

### **CRITERIA FOR SELECTING A GOOD BASELINE METHOD**

Criteria that were balanced in developing a method to estimate baselines and peak savings include:

- **Simplicity**, including ease of use, ease of understanding, and low costs for participant and operator to calculate the baseline load profile and resulting savings.
- **Accuracy**, including lack of bias (i.e., no systematic tendency to over- or under-state reductions), appropriate handling of weather-sensitive accounts, and verifiability

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<sup>1</sup> This report was prepared by KEMA-Xenergy consulting for staff of the California Energy Commission. Copies of the report can be downloaded from the Commission's website at [www.energy.ca.gov/demandresponse](http://www.energy.ca.gov/demandresponse).

- **Minimization** of the ability for customers to game or inflate their baseline load profile
- **Predictability**, or the ability for customers to know the baseline before committing to a particular curtailment amount and event
- **Consistency** with other peak saving methods used by utilities and independent system operators

As a result of the analysis of customer data sets, it was decided the protocol should:

- allow for calculation options that recognize different customer and building circumstances
- favor simple calculation methods if the potential accuracy gains of from more complex methods appear to be slight
- indicate alternatives and trade-offs with respect to the selection criteria

## **Recommendations**

### ***Offering Options***

Baseline calculation protocols used for demand response programs should allow the program administrator to select the most appropriate method based on each customer's load type and operating practices. One way to simplify the provision of options is to establish a default calculation method for all programs or building types and then allow certain deviations in the method for special types of customer accounts.

The basis for the selection of a method should include the customer's business type, historical load patterns, and operating practices. For example, a customer who indicates a desire to be able to cancel a work shift in advance of the control period should have access to a baseline calculation method that does not distort the estimated baseline because of this practice.

At the same time, the program administrator should have some discretion to bar customers from using a calculation approach that they appear to have manipulated in the past. Thus, if there is evidence that a particular customer tends to inflate load after notification, beyond what would reasonably be expected for pre-cooling, that customer might not be allowed to use a method that includes an adjustment to the average load profile based on energy use in pre-curtailment hours.

### ***Practical Default and Alternative Baseline Calculation Methods***

The baseline calculation method found to work best for a range of load types consists of taking a simple average of the last 10 days of demand data, by hour of the day, and then shifting the resulting profile up or down so that it matches the average observed load for the period 1 to 2 hours prior to curtailment. This method can be recommended for both weather-sensitive and non-weather-

sensitive accounts, with both low and high variability, for summer and non-summer curtailments.

If the default method is problematic either because of the potential for customer gaming or because of a need to curtail more promptly, the next best alternative depends on the weather sensitivity and energy use variability of the account. The default and alternatives that performed reasonably well for different types of accounts and seasons are indicated below.

**Table 1  
Methods for Estimating a Baseline Energy Use Profile  
By Customer Account Type and Event-Specific Baseline**

Season:	Summer				Nonsummer			
	Weather-Sensitive		Non-Weather-Sensitive		Weather-Sensitive		Non-Weather-Sensitive	
	Low	High	Low	High	Low	High	Low	High
<b>DEFAULT Baseline Profile</b> : 10 day average baseline load profile (BLP) plus additive adjustment based on actual energy use for 1-2 hours prior to demand response signal.	X	X	X	X	X	X	X	X
<b>ALTERNATIVES:</b>								
10 day average BLP plus additive adjustment based on actual load for three to four hours prior to demand response signal.			X	X			X	X
Weather model to construct BLP based on actual average outside temps when DR signal sent; diagnostics model used to determine if building loads are sufficiently weather sensitive to use this approach.	X	X	X					
Use only the highest five of the last 10 days to construct BLP, with scalar adjustment based on a Temperature-Humidity Index load model.	X	X				X		
Use only the highest five of the last 10 days to construct BLP, without any adjustment for control day.					X			
Use the highest 10 of the last 11 days to construct BLP without adjustment for control day conditions.			X	X			X	X

*Baseline load profile-* The kw demand levels for each hour of a 24 hour day averaged over the previous 10 non curtailment days

*Additive adjustment:* The adjusted BLP is calculated by adding a fixed amount A to the 10 day average BLP for each hour.

*Demand response signal:* Price or emergency signal sent to request reduced electric loads for a fixed time period

*Scalar adjustment:* The adjusted BLP is calculated by multiplying the 10 day average DLP for each hour by a fixed amount S.

*Weather model:* Hourly load data from non-curtailed days is fit by a regression model using weather and calendar variables. The BLP is the fitted model applied to the observed conditions during and after a DR signal.

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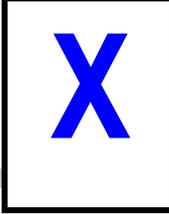
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## **X.1 INTRODUCTION**

### ***X.1.1 Background on this Project***

During the electricity crises of the last two years, a number of states and utilities within these states have developed programs to encourage customers to reduce their peak loads on short notice (under 2 to 24 hours) in exchange for some form of compensation. Such demand response (DR) programs depend on a credible operational procedure for determining the magnitude of load reductions for each customer during each load reduction period.

The use of inconsistent methods for calculating baselines and corresponding load reductions has caused both confusion and dissatisfaction among participating customers. The lack of a standard measurement procedure may be reducing the number of customers willing to participate in DR programs, particularly in smaller- and medium-sized commercial customers in California.

### ***X.1.2 Objectives***

The objective of this work is to develop a standardized measurement and verification (M&V) protocol for use by building engineers, facility operators, or outside M&V experts to “measure” the load drops achieved at a premises. Completion of this protocol is aimed at increasing participation in DR programs from small- and medium-sized customers by reducing the barriers related to inconsistency and confusion about baseline methods.

### ***X.1.3 Project Steps***

Steps in the project include:

- Review of existing methods
- Testing of alternative methods on data sets from various locations and customer types
- Draft report on findings and recommendations, circulated for review and presented for discussion at a public workshop
- Final report
- Submission of the final recommendations to the International Performance Measurement and Verification Protocol (IPMVP) organization for adoption as part of the IPMVP.

This is the final report on findings and recommendations. Included are the review of existing methods and the results of tests on alternative methods.

#### **X.1.4 The Role of the IPMVP**

The IPMVP organization has participated in the development of this report and recommendations. The organization is responsible for the continued development and dissemination of standardized verification methods. It is hoped that the involvement of the IPMVP at various stages of review and the anticipated adoption of the DR protocol as an IPMVP document will represent a broad base of support for the framework developed.

There are direct parallels in the current demand response area to what was occurring in the world of M&V for energy-efficiency performance contracting eight years ago. The core concept of the IPMVP document is that parties involved in contracts to reduce energy use should have a common language with which to structure and manage the settlement of those contracts. The IPMVP was designed to allow parties flexibility in designing M&V procedures that make sense for each contact.

As is true for the energy-efficiency IPMVP, the intent of this report is not to provide a prescriptive set of steps and rules. Rather, the goal is to establish a clear vocabulary, and to offer guidelines on good practice and the pros and cons of alternative method specifications. Toward the goal of developing consistent terminology, this document develops a taxonomy of different methods and attempts to provide clear definitions. We anticipate that a discussion of definitions and distinctions will be an important part of the refinement of this document.

#### **X.1.5 The Role of Other Contributors**

This work would not have been possible without the contributions of several other organizations and individuals.

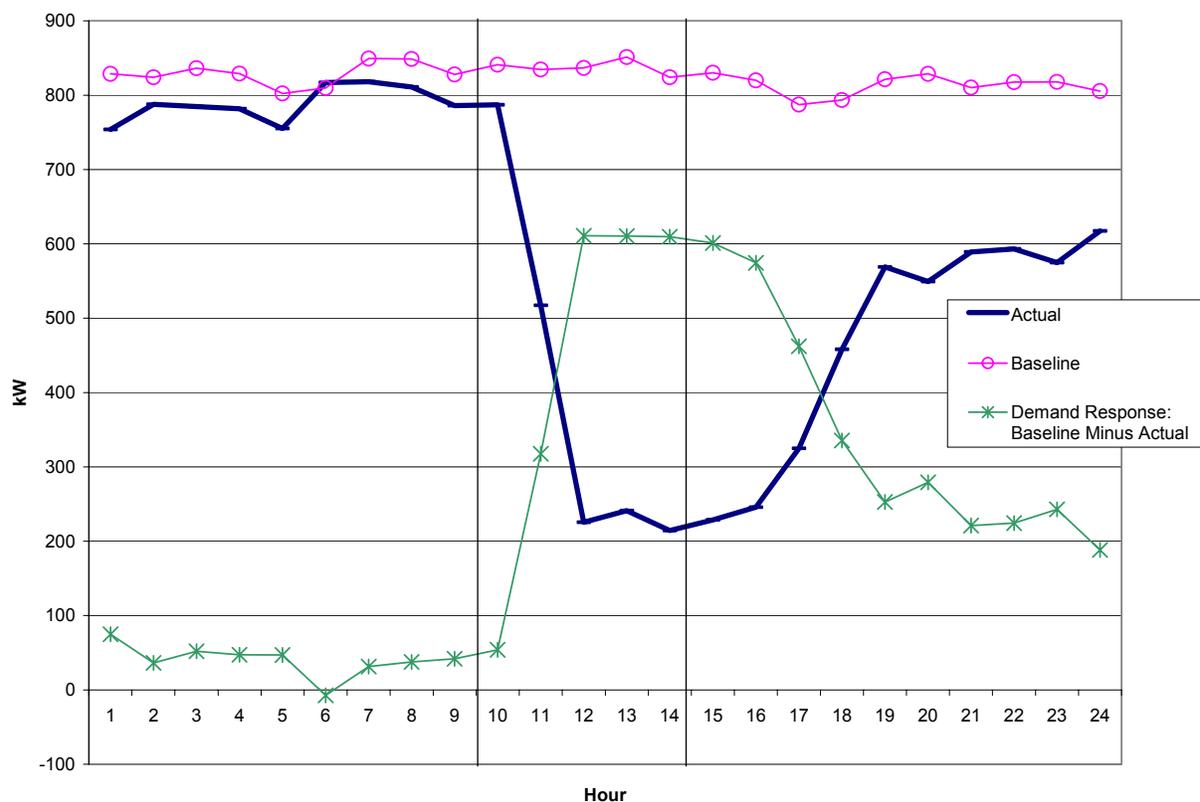
- *Method donors* have shared details of methods they have developed and applied for quantifying demand reductions.
- *Data donors* have provided interval load data from curtailed and noncurtailed customers for use in testing methods.
- *Reviewers* who reviewed the major project deliverables.

## X.2 REVIEW OF EXISTING METHODS

### X.2.1 The Demand Response Baseline

The focus of this study was on calculations of demand response from whole-premise interval load data. Demand response is calculated as the difference between the *baseline* and the actual metered load in each interval (Figure X-1). The baseline is the estimate of what the load would have been in each interval in the absence of the curtailment. Thus, the key question for the demand response calculation is how the baseline is determined.

**Figure X-1**  
Example of Demand Response Calculation from Baseline and Actual Loads



### X.2.2 Desirable Features in a Demand Response Baseline Calculation Method

Most of the goals developers described for the baseline were similar. They were

- to reflect load that would have been used absent the program,
- ease of use for program participants,

- ease of use for program administrators, and
- deterrence of gaming.

Given the multiple objectives, all customer baseline developers understood that the baseline methodology they chose was a compromise. Criteria that are balanced in developing a baseline include

- Simplicity
- Ease of use
- Ease of understanding
- Verifiability
- Accuracy
- Lack of bias (i.e., no systematic tendency to over- or under-state reductions)
- Ability to handle weather-sensitive accounts fairly
- Minimization of gaming
- Ability to be known prior to customer's commitment to a particular curtailment amount and event
- Costs for participant and operator to implement
- Consistency with other ISOs.

### ***X.2.3 Components of Whole-Premise Baseline Calculation Methods***

Baseline calculation methods based on whole-premise interval-metering data can be described in terms of three fundamental components:

- **Data selection criteria** determine what days and time periods of data will be used in the baseline calculation.
- The **estimation method** is a calculation procedure that determines the provisional baseline load at each interval for the curtailment day, using the data selected by the data selection criteria.
- The **adjustment method** shifts or scales the provisional baseline to align it with known conditions of the curtailment day.

#### ***Data Selection Criteria***

Common starting points for data selection include

- Use of the last 10 to 20 uncurtailed business days
- Use of a subset of the last 10 or 11 business days that had the highest load

- Use of a full season of data.

Selection criteria include varying procedures for excluding days from the starting point and replacing excluded days, sometimes in an iterative process.

### ***Estimation Method***

Most estimation methods can be characterized as either an average or some form of weather-based regression model.

### ***Adjustment Methods***

Common adjustment methods (used to adjust interval meter on the day of the curtailment) include:

- Unadjusted
- Additive
- Scalar
- Weather-based additive or scalar.

### ***X.2.4 Characterization of Existing Methods***

Existing baseline estimation methods are summarized in Figure X-1 in terms of the components discussed above.

**Figure X-2  
Summary of Existing Baseline Estimation Methods**

	Load Type Differences Addressed*	How Weather Sensitivity is Addressed**	Time Interval	Data Selection			Estimation Method	Adjustment Hours, If Adjusted
				Initial Timeframe	Final Selection	Excluded Days (other than weekends and previous program Control days)		
PJM-Day Ahead 2002	WS/NWS, Self Gen, Cust. Spec.	Top 5 of 10, Optional adjustment to control-day weather	Hourly	10 days, n-2 to n-11	High 5 of 10	Low Output Days.	Interval Average	h-1, h-2.
PJM Emergency	None	None	Hourly	Hour before	Same	None		
ISO-NE 2001-2002	WS/NWS, Self Gen,	Adjustment to control-day load	Hourly	10 days, n-1 to n-10	Same	Extreme Output Days.	Interval Average	h-1, h-2.
NYISO-DADRP 2001	Self Gen	Top 5 of 10	Hourly	10 days, n-2 to n-11	High 5 of 10	Low Output Days.	Interval Average	
NYISO-DADRP 2002	WS/NWS, Self Gen	Top 5 of 10, Optional adjustment to control-day load	Hourly	10 days, n-2 to n-11	High 5 of 10	Low Output Days.	Interval Average	h-3, h-4.
ERCOT-BUL 2002	WS/NWS	Optional adjustment to control-day load	15 minute	10 days, n-1 to n-10	Middle 8	None	Interval Average	h-1, h-2.
CAISO 2001#1	None	None	Hourly	10 days	None	None	Interval Average	
CAISO 2001#2	None	None	Hourly	11 days	None	None	Interval Average	
XENERGY	WS/NWS	Regression-based estimate, Adjustment to control-day load	Hourly	Variable	None	None	Regression-based	h-1, h-2.
LBNL/Kinney	WS/NWS	Regression-based estimate	Hourly	10 days, n-1 to n-10	None	None	Regression-based	
Nexant	WS/NWS	Adjustment to control-day load	15 minute	10 days	None	None	Interval Average	h-1
Utility A	WS/NWS	Adjustment to control-day load	Hourly	Previous Month	None	All Days that do not fit the match-day criteria.	Interval Average	one hour, 8am - 11am
Utility B	None	None	Hourly	5 days	None	Customer-specified anomalous loads	Interval Average	
Utility C	WS/NWS	Regression-based estimate	Hourly	Undefined minimum data	None	None	Regression-based	
Utility D	WS/NWS	Regression-based estimate	Hourly	Weekdays, June through September	None	None	Regression-based	5am - 10am
Utility E	None	Match based data selection	15 minute	Undefined	10 Days with min. SSE compared to day n-1	None	Interval Average	All match-day hours.
Utility F	WS/NWS, Cust. Spec.	Adjustment to control-day load	Hourly	2-3 previous years	None	Anomalous loads	Interval Average	h-1, h-2.
CMTA Proposed OBMC	WS/NWS	Adjustment to control-day load	Hourly	10 days, n-1 to n-10	None	None	Interval Average	h-1 through h-4

\* WS/NWS: Different methods for weather-sensitive and nonweather-sensitive loads  
Self Gen: Different methods for onsite generation

\*\* Top 5 of 10: Select 5 days with highest average load during the hours curtailed on the curtailment day

### X.3 FINDINGS FROM METHOD TESTS

Several combinations of data selection criteria, estimation method, and adjustment were tested on interval load data from curtailed and uncurtailed customer accounts across the country. A total of 646 accounts were included in the tests. For accounts that were not curtailed, baseline estimates were compared with actual load for each hour of an actual or simulated curtailment period. For accounts that were curtailed, each candidate baseline estimate was compared with the estimate produced by the “best” method.

Performance of each method was assessed in terms of both bias and overall error magnitude. Bias is the systematic tendency to over- or under-state the baseline and corresponding demand reduction. Variability is how wide the swings are around the typical or expected value. Overall error magnitude reflects both bias and variability.

Key findings are indicated below. These findings indicate the effects of various method features on bias and variability as measured in this study for the accounts and specific methods tested. These results offer general guidelines, but the performance of a particular method in a particular situation may be different.

#### X.3.1 Adjustments

- Additive adjustment to the load data from two hours before curtailment can often reduce the bias and variability of almost all methods, including weather models, for weather-sensitive or non-weather-sensitive, high or low variability accounts. Other types of adjustments can improve the performance of averages, but generally with higher bias and variability.
- With this additive adjustment, simple averaging methods in most cases perform essentially as well as complex weather models, even for weather-sensitive accounts.
- Without adjustment, most averages tend to understate the load impacts of a curtailment.
- Additive adjustment to the last 2 hours before a curtailment can be problematic for several reasons:
  - ① It opens the possibility of gaming by deliberately increasing load just before the curtailment period to boost the baseline.
  - ① Legitimate pre-cooling in response to a curtailment notice or expectation will also erroneously increase the baseline.
  - ① Conversely, an operation that achieves its curtailment target promptly upon notification and before the beginning of the required curtailment period will have a severely understated baseline.

### **X.3.2 Data Selection**

- Bias and variability of weather models tends to be reduced by the use of longer input data series, but not dramatically.
- The decreased variability with longer input series is more noticeable for conditional weather models applied to non-weather-sensitive accounts, particularly high-variability accounts.
- The different average methods performed similarly in terms of bias and variability, except for those that select a subset of days based on high load.
- For summer loads, the High 5 of 10 average generally reduces the otherwise negative bias. For summer loads using additive adjustment, the High 5 of 10 days gave the lowest bias measure of any of the averages, for both weather-sensitive and non-weather-sensitive accounts, and comparable variability. The High 10 of 11 average method gave some bias reduction, but not as much.
- For nonsummer loads, however, the High 5 of 10 average method inflates an already positive bias. The other averages perform better and roughly comparably to each other, in terms of both bias and variability, for both weather-sensitive and non-weather-sensitive accounts. The High 10 of 11 is somewhat better than the others in terms of the bias and variability measured in this study.

### **X.3.3 Weather Modeling**

- For summer weather-sensitive accounts, weather models tend to perform somewhat better than averages, but the difference is not dramatic.
- For summer non-weather-sensitive accounts, use of a “conditional” weather model does not increase bias or variability. The conditional weather model automatically deletes weather terms if the statistical diagnostics based on the load data indicate these terms are inappropriate for a particular account. Use of such diagnostics protects against retaining terms in the model that are not well determined and are likely not to be meaningful. Thus, if weather models are used, a single methodology can be applied to both weather-sensitive and non-weather-sensitive accounts.
- For nonsummer loads, weather models do not perform better than averages.

**X.4 PROS AND CONS OF ALTERNATIVE APPROACHES**

Advantages and disadvantages of key method features in terms of the criteria indicated in Section X.2.2 are summarized in the table below. This table is based on both qualitative considerations and the results of the performance tests.

**Table X-1  
Advantages and Disadvantages of Key Baseline Method Features  
Based on Qualitative Considerations and Test Results**

Baseline Method	Variant	Pros	Cons	
Average	Any	Simple, easy to use and understand, low cost	Tends to understate baseline for weather-sensitive loads, especially if unadjusted	
	High 5 of last 10 days	Partial adjustment for weather-sensitive loads	Still tends to understate baseline for weather-sensitive loads	
			Can allow windfall load reduction credit on cool days	
Regression	Any	Provides baseline corresponding to particular weather conditions of curtailment day	More complex, harder to understand, higher cost	
			If observations don't include conditions as extreme as the curtailment day, model estimate may be inaccurate	
			If account isn't weather-sensitive, may be less accurate than simpler methods	
	Full Season	Adequate data and range of variation to yield accurate coefficients	Operating conditions from the period data are taken from may be different from curtailment day	
	Recent 10 days	Operating conditions more likely to be similar to curtailment day	Model based on limited data may be inaccurate	
	Lag temperature/degree-day	Tends to reduce bias for weather-sensitive accounts	Tends to increase variability of baseline estimate.	
Adjustment to precurtailment hours	Any	Simple, easy to use and understand, low cost	May be potential for gaming behavior during day-of-curtailment adjustment period	
			Adjusts to weather and operating conditions of curtailment day	Appropriate pre-curtailment increase in load (e.g., pre-cooling) will result in overstated baseline
			Limits potential for collecting windfall credits for planned shut-downs	Pre-curtailment decrease in load in response to curtailment request (e.g., long ramp-down, canceling a shift) will result in understated baseline
	Additive	May adjust well for load change that is constant throughout day (e.g., industrial processes)	May not be appropriate if load changes during curtailment period (ratio adjustment may be better suited)	
	Scalar	May adjust well for load change that is function of exogenous factor throughout day (e.g., higher levels of occupancy)	May not be appropriate if the day-to-day load variation is constant over the day (additive adjustment may be better suited)	
	to last 2 hours before curtailment period	If load in these hours is unaffected by anticipated or initiated curtailment, provides best accuracy	If substantial curtailment is initiated in these hours, severely understates baselines	
	to 3rd and 4th hour before curtailment period	Less potential for understated baseline due to pre-curtailment-period demand response	More variability than adjustment to last 2 hours	
Weather-Based Adjustment	Any	Explicitly takes into account weather conditions	Adjustment may not be known to customer until after curtailment period (i.e., until after weather conditions are known for the day)	
			No opportunity for gaming as with adjustment to precurtailment hours	If no observations are available for extreme conditions, estimates used for adjustment may be outside range of model
				Will badly predict load reductions if the buildings are dominated by internal loads
				Less accurate than alternative adjustments or weather model for both weather-sensitive and non-weather-sensitive accounts

## X.5 RECOMMENDATIONS

In developing our recommendations, we did not attempt to score each method or feature with respect to each of the desirable features indicated above, nor assign explicit weights to the criteria. In general, our approach is

- allow for options that recognize different circumstances
- favor simplicity if the potential accuracy gains of greater complexity appear to be slight
- indicate alternatives and trade-offs with respect to the criteria.

### X.5.1 *Proposed Approaches by Account Type*

#### *Offering Options*

A general recommendation is that baseline calculation protocols should provide for alternatives based on customer load characteristics and operating practices. One way to simplify the provision of options is to establish a default method and allow certain deviations.

The basis for the selection of a method should be not just the customer's business type, but also the load patterns evident in the data as well as the customer's description of operating practices. Thus, for example, a customer who indicates a desire to be able to cancel a shift in advance of the control period should have access to a baseline calculation method that is not distorted by this practice.

At the same time, the program operator should have some discretion to bar customers from using an approach that they appear to have manipulated in the past. Thus, if there is evidence that a particular customer tends to inflate the baseline load after notification, beyond what would reasonably be expected for pre-cooling, that customer might not be able to use a method that includes adjustment to the 2 pre-curtailement hours.

#### *A Practical Default Baseline Calculation Method*

A method that generally works well for a range of account types is the simple average of the last 10 days, with additive adjustment to the load shape 2 hours prior to the curtailment period. This method can be recommended for both weather-sensitive and non-weather-sensitive accounts, with both low and high variability, for summer and nonsummer curtailments.

This method is not recommended for accounts that tend to curtail in advance of the required period in response to a curtailment notice. It is also not recommended for situations where the potential for gaming is a strong concern, whether across the program or for particular customers.

### ***Alternatives for Summer Weather-Sensitive Accounts***

For summer programs, practical alternatives for weather-sensitive accounts include the following:

- Unadjusted weather models. Longer input time periods to estimate the baseline load are preferable, particularly for high-variability loads.
- The High 5 of 10 day average with Temperature-Humidity Index (THI) adjustment.

Simpler methods with less desirable but potentially acceptable performance include:

- Unadjusted averages, particularly the High 5 of 10.
- Averages or weather models adjusted to the third and fourth hour before curtailment.

### ***Alternatives for Summer Non-Weather-Sensitive Accounts***

For non-weather-sensitive summer loads, the unadjusted High 10 of 11 average performs nearly as well as the recommended default, particularly for low-variability loads. Next best is the simple average of the last 10 days with additive adjustment to the third and fourth hours before curtailment.

For low-variability loads, unadjusted weather models, with weather terms retained only if indicated by the data, actually perform slightly better than the recommended default. However, unlike the case for weather-sensitive accounts, these models perform better if based on shorter periods of data. For high-variability loads, unadjusted weather models tend to be worse than the unadjusted High 10 of 11 average.

### ***Alternatives for Nonsummer Accounts***

For nonsummer loads, modeling is more challenging and there are fewer alternatives. For weather-sensitive accounts, the High 5 of 10 day average with THI adjustment can be used. For low-variability loads, the unadjusted High 5 of 10 day appears to perform slightly better, but for high-variability loads it is worse.

For non-weather-sensitive nonsummer loads, the unadjusted High 10 of 11 appears to be the best alternative. Any of the averages with additive adjustment to the third and fourth hour before curtailment do not perform as well.

### ***Summary of Recommended Methods and Alternatives***

The recommended methods and alternatives for different account types are summarized in the table below.

**Table X-2  
Recommended Methods and Alternatives**

Season	Weather Sensitivity	Variability	Recommended Default			Recommended Alternatives		
			Estimation	Data Selection	Adjustment	Estimation	Data Selection	Adjustment
Summer	Weather-Sensitive	Low	Average	last 10	add 1-2	weather models	any	none
						Average	High 5	THI
Summer	Weather-Sensitive	High	Average	last 10	add 1-2	weather models	longer is better	none
						Average	High 5 of 10	THI
Summer	Non-Weather-Sensitive	Low	Average	last 10	add 1-2	weather models	shorter is better	none
						Average	High 10 of 11	none
						Average	last 10	add 3-4
Summer	Non-Weather-Sensitive	High	Average	last 10	add 1-2	Average	High 10 of 11	none
						Average	last 10	add 3-4
Nonsummer	Weather-Sensitive	Low	Average	last 10	add 1-2	Average	High 5 of 10	none
Nonsummer	Weather-Sensitive	High	Average	last 10	add 1-2	Average	High 5 of 10	THI
Nonsummer	Weather-Sensitive	Low	Average	last 10	add 1-2	Average	High 10 of 11	none
						Average	last 10	add 3-4
Nonsummer	Weather-Sensitive	High	Average	last 10	add 1-2	Average	High 10 of 11	none
						Average	last 10	add 3-4

## X.6 AREAS FOR FUTURE DEVELOPMENT

Reviewers of a draft of this report offered a number of valuable suggestions. Many of these suggestions have been incorporated in the final version. Others, while of considerable merit, were beyond the scope of what could be accomplished in this study.

Most of the suggestions that could not be addressed were in the following categories:

1. Test additional methods
2. Examine results by finer categories of customer type
3. Provide more explicit rules and clear-cut bases for choosing among alternatives, including methods for identifying gaming.

These issues will be explored in further work by the IPMVP Technical Committee. The committee will be building on this study to develop a DR baseline protocol that can be adopted as part of the IPMVP document. The Protocol itself will include the establishment of consistent terminology, guidance on appropriate methods for different situations, and rationale for that guidance. The technical analysis that forms a major portion of this report will not itself be part of the Protocol, but will be referenced as part of the rationale for the guidance.

As part of the further work by the IPMVP, some additional methods may be tested. Candidates for testing include:

- ASHRAE load forecasting models
- variable degree-day models
- use of a single hour or two hours prior to curtailment as a flat baseline.

The additional testing may also examine results by finer segments. Customer type is not known for most of the data sets examined in this study. However, customers can be classified by size, and possibly by other patterns in the load data.

An IPMVP Protocol by its nature will offer options and guidance rather than being prescriptive. However, this Protocol can serve as the basis for establishing specific rules and procedures within a jurisdiction, and provide a common language for understanding these procedures.

## **1.1 PROJECT BACKGROUND**

During the electricity crises of the last two years, a number of states and utilities within these states have developed programs to encourage customers to reduce their peak loads on short notice (under 2 to 24 hours) in exchange for some form of compensation. Compensation may be a specified incentive payment per kW reduced, or other benefits. Many programs involve a contracted magnitude demand reduction, with incentives paid if the contracted load drop is delivered. Some involve a penalty if the contracted reduction is not delivered.

Such demand response (DR) programs depend on a credible operational procedure for determining the magnitude of load reductions. Different regulatory jurisdictions, utilities, and system operators have ended up defining different methods of calculating both the load curtailments achieved by participating accounts and the “baseline” load shapes that should be used to calculate the level of load reduction realized.

The use of inconsistent methods for calculating baselines and corresponding load reductions has caused both confusion and dissatisfaction among participating customers. This situation may serve as a barrier to entry to new customers who want to participate in demand response programs but don’t want to take the time to master the details of estimating and confirming load reductions at their premises. More importantly, the lack of a standard measurement procedure may be reducing the number of customers willing to participate in DR programs, particularly in smaller and medium sized commercial customers in California.

The objective of this work is to develop a standardized measurement and verification (M&V) protocol for use by building engineers, facility operators or outside M&V experts to “measure” the load drops achieved at a premise. Completion of this protocol is aimed at increasing participation in DR programs from small and medium sized customers by reducing the barriers related to inconsistency and confusion about baseline methods.

The intent of the protocol is to facilitate program participation and operations. As a result, the protocol development must consider the practicality of implementation and potential effects on program and customer operations as well as the technical performance of candidate methods. To this end, this work begins with a review of the issues that drive the development of demand response baseline methods, and the rationale behind several existing methods. We then provide the technical performance assessment for a wide range of methods. The recommendations developed attempt to strike a balance between technical accuracy and practical implications for program operators and participants.

## 1.2 PROJECT AND REPORT ORGANIZATION

### 1.2.1 *Steps in the Project*

Project tasks include:

- Review of existing methods
- Selection of alternative methods for testing
- Testing of alternative methods on data sets from various locations and customer types
- Draft report and workshop on findings and recommendations
- Compilation of comments on the draft
- Final report
- Submission of the final recommendations to the International Performance Measurement and Verification Protocol (IPMVP) organization for adoption as part of the IPMVP.

This is the final report on findings and recommendations. Included are the review of existing methods and the results of tests on alternative methods.

### 1.2.2 *Organization of the Report*

The next section provides background on demand response calculation methods. Included here are discussions of the purposes of the calculation, and the rationale for different method features. We provide a taxonomy of demand response calculation methods to provide a consistent vocabulary for discussing these features.

In Section 3 we discuss the issues and concerns that have been at the forefront in the development of demand response calculation methods in different parts of the country. We describe the specific approaches that have been adopted to address these concerns, and summarize advantages and disadvantages of key method features. Appendix A provides further detail on individual methods.

Section 4 describes the analysis conducted to test alternative method performance. Results of the analysis are presented in Section 5. Recommendations based on the review and analysis are offered in Section 6. A glossary of terms is given in Appendix C.

### 1.2.3 *The Role of the IPMVP*

The International Performance Measurement and Verification Protocol (IPMVP) organization has participated in the development of this report and recommendations. The “IPMVP “ refers to a document as well as an organization. The organization is responsible for the continued development of the concept of standardized verification methods, distribution of the document, and providing guidance and training on the appropriate use of the document. The latest document (Concepts and Options for Determining Energy and Water Savings) discusses issues pertaining

to quantifying the long-term results of energy efficiency projects. The core concept of the IPVMP is that parties involved in contracts to reduce energy use should have a common language with which to structure and manage the settlement of those contracts. The IPMVP was designed to allow parties flexibility in designing monitoring and verification (M&V) procedures that make sense for each contact.

There are direct parallels in the current demand response area to what was occurring in the world of M&V for energy efficiency performance contracting eight years ago. Development of protocols for DR calculation methods with the goal that they may be adopted as another IPMVP document means several things. First, two individuals representing the IPMVP organization are actively involved in this project. They bring to the project the lessons and discipline of the earlier IPMVP development. Second, the approach to demand response measurement protocols is similar to that of the energy efficiency IPMVP. That is, the intent is not to provide a prescriptive set of steps and rules. Rather, the goal is to establish a clear vocabulary, and to offer guidelines on good practice and the pros and cons of alternative method specifications. Finally, the involvement of the IPMVP organization at various stages of review and the anticipated adoption of the DR protocol as an IPMVP document will represent a broad base of support for the framework developed.

Toward the goal of developing consistent terminology, this document develops a taxonomy of different methods, and attempts to provide clear definitions. A glossary of terms and acronyms is included as Appendix C. We anticipate that a discussion of definitions and distinctions will be an important part of the refinement of this document.

#### **1.2.4 The Role of Other Contributors**

Several other organizations have contributed to this work in one of several forms:

- *Method donors* have shared details of methods they have developed and applied for quantifying demand reductions.
- *Data donors* have provided interval load data from curtailed and noncurtailed customers for use in testing methods.
- *Reviewers* have (agreed to) review the major project deliverables.

The contributors at the different levels are listed below.

**Table 1-1  
Contributors**

\*† Brian Soth, Director, Retail Energy Products, and Meghan Jonee-Guinn, Operations Manager, Demand Buy Back Program Portland General Electric Company.

\*† Carl Raish, Administrator, Load Research, Tampa Electric.

\* Tennessee Valley Authority.

\*† Suzanne Galster, Load Research Manager, and Brett Johnson, Load Research Contractor/Analyst, Xcel Energy.

\*† Mary Ann Piette, Staff Scientist, and Satkartar Kinney, Senior Research Associate, Lawrence Berkeley National Laboratory.

John Avina, Director of Operations, Abraxas Energy Consulting

Stephen Fernands, President, Customized Energy Solutions

Rich Hackner, GDS Associates/Wisconsin Focus on Energy program

Srinivas Katipamula, Ph.D, Senior Research Scientist, Pacific Northwest National Laboratory

Peter Livingston, PE, CEM, Program Manager, San Diego Regional Energy Office

Gregory Urbin and Mary Straub, Baltimore Gas and Electric Company

Glen Perez, Compliance Audits Manager, California ISO

Linda Low, Mark Martinez, David Reed, and Mark Wallenrod, Southern California Edison

San Diego Gas & Electric Company

Steven Schiller, P.E., Senior Vice President, Nexant, Inc.

Jay Zarnikau, Ph.D., Frontier Associates

Additional data and method donors, names withheld by request.

\* Data Donor

† Method Donor

This section provides background on demand response calculation methods. We begin by discussing the different purposes that a demand response calculation may serve. We then present a “taxonomy” of demand response calculation methods. We describe broad classes of approaches to determining individual customers’ demand reductions during particular control events. We then present a classification scheme for methods based on analysis of whole-premise load data. These methods are the focus of this study.

## 2.1 PURPOSES OF DEMAND RESPONSE CALCULATION METHODS

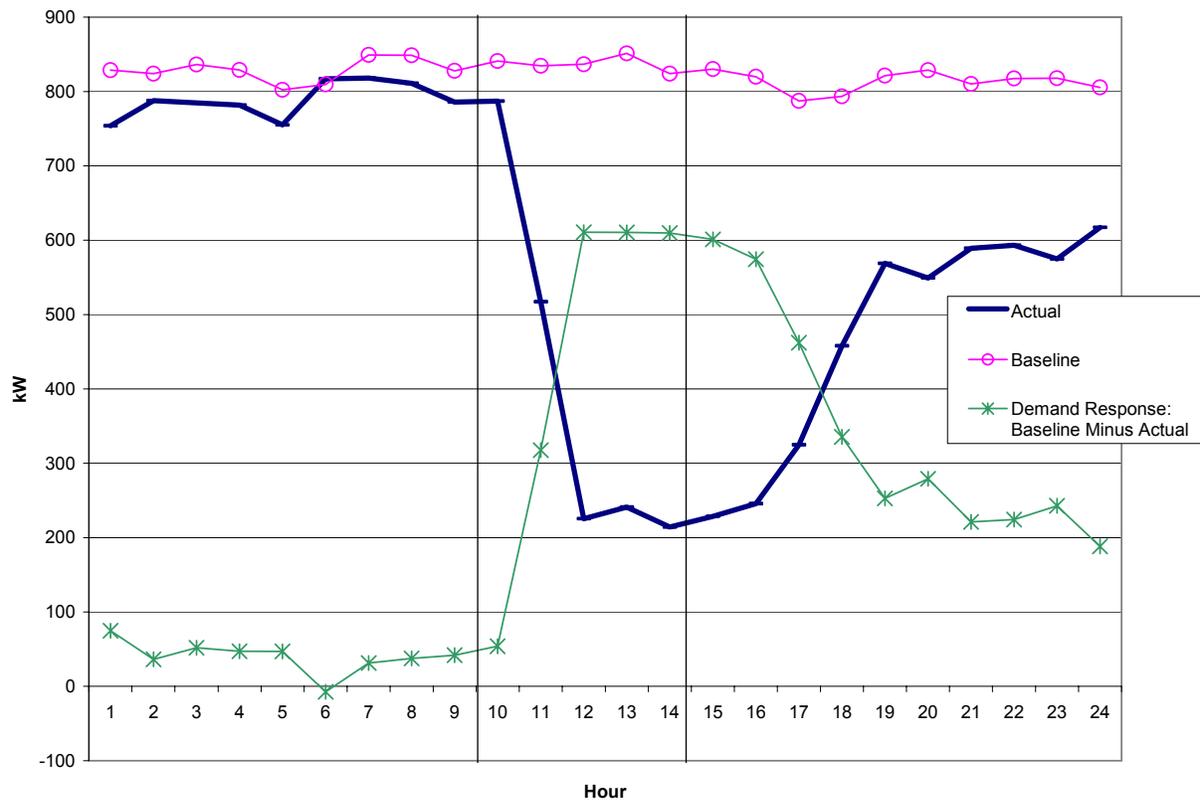
Programs that pay customers according to the amount of demand reduced during each curtailment period require an agreed procedure for calculating this demand response. The objective of this study is to assess alternative methods for this application.

Figure 2–1 illustrates the demand response calculation. The actual load is the customer’s metered load for each hour of the day. This load shows a precipitous drop in response to a curtailment call. The “baseline” is an estimate of what the customer’s load would have been across the day in the absence of the curtailment call. This baseline matches the actual load reasonably well prior to the curtailment. The difference between the baseline and the actual load is the calculated demand response for each hour of the curtailment period. Thus, the load reduction credited to the customer depends on the method for calculating the baseline estimate of what would have occurred in the absence of the program.

There are load management programs that do not require explicit calculation of each customer’s load reduction as a basis for financial settlement between the customer and the utility or program operator. Utility programs based on firm load agreements or stipulated default loads, described below, are primary examples. For these programs, customer load reductions are often calculated for purposes of overall program evaluation and rate setting. Several of the methods reviewed here were developed for this purpose, rather than as a formal basis for financial settlement for program participation.

Demand response calculation methods differ also in the parameters targeted by the calculation. For programs that make payments based on calculated load reduction in each curtailment period, the key parameter is the difference between the actual load (kW) and load that would have occurred absent the program kW for each time increment in the curtailment period. In some cases, the minimum, maximum, or average of these differences over the curtailment period may be of interest. For evaluation, rate setting, and sometimes for determination of capacity requirements in capacity markets, the demand reduction at the time of the system peak is important. Evaluation and payments may also require estimates of total energy reduction (kWh) over control periods as well as demand reduction in each interval.

**Figure 2-1**  
**Example of Demand Response Calculation from Baseline and Actual Loads**



Many of the newer demand response programs offered by Independent System Operators (ISOs) provide monetary incentives to end-users commensurate with actual load reductions. This is a shift from traditional utility load management programs that attract participation with lower tariffs in return for the potential of a certain number of service curtailments. Demand reduction for the ISO programs generally involves computation of the kW reduction for each time increment of the control period. In some cases (e.g., the New York ISO) there are separate protocols for measuring load (kW) demand response as compared to energy (kWh) response, as the demand reduction is bid into two separate markets. The development of a baseline protocol is then at least a partial function of its purpose.

Our review of existing methods and their development focuses primarily on methods developed for ISO or utility programs that attempt to measure the whole-premise demand reduction for each time increment of the control period. Deviations from this context are explicitly noted.

## 2.2 TAXONOMY OF DEMAND RESPONSE CALCULATION METHODS

### 2.2.1 *Classes of Approach*

Crediting customers for demand response or load reduction during a given period requires a means of determining the amount of load reduced. There are three primary classes of approach to the demand response calculation.

- A. **Stipulated Default Load.** The most common example of a stipulated approach is a “firm load” arrangement. A participant reduces load to a pre-determined “firm” load level upon notice. Failure to do so may invoke penalties, expose the participant to market prices, or requires the participant to pay for the energy at a higher than usual price. Determination of payments due to and from the customer depends only on confirmation that the customer’s load did not exceed the firm level during the control period. The credit given to the customer for reducing to the firm level on notice is negotiated in advance, based on an estimate of the typical magnitude of load reduction.

Another version of a stipulated default allows the customer to specify and pay for a base load level. The customer then pays for load above that level or receives credit for load below that level at prices related to market conditions. This approach provides a variant of a real-time pricing program.

- B. **End-Use Metering of Self-Generation.** The demand response is measured as the metered onsite generation. There may be no attempt to account for what level of onsite generation might otherwise have occurred, or to assess whether load at the site has increased in ways that offset the additional generation.
- C. **Whole Premise.** The demand response is measured as the difference between the metered load at each interval and an estimate of the load that would have occurred absent the demand response program. This estimate of load in the absence of the program is referred to by most programs and in this document as the “baseline” or “customer baseline load” (CBL). The baseline is determined from analysis of whole-premise interval metering data before and after the beginning of the control period. The demand response can be a combination of demand reduction and/or increased use of onsite generation. In either case the net load is metered at the whole premise utility or meter service provider revenue meter.

Use of stipulated approaches and metering of self-generation are fairly straightforward and have not been highly contentious. The focus of this review is on the Whole Premise approach, and in particular on baseline calculation methods.

### 2.2.2 Components of Whole-Premise Baseline Calculation Methods

Baseline calculation methods based on whole-premise interval metering data can be described in terms of three fundamental components.

- A set of data selection criteria,
- An estimation method, and sometimes
- An adjustment method.

These three components are explained below. Details on different procedures that have been used for each of them are then described.

#### **Data Selection Criteria**

The data selection criteria determine what data will be used in the baseline calculation. What data selection rules are appropriate depends in part on the estimation method. The selection criteria address both what should be included and what should be excluded. Inclusion is frequently determined by time period (e.g., a certain number of previous days). The other common approach is to select days that are similar to the curtailment day in terms of weather variables and/or system load. Exclusions are less varied across different calculation methods. All baseline calculation methods examined exclude hours in which there was a curtailment in effect. Other exclusion criteria are targeted to identifying abnormal load unrelated to curtailment events. These exclusions vary with particular methods.

#### **Basic Estimation Method**

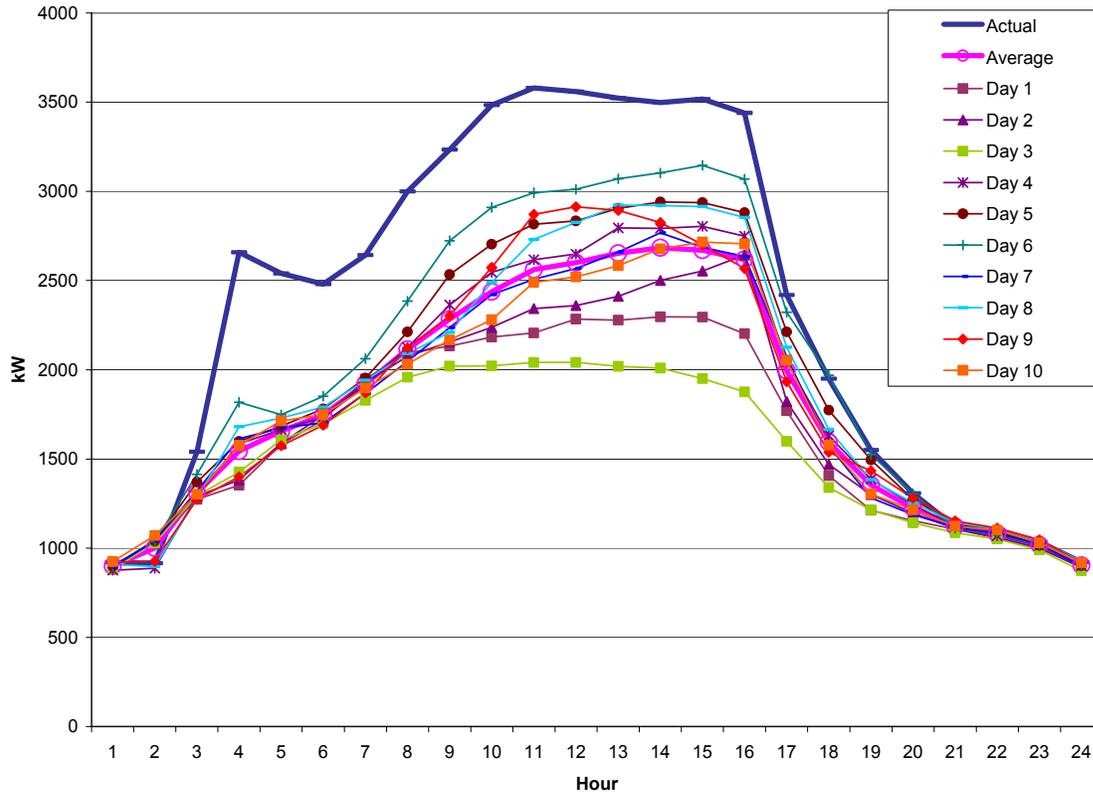
Once the data selection criteria have determined the appropriate data for a baseline calculation, the **estimation method** delivers an estimate of the load curve for the hours in question. If the selection criteria limit the data to a single load observation for each hour, there is no estimation method required. When the selection criteria return more than one possible load for each hour, the estimation method combines these data.

The two general types of estimation methods used are averaging and regression models. Averaging means that for each hour of the control period, the baseline is calculated as the average over all selected days of the load at that hour.

Figure 2–2 below illustrates a baseline calculated as the average of the past 10 uncurtailed business days. This is the baseline method used for the Figure 2-1 above. For the illustration below, a customer that was not curtailed is shown, so that the calculated baseline can be compared with the actual load. The figure shows the hourly loads for each of the 10 days, and the average. Also shown in the figure is the actual load curve on the curtailment day. The loads on the recent uncurtailed days are lower than the loads on the curtailment day. This is a common occurrence when the whole premise consumption, as well as the possibility of curtailment, is

weather sensitive (e.g., curtailment is much more likely on a very hot day). As a result, the average understates the curtailment-day load.

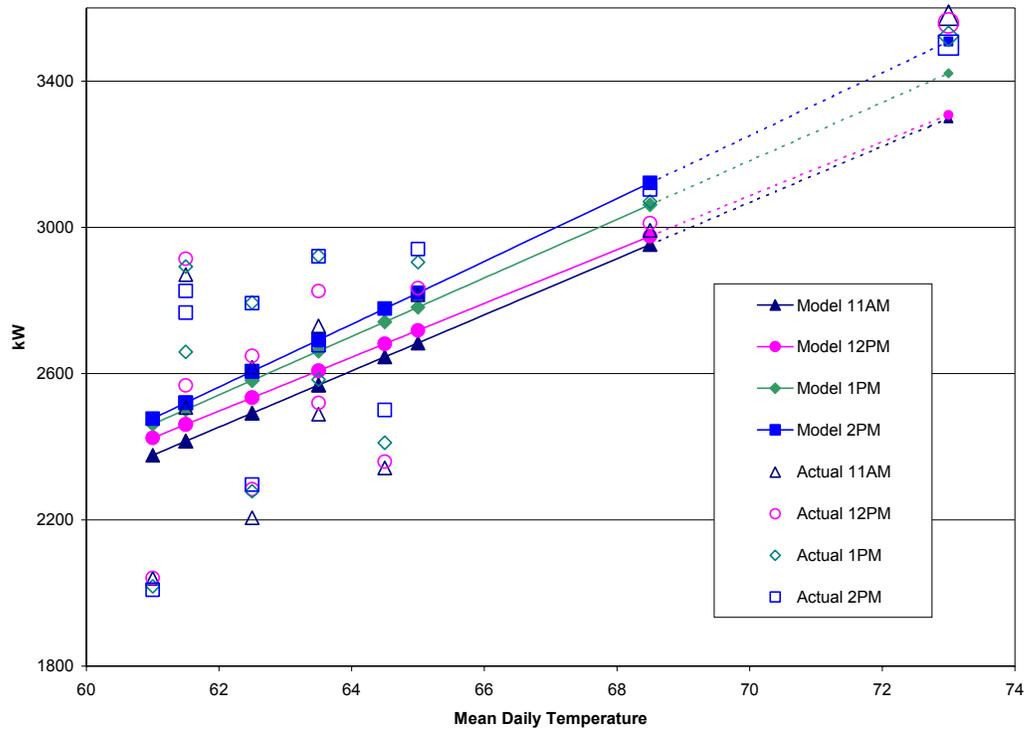
**Figure 2-2**  
**Illustration of Baseline Calculated by Averaging**



A simple regression model using 10 days of data is illustrated in Figure 2–3. In this model, the load  $L_{dh}$  at each hour  $h$  of a given day  $d$  is modeled as a function of the daily cooling degree-days  $CDD_d$ :

$$L_{dh} = \alpha_h + \gamma_h CDD_d.$$

**Figure 2-3**  
**Illustration of an Hourly Regression Model**

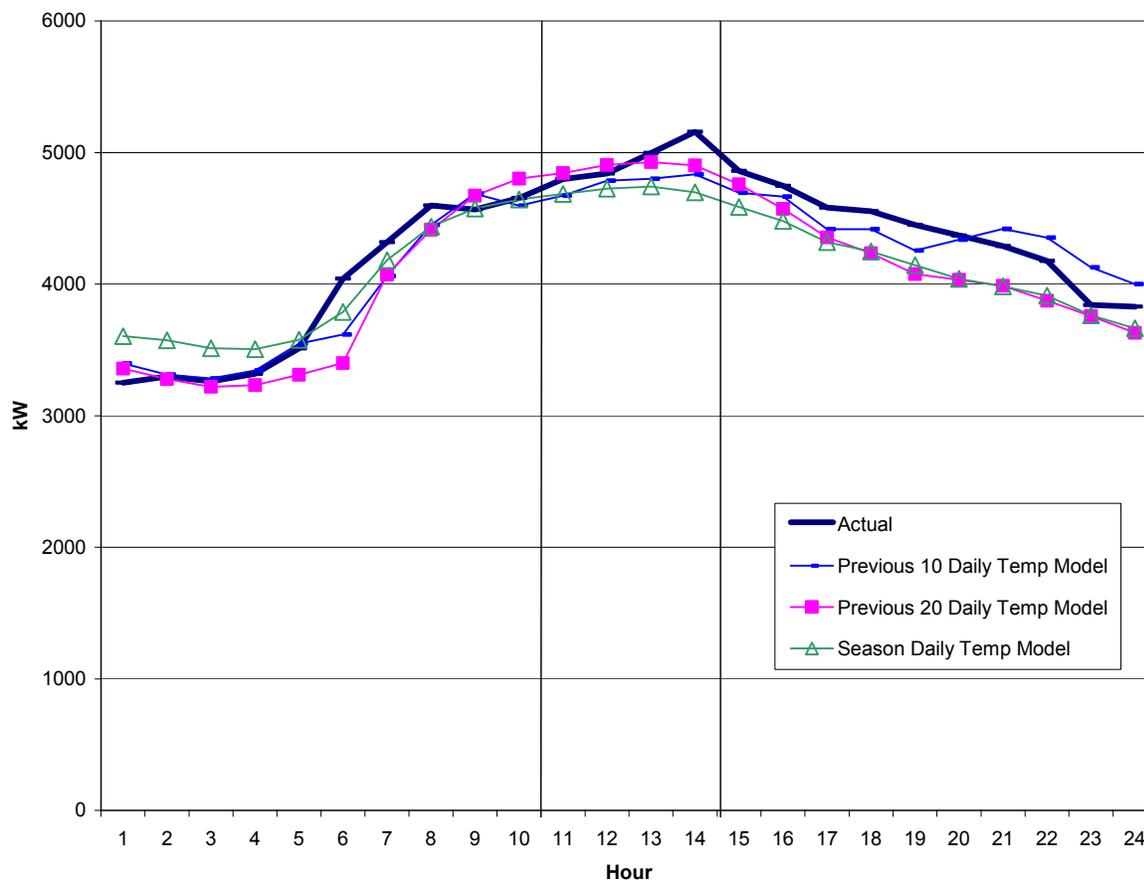


That is, for each hour  $h$  of the curtailment period, a separate line is fit to the loads at that hour.

Figure 2–3 shows the actual load observations for the 10 days, for each hour  $h$  in the curtailment period. Also shown are the fitted lines for each hour. Days used in the regression all had daily temperature below 70°F. At right side of the plot, at a higher temperature than on any of the days used to fit the regression model, are the actual loads on the curtailment day. Despite the scatter in the data, the model does reasonably well at estimating the loads for this day. As in the previous figure, the illustration is for a day when curtailment did not occur, so that the actual load can be compared with the model.

The baseline estimated by this regression model for the curtailment day is shown in Figure 2–4. Also shown in Figure 2–4 are baselines calculated using data from the past 20 uncurtailed days, and using a full season of data. In this example, the models based on different lengths of input data give fairly similar results.

**Figure 2-4**  
**Illustration of Baselines Calculated by Regression Models**  
**Using Varying Data Selection Criteria**



### ***Adjustment Method***

Many baseline calculation methods include an **adjustment method** to take advantage of data from the day of a program implementation. That is, a “provisional” baseline is adjusted to the actual load data of that day. Actual load from some hour or hours immediately preceding<sup>1</sup> curtailment is compared to the provisional baseline created by the estimation method. The provisional baseline is then adjusted to line up with the actual load for those last non-curtailment hours. Adjustment methods vary both with respect to which hours are used for the adjustment and the type of adjustment, typically additive or multiplicative. Further details and specific examples are described below.

<sup>1</sup> ERCOT considered employing an adjustment of load both preceding and following the curtailment call.

### 2.2.3 Further Details on Components of Baseline Calculation Approaches

#### **Common Combinations of Data Selection Criteria and Estimation Methods**

Baseline methods can be defined by any combination of data selection criteria, estimation method, and adjustment method. However, certain data selection criteria and estimation methods tend to be used together, because one is designed to compensate for limitations of the other. The common combinations are the following:

- **Single point data selection criteria – No estimation method required:** These methods involve the selection of a single day or single load levels as the baseline. As a result, no estimation method is required to combine data from multiple days. One example is a flat baseline defined by the load in the hour before curtailment, as in the PJM emergency program. Another is the selection of a single “best-fit” match day based on similarity of temperature, system peak load, or other criteria; in this case, the baseline for each hour is the load on the match day at that hour. Alternatively, the previous day’s hourly loads may be taken as the baseline loads.
- **Multiple day selection criteria – Estimation method required for aggregation:** Multiple days are selected from the recent days. Possible selection criteria are described below. When multiple days are selected, some means is needed to aggregate the load data from these days into a baseline. Averaging by hour of the day is the most common method of aggregation. Regression models are also used.
- **Seasonal data selection criteria – Regression approaches:** When a full season of data are used as the basis for calculating the baseline, regression models rather than simple averages are typically used. Regression techniques allow for the explicit incorporation of additional variables other than loads on uncontrolled days. These methods provide estimates for a particular set of conditions, without requiring that the input data be screened to match those conditions. When a full season of data are used, regression rather than averaging is typically used, to develop an estimate for conditions similar to the curtailment day. However, regression methods can be used with shorter than seasonal data selection.

#### **Estimation by Averaging**

The most common approach is a combination of multiple day selection criteria and a simple average for each hour of the curtailment. Averaging has the advantage of simplicity but depends on the assumption that the selected data approximate what the curtailment day load would have been without the curtailment. If the selected days are expected to be similar to what the curtailment day would have been, the average based on a larger pool of days will be a more accurate baseline. On the other hand, increasing the number of days by including days that are less likely to be like what the curtailment day would have been can make the average less accurate as a baseline.

Key factors that can affect how similar the days in the baseline are to the curtailment day include day type, weather, and structural/operational changes at the facility. Day type is a classification of days according to the calendar, such as by day of the week (at a minimum, weekday or weekend), holiday, and season or month. Facility operations tend to vary with day type. Weather affects heating and cooling loads. Structural or operational changes refer to either changes in the equipment or the building itself, or to long-term changes in operations such as changing shifts or schedules.

### ***Data Selection Criteria Used with Averaging***

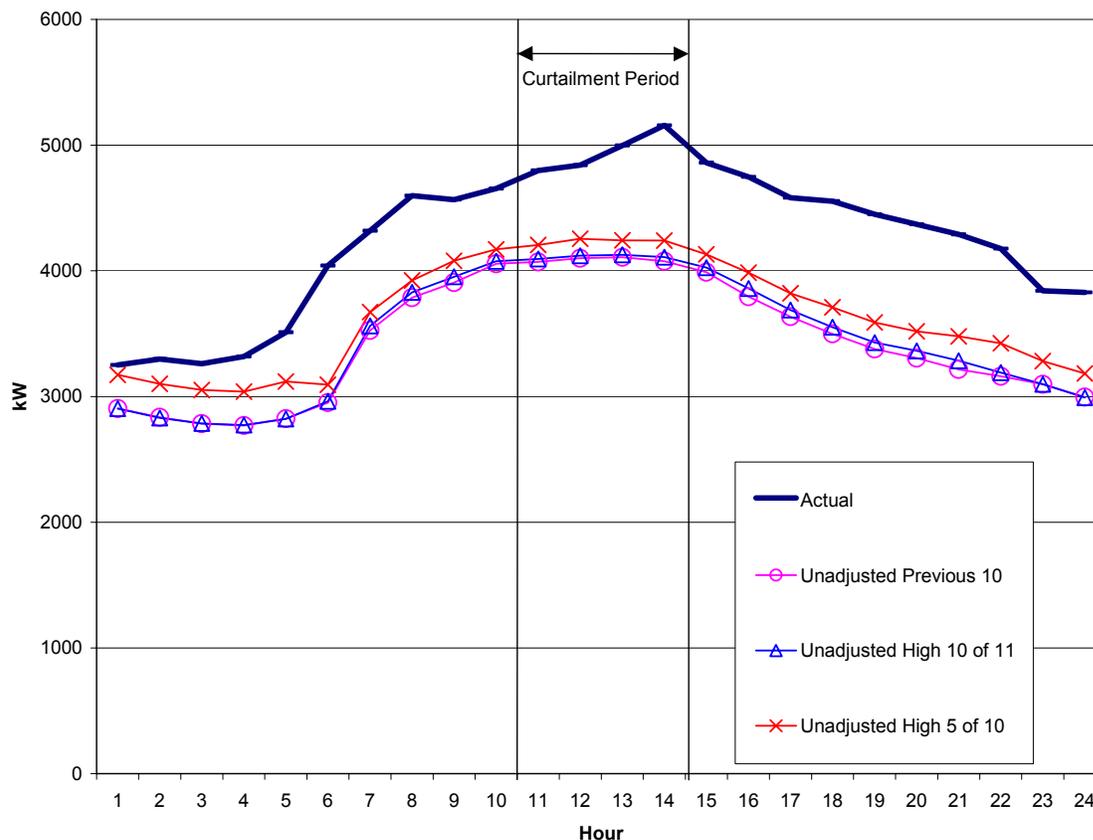
Data selection criteria used with averaging generally limit data so as to limit the potential for distortions in the baseline due to such factors. Most baseline calculation methods used recently by the ISOs limit data to the 10 or 11 preceding business days, excluding days when curtailments occurred. This data restriction removes weekend days and holidays and puts a limit on the ongoing effect of large-scale weather and structural changes. For non-weather-sensitive accounts with a consistent load curve within any two-week period this approach is suitable. Where weather and structural changes are clearly factors within a two-week span, these data selection criteria are limited in their ability to control for these factors in the averages.

Weather is a particularly critical issue when averaging is used and load is weather-sensitive. To the extent that the previous two weeks' weather is not similar to the curtailment day weather, an estimate based on averages will tend to understate baseline loads and corresponding demand reductions. The reason is that curtailment events are most likely to be called during periods of high load, which tend to correspond to extreme weather. Recent uncontrolled days will usually correspond to less extreme weather and loads. Furthermore, the exclusion of recent days with program implementation assures that representative load data will stay out of the sample regardless of whether curtailment took place at a particular site. Thus, estimated baselines for weather-sensitive accounts are likely to be systematically understated for the periods when the baseline calculation is most likely to be needed.

The understatement of load due to weather sensitivity can be addressed both indirectly and directly within the averaging estimation method. An indirect adjustment is to select for the baseline calculation only the recent days with the highest loads. An example is the "5 out of 10" rule used by the NYISO and PJM. From the previous 10 uncontrolled business days, the five days with the greatest curtailment period total load are selected. This approach reduces the problem of understatement of the baseline, but does not eliminate it. Even the highest 5 of the last 10 uncontrolled days will typically have lower loads than would have occurred on a day when curtailment was needed. That is, days when curtailments are called are likely to be more extreme than the days used to construct the baseline, when no curtailment was called. On the other hand, if demand response is invoked on a day when the weather is not extreme, or is extreme only in a small part of the region covered by the curtailment call, any method that selects high load days for defining the baseline would have an upward bias on such days.

Examples of alternative selection rules are illustrated in Figure 2-5 for a particular account on a curtailment day. This example is for an account that was not curtailed, so that the baseline estimates can be compared with the customer's actual metered load. This actual load is the heavy curve in the picture. The lowest curve is the baseline calculated as the simple average of the load at each hour, over the previous 10 uncurtailed business days. The dotted line is for the average of the highest 5 of the last 10 days. Between these two, just slightly above the simple average of the last 10, is the average of the highest 10 of the last 11 days.

**Figure 2-5**  
**Examples of Alternative Selection Rules**



A more direct approach to selecting days for the baseline that are more similar to the curtailed day is to account for weather in the data selection process. Match day criteria, whether load or temperature based, can be used to select days with similar load characteristics. Clearly this approach only works to the extent that such comparison days exist. Match day approaches consequently require a sufficiently large pool of days to select from that comparable days are likely to be found. Match day criteria will be ineffective during the first heat wave of a summer unless either previous summer load is available for consideration, or the baseline calculation can be deferred until more summer data are available. However, any extension of the overall time span from which data can be drawn increases the possibility of structural changes affecting the accuracy of the baseline. This is less of a problem if current season data are used than if prior season data are used. However, for programs that involve financial settlement for individual

control events, parties are typically reluctant to wait until the end of the season to determine curtailment amounts.

### ***Estimation by Regression***

The other common estimation methods are regression-based approaches. An advantage of a regression estimation method is the explicit modeling of factors that cannot be accounted for in an averaging approach.

In simple terms, a regression model determines the relationship between some observable factors and load. Using this relationship, load can be estimated for any scenario based on the levels of those factors for that scenario.

Factors affecting a customer's load at a given hour include:

- Operating schedules across days and hours
- Activity levels, such as production levels at a manufacturing plant, or occupancy levels in a hotel or hospital
- Weather conditions that drive cooling and/or heating loads.

Load models tend to include terms for day type, hour of the day, and weather. While activity levels are important drivers of load, it is difficult to obtain measures of activity that are objective and meaningful for a specific customer. In a customized model, activity measures appropriate to a particular customer can be incorporated.

Regression approaches also have disadvantages. Regression estimation is a more complicated technique than simple averaging. Ease of calculation and transparency are both important considerations for baseline protocols. Regression approaches also can require more data. The concerns with respect to longer data spans and structural load changes remain. That is, obtaining good estimates of the effects of the regression variables requires that data be available over a range of conditions; however, expanding the range of input days increases the chance of including days when the relationships being estimated in the model were different than on the curtailed day. Regression approaches operate on the assumption that the relationship between, say, cooling degree-days and load is the same on curtailment days as on the noncurtailment days that contributed to the regression estimates.

Finally, if the regression model includes factors that do not influence the particular customer's load, the model may simply add noise compared to a simpler average. In particular, using weather models for non-weather-sensitive accounts may do more harm than good.

### ***Data Selection Criteria for Regression Models***

When regression models are used, data selection criteria are typically fairly simple. The key question is how far back, and possibly forward, to go in time. If the regression model is offered

as an alternative to a default averaging method, the regression may use the same data selection rules as for the average.

Regressions based on the past 10 uncurtailed days have the advantage of using operating conditions likely to be similar, apart from weather, to those of the curtailment day. The disadvantage is that the short series means that the model is estimated less accurately. This is particularly a problem if the range of weather variation is slight, which makes it hard to estimate the effects of changes in weather. Moreover, with more limited data, the model diagnostics will be less reliable indicators of whether the model form itself is appropriate to this customer. If the model is not appropriate, using the fitted model to extrapolate to more extreme weather conditions, which is the typical application in this context, can introduce large errors. In addition, a smaller number of input days increases the potential effect of an occasional anomalous day.

Regressions based on a full season of data will tend to be more accurate. However, most program operators and participants do not want to wait until the end of the season to determine curtailment credits. Models based on the previous season can be used. This approach introduces errors if the operations have changed in the interim.

### ***Adjustment Methods***

Adjustment approaches in use include:

- None (unadjusted).
- Additive adjustment. Adjusts a provisional baseline load curve. A constant is added to the provisional baseline load for each hour of the curtailment period. For simple additive adjustment, the constant is calculated as the *difference* between the actual load and the provisional baseline load for some period prior to the curtailment.
- Scalar adjustment. Adjusts a provisional baseline load curve. The provisional baseline load for each hour of the curtailment period is multiplied by a fixed scalar. For simple scalar adjustment, the scalar multiplier is calculated as the *ratio* of the actual load to the provisional baseline load for some period prior to the curtailment.
- Weather-based adjustment. A model of load as a function of some weather parameter is fit to historical load data. The fitted model is used to estimate load (a) for the weather conditions of the days included in the provisional baseline, and (b) for the weather conditions of the curtailment day. The difference or ratio of these two estimates is calculated, and applied to the provisional baseline as an additive or scalar adjustment.

### **Additive and Scalar Adjustments**

The additive and ratio or scalar adjustments are illustrated in Figure 2–6. The unadjusted baseline is the average of the last 10 business days. The additive adjustment shifts this unadjusted baseline up to match the load in the two hour before curtailment. The scalar

adjustment scales the unadjusted baseline to match the load in the same two hours. Both these adjustments bring the unadjusted baseline closer to the actual load during the curtailment period.

**Figure 2-6**  
**Additive and Scalar Adjustments**  
**to the Two Hours Prior to Curtailment**

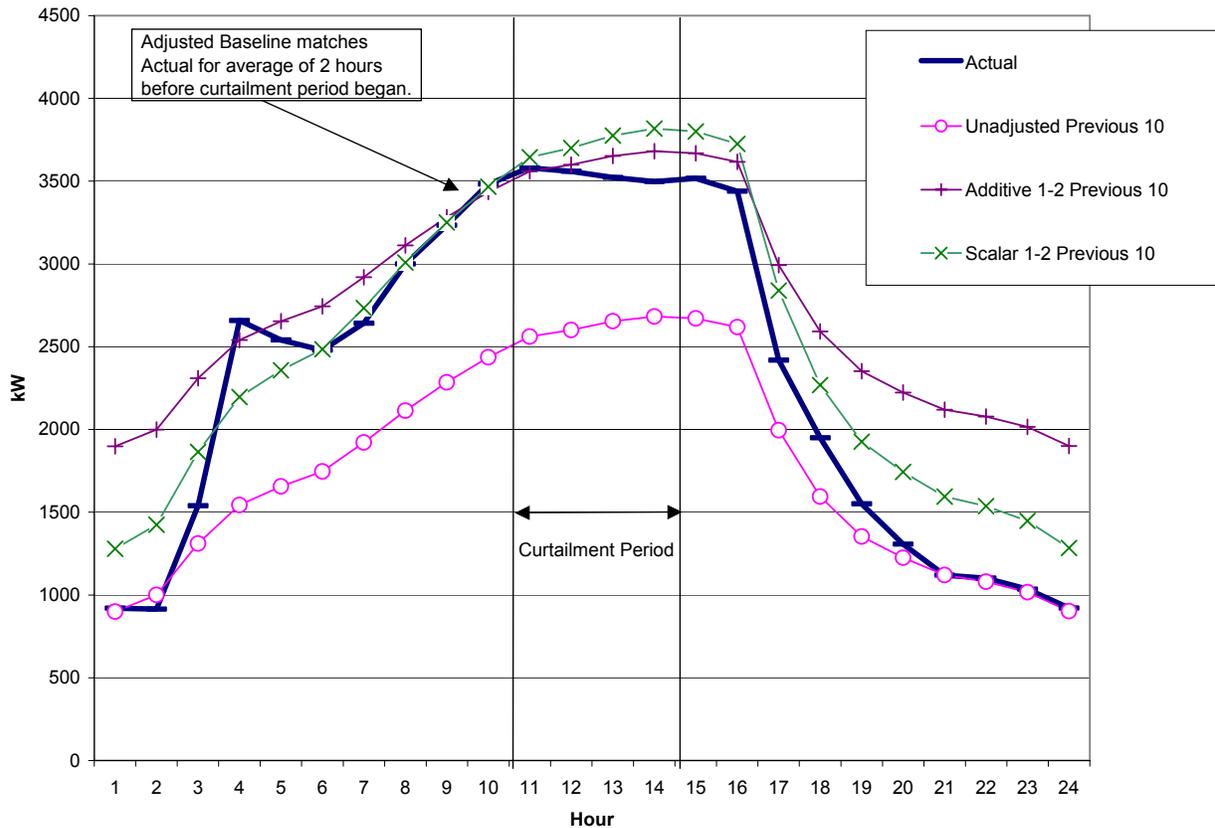
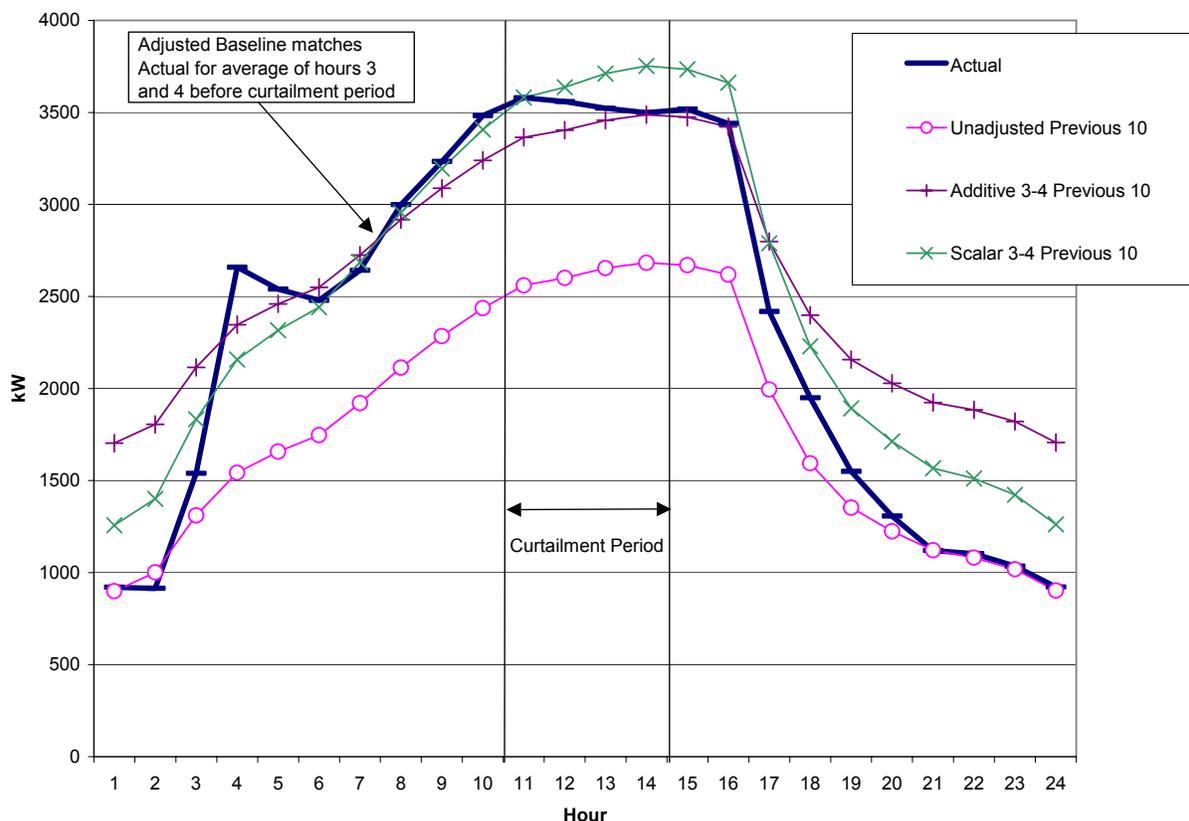


Figure 2-7 illustrates the same type of adjustments, but adjusting to the third and fourth hours before curtailment. This period is typically prior to the time customers would have been notified of the curtailment.

**Figure 2-7**  
**Additive and Scalar Adjustments**  
**to the Third and Fourth Hours Prior to Curtailment**



Reasons to prefer adjustment to earlier hours include the following:

1. There is less opportunity for the customer to manipulate the baseline by artificially boosting load after receiving a curtailment call but before the beginning of the curtailment period.
2. There is less possibility that the baseline will be set too low because the customer began curtailment promptly after notification, prior to the start of the formal curtailment requirement. In these cases, the adjustment to the two hours prior to the curtailment period would shift the baseline down to match already curtailed load.

On the other hand, if neither of these reasons is a concern, the third and fourth hour prior to curtailment may not be as accurate a basis for adjusting the load as the closer first and second hours.

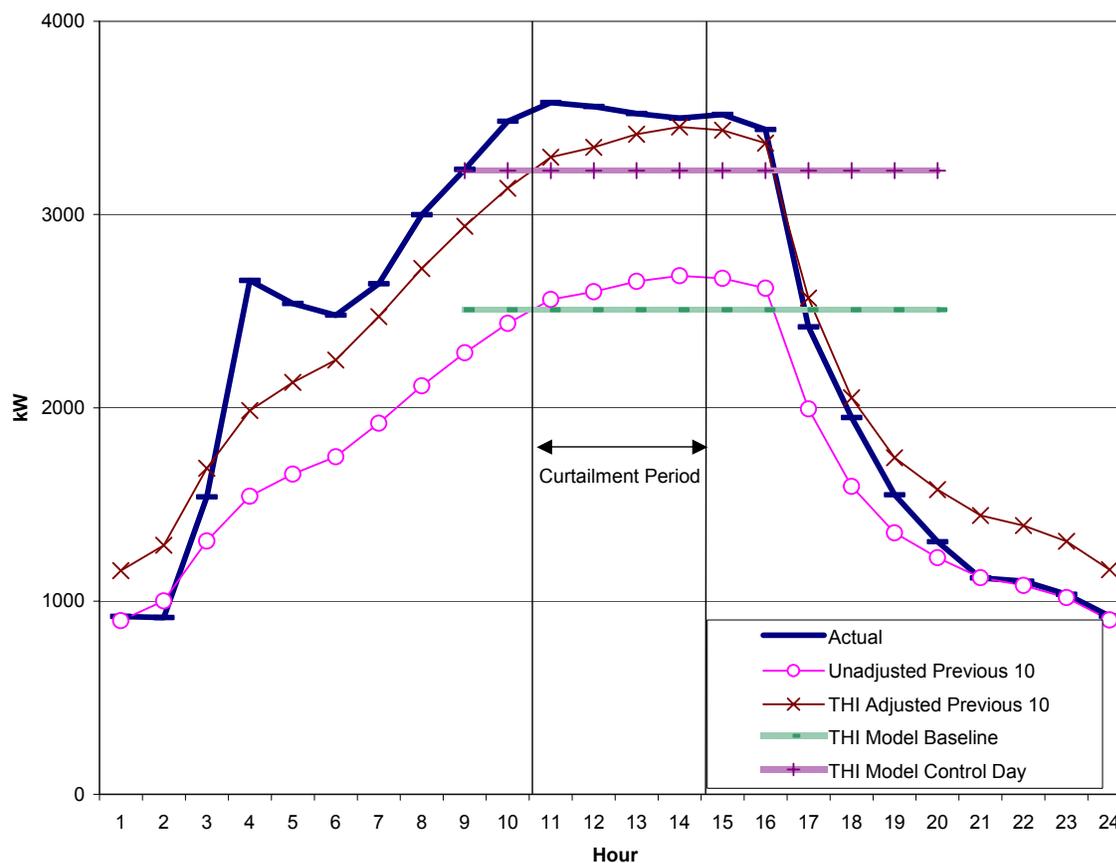
### **PJM Weather-Based Adjustment**

A weather-based adjustment is used by PJM. This method first fits a regression model to load as a function of the temperature-humidity index (THI). The time period used to fit this regression is

longer than the limited window used for the provisional baseline. The fitted model is not used directly to construct the baseline. Instead, the model is used to estimate the load for two conditions, one the average THI for the peak hours of the curtailment day, the other the average THI for the peak hours on the baseline days. The ratio of the modeled curtailment-day load to the modeled baseline-day load is then used as a multiplicative adjustment to the provisional baseline based on a simple average.

The method is illustrated in Figure 2–8. The two horizontal lines spanning the peak hours indicate the THI model estimate of load for the curtailment day and for the baseline days. The bottom load curve is the provisional baseline, the simple average of the last 10 uncurtailed business days. The curtailment-day THI model estimate is around the average value of the actual load across the peak hours on that day, indicating that the THI model itself is doing a reasonable job of matching actual loads. Likewise, the baseline-period THI model estimate is around the average value across the peak hours of the provisional baseline. The final, adjusted baseline is the provisional baseline scaled by the ratio of the two THI model estimates. The THI-adjusted baseline is much closer to the actual load than is the unadjusted baseline.

**Figure 2-8**  
**Illustration of PJM's THI-model Adjustment**



Use of a longer time period as input to the THI regression avoids some potential sources of modeling error. Use of the model to develop an adjustment factor mitigates systematic errors that may exist in the fitted model. Applying the adjustment factor to a baseline developed from recent data limits problems related to operational changes over the time span of the data. The same type of approach could be used with a different weather model, or with an additive rather than scalar adjustment.

### **Effects of Adjustment**

Adjustments may be made to any of the base estimation methods. Adjustment factors take advantage of very recent data to overcome potential limitations of any provisional baseline calculation. Adjustment factors have the obvious advantage of utilizing data from immediately before (and in some cases also after) the curtailment period.

Adjustment methods retain the daily shape produced by the estimation method, but translate it to align with known conditions of the curtailment day. An additive adjustment shifts the curve up or down by a constant amount. A scalar or ratio adjustment scales the shape by a constant amount.

Any such adjustment approach assumes the adjustment hours' load is a fair indicator of that day's load in the absence of curtailment. If the adjustment hours' load is abnormally high, the adjustment and thus the baseline will be high for the whole day. This high load could be the result of the perfectly sound policy of pre-cooling with the intent of shedding load during a curtailment period. It could also be a result of a strategic decision to increase the adjustment and thus increase the credited reduction (i.e., game the baseline). In fact, these two approaches would be indistinguishable to the outside observer and yet both would unfairly overstate the baseline.

Conversely, industrial processes frequently take time to shut down, or schedule operations in blocks of hours. Thus, if a curtailment is required to start at a particular time, it may be necessary to begin the curtailment substantially before that time. As a result, adjustment to the hours just prior to the official start of the curtailment period can produce an unfairly low baseline.

Finally, the hours used for calculating the adjustment amounts often occur during the daily ramping up period (e.g., 8–10 AM). There is potential for more variation during this period of increasing load. This effect can result in wide swings if adjustments are used.

Any of these issues can change an adjustment designed to refine a provisional baseline into an additional source of error. The volatility of adjustment period load, for any of the above reasons, is a fundamental concern with any adjustment approach.

### **Additive Versus Scalar Adjustments**

The two different adjustment methods, additive and ratio, assume a different relationship between adjustment period loads and curtailment period loads. The additive adjustment implicitly assumes that the observed difference between curtailment-day and baseline load at the adjustment hours reflects a difference in operations that would be the same in magnitude across all hours of the day. An example might be a constant-load process that is on or off for the day.

For weather-sensitive accounts, the difference between the provisional baseline and the curtailment day would generally not be expected to be the same in each hour. Nonetheless, several programs use additive adjustments as a rough correction for weather sensitivity.

Some practitioners believe that a ratio or scalar adjustment provides a better correction for weather sensitivity. This adjustment assumes that the difference between the curtailment-day load and the provisional baseline reflects factors that will vary in magnitude roughly in proportion to the hourly provisional baseline. If load is high in the early morning because the day is hot, the increased load will be even greater later in the day. There can also be cases where fluctuations in non-weather-sensitive accounts are better described by scaling a basic load curve than by an additive shift. An additional advantage of scaling compared to an additive adjustment is that scaling avoids the possibility of calculating negative loads for the adjusted baseline.

One way to view a regression approach is that it attempts to find an appropriate mix between adjustments for fixed loads and adjustments for variable loads. Even so, some methods use a mix of regression and additive or scalar adjustment to the curtailment day. One example is the PJM weather-based adjustment, described above. This method uses a weather model as the basis for adjusting a simple average provisional baseline. Conversely, a provisional baseline based on a weather model can be combined with a simple adjustment method, such as the additive adjustment to align with load in the two hours before curtailment.

### ***Methods for Non-Weather-Sensitive Accounts***

While much of the attention in baseline method development has been given to addressing weather sensitivity, many of the customers participating in demand response programs may have little weather sensitivity. Indeed, many of the simpler methods that do not account for weather variation were developed in the context of programs with large, non-weather-sensitive accounts. For such loads, methods designed to mitigate weather-related biases can simply increase random errors.

Many programs address this issue by making weather-adjustment procedures optional. Customers enrolling in the program choose the form of the baseline calculation that will be used. For instance, PJM has three choices: (1) for non-weather-sensitive accounts, (2) for weather-sensitive accounts, and (3) the possibility of a custom baseline (that must be approved).

In this section, a number of existing demand response calculation methods are reviewed. This review was based on several sources:

- public documentation of baseline methods, in particular from ISO and utility websites
- papers shared by analysts who have developed methods, primarily from utilities
- interviews with analysts and stakeholders involved with the method development process at ISOs and utilities.

We begin by describing the process of developing the methods, and the key issues that were considered by the parties involved. We then describe a number of specific methods, and summarize their advantages and disadvantages.

### **3.1 DEVELOPING DEMAND RESPONSE CALCULATION METHODS**

The demand reduction is calculated as the difference between the metered load and an estimated “baseline” in each increment. Thus, the central question is how the baseline is determined. As noted, the accuracy of the calculated baseline as an estimate of what the customer’s load would have been in the absence of the program is only one of several criteria for defining the baseline calculation methods. Other criteria relate to the practicality of the method for operators and customers, and its potential effect on decision-making.

To better understand these other criteria, XENERGY interviewed 11 key participants in the development of the baseline methodology for five independent system operators (ISOs) and three utility programs. Notes of working groups, program and tariff filings reports, and program documentation also informed analysis of the baseline method development. We have also drawn on conference presentations and informal conversations with demand response program analysts and stakeholders in the baseline method development process.

#### **3.1.1 Key Issues**

Key observations on the baseline development process based on this review include the following:

1. The baselines for ISO programs tend to be created by working groups exclusively focused on demand response programs, while small teams or individuals created the baselines of utility programs.
2. Baselines used by utilities for program evaluation are more likely to be calculated from a more sophisticated model.

3. The ISO baselines evolved between the 2001 and 2002 program years.
4. ISOs considered and used different portions of baseline methodologies of other ISOs, but each ISO had its own variant.
5. A baseline approved by another ISO was a significant seal of approval when considering various methodologies.
6. The ISO New England (ISO-NE) baseline development process was much less interactive than the other ISOs.
7. All parties understood that there were imperfections and tradeoffs in their baselines.
8. NYISO (New York Independent System Operator) and PJM (Pennsylvania Jersey Maryland Interconnection) working groups were many times contentious and political. The baseline was just one of many issues in implementing their programs.
9. Trade-offs were made between simple baselines, which were perceived to be less likely to capture the “real” load reductions absent the demand response program, and the more custom baselines for individual sites.
10. Gaming (manipulating load to create a more advantageous baseline) and/or free-ridership (obtaining incentive payments for load reductions that would have taken place without the program) were a major concern in baseline development.
11. There are sharp differences on the issue of demand response and shut-downs. Should all day / long-term shut-downs be compensated? Most of the baselines will not compensate for multiple-day shut-downs.
12. In some cases (the 2001 California ISO Discretionary Load Curtailment Program, and the 2001 and 2002 PJM programs) the managing organization allowed the participant to propose an alternate measurement program that would be reviewed and approved by the ISO. For the California ISO (CA ISO), this allowed for other options such as engineering analysis, operational or test data, use of loggers versus interval metering, etc.
13. While there have been many discussions of the implications of choosing different types of baselines, there has been little statistical justification of choosing a particular baseline. They are all works in progress.

These observations substantially mirror the experiences of developing the energy efficiency IPMVP. This activity involves highly technical situations and requires trained professionals for some of the engineering and statistical calculations. At the same time, establishment of a savings calculation method is primarily a contractual undertaking that seeks to apportion risk and provide fair rewards. Thus, an important first step is to create a framework that any sensible person could understand. Details and refinements can be added in time. Minimizing the number of different variations of reasonable approaches can improve the attractiveness of programs and increase participation levels.

### **3.1.2 The Process of Developing the Methods**

From a process point of view there is generally a sharp differentiation between the utility and ISO development of baselines for the purposes of measuring the impacts of demand response programs. For the ISO programs, the purpose of the baseline is to determine payments to participating customers for individual curtailment events. For traditional utility programs, payments to customers are often not tied to explicit calculations of load reductions.

Even where new utility programs are designed to create market-based mechanisms for demand response, the utility is generally able to develop its baseline approach largely at its own discretion. Their program designs are subject to regulatory review, but are generally not the subject of wide public debate.

By contrast, the ISO, which acts as an impartial market operator, tends to develop baselines through a participatory stakeholder process. The ISO baselines generally have been created via committee, where many parties give their input. The baseline is only one component in the design of a demand-response program. These programs must be approved by vote. One respondent noted that simplicity in explaining the baseline methodology to the voting members was an important criterion.

In addition at the ISO level, demand response programs are looked at warily from entrenched market participants who may lose revenue or be assessed program costs. Counterbalancing this resistance is pressure from the Federal Energy Regulatory Commission (FERC), and state Public Utility Commissions (PUCs) to make economic demand response an important integrated part of the market.

The implementation of the PJM economic load response program has been particularly contentious. Numerous comments and protests have been filed at the FERC for the proposed 2002 program (Docket #ER02-1326). The baseline methodology, and even the use of a baseline as a program component, has been called into question. Specifically in regards to the baseline, PJM has had to defend the use of the five highest days out of ten methodology and the weather-sensitivity adjustment. These method elements are discussed in Section 4.

### **3.1.3 Desirable Features in a Baseline Calculation Method**

Most of the goals developers described for the baseline were similar. They were

- to reflect the estimated level of load (kW) that would have occurred in the absence of the program,
- ease of use for program participants,
- ease of use for program administrators, and
- deterrence of gaming.

Given the multiple objectives, all baseline developers understood that the baseline methodology they chose was a compromise. Development of the ISO's baselines were further complicated by the political realities of the approval process. None of the respondents believes their method is the universal best way to calculate the baseline. In practice, the baseline methodology has been driven by the comparative importance of the objectives of the demand response program, the wholesale environment, the structure of the group choosing the baseline, and financial considerations. The financial impact includes cost to implement (e.g., need for sub-metering) and assessment of program costs (e.g., who is financially responsible for incentive payments).

In program documentation, criteria for the baseline choice were not explicit, with an exception of the development of the Electric Reliability Council of Texas (ERCOT) baseline. Criteria reported by interview respondents generally included:

- Simplicity
- Ease of use
- Ease of understanding
- Verifiability
- Accuracy
- Lack of bias (i.e., no systematic tendency to over- or under-state reductions)
- Ability to handle weather-sensitive accounts fairly
- Minimization of gaming
- Ability to be known prior to customer's commitment to a particular curtailment amount and event
- Costs for participant and operator to implement
- Consistency with other ISOs.<sup>1</sup>

While not necessarily mentioned explicitly, simplicity, ease of use, and ease of understanding are all related to a desire to minimize the burden on participants and program operators. Burden means costs, as well as related time and nuisance factors.

Accuracy has two aspects. One is lack of bias. Bias is a systematic tendency to over- or under-state the baseline and the corresponding demand reduction. The second aspect of accuracy is variability. A method may be close to unbiased, that is, to be close to correct on average, yet have a high variance, meaning it tends to have large errors in either direction. Methods that have high variance are unreliable, and add risk to program participation and operations.

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<sup>1</sup> Indeed, PJM cites consistency with NYISO program as a positive program attribute in a filing to the FERC. *For example, PJM adopted a Customer Baseline Load ("CBL") calculation methodology that is very similar to the one used in the New York program and has thus standardized the measurement of load response.* Response of PJM Interconnection L.L.C. To Protests. Docket ER02-1326 April 22, 2002.

Handling weather-sensitive accounts fairly is a question of both limiting bias and limiting variance related to weather-sensitivity. At the same time, methods introduced to improve baselines for weather-sensitive accounts should not increase errors for non-weather-sensitive accounts.

Gaming issues and the value of knowing the baseline in advance are discussed below.

## 3.2 CONTENTIOUS ISSUES IN BASELINE DEVELOPMENT

As noted, there are a number of desirable features in baseline methods. Attempting to balance competing objectives has been a challenge to the groups that have developed the rules for different areas. Following is a discussion of some of the most contentious issues.

### 3.2.1 Data Selection and Weather Adjustment

Two of the most contentious issues for the baseline has been the justification of the days used to calculate the baseline and the use of a weather-sensitive adjustment. These issues are related, in that the selection of days is used in part to address weather sensitivity. Both PJM and the NYISO have used a “high 5 of 10” method, which selects the 5 days with the highest loads from the past 10 business days. The use of a particular window of days such as the highest 5 of 10 is justified explicitly by PJM in its filing.

*By eliminating the five lowest usage days, PJM creates a baseline that reflects load conditions that most approximate those conditions when load reductions are likely to occur — i.e., when it is hot and consumption is high. Under cool conditions (i.e., low usage days), participants are not likely to reduce load; therefore, to include the low usage days in the calculation would create a baseline that is not representative of the participant’s load absent a load reduction. Further, contrary to Mirant, the baseline methodology should include a weather-sensitivity adjustment, which will serve to either raise or lower a customer’s calculated baseline according to weather fluctuations, eliminating the possibility that utilization of the highest five days prior to a relatively cool day will result in over-estimation of the customer’s actual load.*

The 5 highest out of 10 day methodology was debated at PJM and the NYISO. An alternative methodology of the lowest 5 days out of last 10 was proposed by Mirant at the PJM working group level (see [http://www.pjm.com/committees/user\\_group/dsrwg/meeting/20020225\\_meeting\\_materials.html](http://www.pjm.com/committees/user_group/dsrwg/meeting/20020225_meeting_materials.html)). Mirant contended that this method would be much more likely to deter gaming and reimbursement for load reduction not actually delivered. While this is probably correct, the methodology was not endorsed at the working group level as other priorities prevailed.

The “high 10 of 11,” the average of the highest 10 of the last 11 uncurtailed business days, was employed by the California ISO for its 2001 Demand Relief Program. The adoption of this methodology was relatively uncontroversial according to a California ISO representative. In 2000 the California ISO had a smaller program that used the average of all 10 of the last 10 days for the baseline. This methodology was exactly the same as used by the major utilities for their (similar) programs, and was easily adopted for the 2000 program. In the design of the 2001 Demand Relief Program, the California ISO got input from various stakeholders and reached a consensus to use the previous 11-business days and drop out 1 day that was the lowest demand.

The New York ISO methodology evolved from 2001 to 2002. In 2001 there was the implicit assumption used that the use of the high 5 of 10 methodology was an approximate weather-sensitivity adjustment. According to interviewees, this proved to be insufficient. Accordingly, the New York ISO looked for ways to improve their baseline for weather sensitive accounts for the 2002 baseline. To this end they included an adjustment similar to that used by the ISO New England (ISO-NE).

While most ISOs now include an adjustment as a way of addressing weather-sensitive accounts, the specifics vary. The ISO-NE baseline uses an additive adjustment to the two hours prior to curtailment, as described in Section 2. That is, a constant amount is added to the initial baseline load in each time increment, so that the adjusted baseline matches the metered load for the average of the two hour period prior to the curtailment period. The NYISO, ERCOT, and PJM use a scalar adjustment. That is, the initial baseline load in each interval is scaled by a constant factor. The PJM adjustment, as described in Section 2, does not align the baseline with the observed load at a previous hour; instead, the adjustment scales the provisional baseline according to the relationship between the curtailment day and the baseline as indicated by a weather model.

There has been little hard evidence offered to justify either the additive or the ratio adjustment process. These adjustment procedures are described further in Section 5, and their performance examined.

The utility programs use more sophisticated and more opaque, but possibly more accurate methods to calculate baselines. The Cinergy method is the prime example of this type of methodology. It is econometrically sophisticated (e.g., uses state space and Kalman filtering to estimate mean daily load in the first of two stages of baseline computation), and is proprietary. The Cinergy method almost certainly would be rejected as too complicated for an ISO method. The ISOs, because of their process (e.g. consensus or vote at working group and then approval votes at higher levels) were constrained to relatively simple, straightforward, methods that are (relatively) easy to understand, and replicate.

### **3.2.2 Gaming and Free Ridership**

Establishing rules to limit opportunities for “gaming” or “free ridership” has been a frequent concern in baseline method development. Gaming means manipulating loads deliberately to inflate the baseline artificially and obtain excess incentive payments. Free ridership means obtaining payments for actions that would have been taken anyway without the demand response program. Many data selection rules have been established to limit gaming and free rider opportunities. Some special situations are worth noting.

One situation of particular concern is plant shut-down. Other concerns relate to the potential for demand reductions to be credited when none has taken place. Sometimes procedures designed to reduce systematic over- or under-statement in one situation can generate an opposite potential error in another.

### Shut-Downs

A good deal of discussion in the creation of baselines has been the appropriate way to handle temporary complete or partial closure of customers sites resulting in drastic reductions in load (also known as “shut-downs”). For an industrial plant that shuts down for two weeks over the summer, there have been debates over whether the plant should be able to claim compensation for that load reduction. Many argue that if the plant was going to shut down regardless of a demand response program, and then obtains “windfall” payments from the demand response program, this is a case of free ridership. That is, payments that were intended to provide incentives to change customer behavior are being made to a customer whose behavior is the same as it would have been without the program.

One way the shutdown problem is addressed is by using a baseline with a scalar adjustment to the hours just before curtailment, as described in Section 2. With this adjustment, zero usage during the pre-curtailment period results in a baseline of zero during the curtailment period. Thus, there is no opportunity to collect windfall payments as a free rider in the demand response program for the shut-down.

On the other hand, shut-downs may be initiated, at least in part, because of program incentives. Screening out the largest responses may take away an appropriate mechanism to signal such behavior.

### Minimum Bids to Limit Free Riding on Weather or Shut-Downs

For some economic bidding programs (e.g., New York and PJM) only bids with a minimum price are accepted (e.g., \$50–\$75/MWh). This rule inhibits participants from bidding demand reduction that may be based only on weather effects.

For example, if the baseline is an average with the high 5 of 10 data selection rule, the baseline would tend to overstate expected load on a cool day for a weather-sensitive account. The customer could therefore bid a “reduction,” and count on receiving credit for it, without actually doing anything to reduce load compared to normal operations.

Employing a minimum bid to inhibit free riding on weather implicitly assumes that high prices are strongly correlated with extreme weather conditions. If the minimum bid price is \$75/MWh, and if the price of energy (generally) goes above \$75/MWh only on hot days, then it is impossible to get a “free ride on weather” on cool days. That is, the customer could bid \$75/MWh on cool days, but the bid (generally) would not be accepted because the clearing price would be below that level.

In the absence of a day-of adjustment, the minimum price bid would also deter free riding on shut-downs. For example, if a plant were to be shut down for a week, it would be easy to bid a low price into an economic program for the week and know with near certainty that the load reduction bid would be accepted. The minimum bid price would preclude the acceptance of such bid for “normal” days.

Of course, picking an appropriate minimum bid price is very important. If the market generally has prices higher than the minimum bid (e.g., \$75/MWh in the California ISO during early 2001), then free ridership potential would be high. Conversely, if the market minimum price is set too high, there will be few if any opportunities for demand response participation, and little incentive to invest in demand response systems and technology.

### **Manipulating Baseline Loads**

Gaming, that is altering behavior to artificially inflate a baseline, was also a major concern for many developers of baselines. A number of programs (e.g., ISO-NE, PJM, NYISO) screen out large changes in load in the creation of the baseline. For example, the ISO-NE 2002 program excludes days with four or more consecutive hours that are less than 75 percent or greater than 125 percent the average of a provisional baseline. This means that if a customer sees a heat wave coming, maneuvers of using additional energy to increase their baseline will be restricted.

### **3.2.3 Advance Customer Knowledge of the Baseline**

Another factor considered was the customer's ability to know its baseline prior to committing to a load reduction, particularly for bidding programs. Knowing the baseline prior to commitment reduces customer risk. To meet a program commitment the customer has to reduce total load to the computed baseline level less the amount of the load reduction bid. If the baseline is not determined until after the load reduction commitment is made a risk-averse customer will commit less load reduction than they can deliver in order to ensure that they can deliver their full load-reduction commitment. Generally, customers will not know their baseline prior to load reduction commitment when the baseline includes a day-of curtailment adjustment(s). If a weather adjustment is used, then it is likely that the customer will not know their baseline until after the day (curtailment period) is over as the adjustment will be based on the day (curtailment period) weather conditions.

If the baseline is not determined until after the curtailment, the customer can't know until after the curtailment whether they will be credited with enough load reduction to fulfill their bid commitment. As many programs have penalties for non-performance, bidders will tend to be conservative in their bids.

Not knowing the baseline in advance also increases the cost of participation in these programs, as the bidders must forecast what they believe their baselines will be prior to bidding. That is if baseline is based on weather, then the customer will have to procure a weather forecast, and forecast a baseline in order to determine how much load they should actually reduce in order to meet their load reduction commitment.

On the other hand, knowing the baseline in advance could lead to gaming. For days when the baseline seems to be understated (e.g., cool days after a heat wave), customers could confidently bid load reduction, with the expectation that they will not have to alter their operations at all to be credited with the full load reduction.

Advance customer knowledge was a major issue in the development of the NYISO baseline. For this ISO's day-ahead bidding program the baseline is based on days at least two days prior to the event, or one day prior to the bid. This has the dual effect of

1. allowing the customer to know at the time of the bid decision the baseline that will determine the customer's incentive, and
2. making it more difficult to game the baseline.

For example, in the New York ISO day-ahead bidding program, a bid for Wednesday load reduction is made on Tuesday. Possible days in the baseline begin with Monday and work into the past. Thus, a participant cannot blatantly increase load on Tuesday to boost its baseline. This procedure does not preclude increasing load in the previous days to increase the baseline, but the uncertainty of the market-clearing price makes such behavior risky for participants contemplating premeditated gaming.

### **3.3 CHARACTERIZATION OF DIFFERENT BASELINES**

A categorization of baseline calculation methods reviewed is provided in Table 3-1. More detail on these protocols is provided in Appendix A. A brief discussion of the key features of the methods presented in the table follows.

**Table 3-1  
Summary Baseline Protocol Matrix**

	Load Type Differences Addressed*	How Weather Sensitivity is Addressed**	Time Interval	Data Selection			Estimation Method	Adjustment Hours, If Adjusted
				Initial Timeframe	Final Selection	Excluded Days (other than weekends and previous program Control days)		
PJM-Day Ahead 2002	WS/NWS, Self Gen, Cust. Spec.	Top 5 of 10, Optional adjustment to control-day weather	Hourly	10 days, n-2 to n-11	High 5 of 10	Low Output Days.	Interval Average	h-1,h-2.
PJM Emergency	None	None	Hourly	Hour before	Same	None		
ISO-NE 2001-2002	WS/NWS, Self Gen,	Adjustment to control-day load	Hourly	10 days, n-1 to n-10	Same	Extreme Output Days.	Interval Average	h-1,h-2.
NYISO-DADRP 2001	Self Gen	Top 5 of 10	Hourly	10 days, n-2 to n-11	High 5 of 10	Low Output Days.	Interval Average	
NYISO-DADRP 2002	WS/NWS, Self Gen	Top 5 of 10, Optional adjustment to control-day load	Hourly	10 days, n-2 to n-11	High 5 of 10	Low Output Days.	Interval Average	h-3, h-4.
ERCOT-BUL 2002	WS/NWS	Optional adjustment to control-day load	15 minute	10 days, n-1 to n-10	Middle 8	None	Interval Average	h-1, h-2.
CAISO 2001#1	None	None	Hourly	10 days	None	None	Interval Average	
CAISO 2001#2	None	None	Hourly	11 days	None	None	Interval Average	
XENERGY	WS/NWS	Regression-based estimate, Adjustment to control-day load	Hourly	Variable	None	None	Regression-based	h-1, h-2.
LBNL/Kinney	WS/NWS	Regression-based estimate	Hourly	10 days, n-1 to n-10	None	None	Regression-based	
Nexant	WS/NWS	Adjustment to control-day load	15 minute	10 days	None	None	Interval Average	h-1
Utility A	WS/NWS	Adjustment to control-day load	Hourly	Previous Month	None	All Days that do not fit the match-day criteria.	Interval Average	one hour, 8am - 11am
Utility B	None	None	Hourly	5 days	None	Customer-specific anomalous loads	Interval Average	
Utility C	WS/NWS	Regression-based estimate	Hourly	Undefined minimum data	None	None	Regression-based	
Utility D	WS/NWS	Regression-based estimate	Hourly	Weekdays, June through September	None	None	Regression-based	5am - 10am
Utility E	None	Match based data selection	15 minute	Undefined	10 Days with min. SSE compared to day n-1	None	Interval Average	All match-day hours.
Utility F	WS/NWS, Cust. Spec.	Adjustment to control-day load	Hourly	2-3 previous years	None	Anomalous loads	Interval Average	h-1, h-2.
CMTA Proposed OBMC	WS/NWS	Adjustment to control-day load	Hourly	10 days, n-1 to n-10	None	None	Interval Average	h-1 through h-4

\* WS/NWS: Different methods for weather-sensitive and nonweather-sensitive loads  
Self Gen: Different methods for onsite generation

\*\* Top 5 of 10: Select 5 days with highest average load during the hours curtailed on the curtailment day

### **3.3.1 Purpose of the Demand Response Calculation**

The methods reviewed for ISO programs have all been used as the basis for payments to participants for particular curtailment-day reductions. Many of the other methods reviewed were developed as proposals or custom approaches for use in the ISO programs. Most of the utility methods reviewed were developed for program evaluation rather than as a basis for payments.

### **3.3.2 Addressing Weather-Sensitive Accounts**

Many of the procedures reviewed allow different calculation methods for weather-sensitive and non-weather-sensitive accounts. Methods used to address weather sensitivity include regression models with weather terms, additive and scalar adjustments to curtailment-day load before curtailment, data restriction to days with higher loads, and match days based on load or weather match criteria.

### **3.3.3 Time Increment**

Most of the methods are defined for hourly load data. A few use 15-minute data. The same methods could be used with whatever time increment is required for settlement.

### **3.3.4 Data Selection Criteria**

Most of the methods that use a version of averaging, with or without adjustment, use 10 or 11 noncurtailment business days prior to the curtailment day as the basis for the baseline calculation. Restriction to the 5 days with highest average load out of these 10 and exclusion of extreme high or low load days are common screens. Rules for which days may be included, how far back in time to go to replace excluded days, and the sequence for screening days out and replacing them vary widely across programs and are often complex. Details are provided in Appendix A.

Methods that rely on regression or match days often use a full season or even multiple years of data in the regression. A few regression methods, developed as alternative to ISO averaging methods, rely on the same 10 days as required for the average.

### **3.3.5 Estimation Method**

All the methods reviewed can be characterized as some form of averaging or regression, sometimes with adjustments. The one exception is the PJM emergency program, which uses the single hour before control as the baseline for the entire curtailment period. Thus, there is no “estimation” required other than selecting this hour’s load.

### 3.3.6 Adjustments

Most of the adjustments to curtailment-day conditions match to the load one to two hours before curtailment. Additive and scalar adjustments were roughly equally common.

## 3.4 PROS AND CONS OF ALTERNATIVE APPROACHES

No baseline methodology is perfect. Thus implicit in the choice of any baseline methodology are tradeoffs. The table below summarizes some of the most prominent pros and cons of various baseline methodology components.

**Table 3-2**  
**Pros and Cons of Key Baseline Methods and Combinations**

Baseline Method	Variant	Pros	Cons
Average	Any	Simple, easy to use and understand, low cost	Tends to understate baseline for weather-sensitive loads.
	High 5 of last 10 days	Partial adjustment for weather-sensitive loads	Still tends to understate baseline for weather-sensitive loads
			Can allow windfall load reduction credit on cool days
Regression	Any	Provides baseline corresponding to particular weather conditions of curtailment day	More complex, harder to understand, higher cost
			If observations don't include conditions as extreme as the curtailment day, model estimate may be inaccurate
			If account isn't weather-sensitive, may be less accurate than simpler methods
	Full Season	Adequate data and range of variation to yield accurate coefficients	Operating conditions from the period data are taken from may be different from curtailment day
Recent 10 days	Operating conditions more likely to be similar to curtailment day	Model based on limited data may be inaccurate	
Adjustment to precurtailment hours	Any	Simple, easy to use and understand, low cost	May be potential for gaming behavior during day-of-curtailment adjustment period
		Adjusts to weather and operating conditions of curtailment day	Appropriate pre-curtailment increase in load (e.g., pre-cooling) will result in overstated baseline
		Limits potential for collecting windfall credits for planned shut-downs	Pre-curtailment decrease in load in response to curtailment request (e.g., long ramp-down, canceling a shift) will result in understated baseline
	Additive	May adjust well for load change that is constant throughout day (e.g., industrial processes)	May not be appropriate if load changes during curtailment period (ratio adjustment may be better suited)
	Scalar	May adjust well for load change that is function of exogenous factor throughout day (e.g., higher levels of occupancy)	May not be appropriate if the day-to-day load variation is constant over the day (additive adjustment may be better suited)
Weather-Based Adjustment	Any	Explicitly takes into account weather conditions	Adjustment may not be known to customer until after curtailment period (i.e., until after weather conditions are known for the day)
			If no observations are available for extreme conditions, estimates used for adjustment may be outside range of model
			Will badly predict load reductions if the buildings are dominated by internal loads

A major element of this project was to test several alternative baseline methods on several data sets from different locations. Interval load data were provided for customers who have participated in some type of demand response or controllable rates program. In addition, for most locations load data were also provided for a group of customers of similar size who were not participants in such a program. Performance measures for different baseline methods were developed by analysis of both curtailed and uncurtailed accounts.

In this section, we describe

- the baseline calculation methods selected for testing
- the time periods studied for both controlled and uncontrolled accounts
- the statistics calculated as measures of method performance.

#### **4.1 BASELINE CALCULATION METHODS TESTED**

The taxonomy of existing methods presented in Section 3 classified methods based on three elements:

- data selection criteria
- estimation method
- adjustment method.

We tested various combinations of these elements, rather than testing only those combinations currently being used. Some of the selection criteria in use for specific methods are complex, with an iterative process of screening days out, then going back further in time to replace the eliminated days. For purposes of the tests, we simplified some of these screening rules. We do not believe these simplifications substantially alter the performance characteristics of the methods.

It was not practical to test all possible combinations of candidate selection criteria, estimation, and adjustment methods. We did try to test each component in combination with enough variations in the other components to get a good sense of the effect of each. In addition, we made sure to include the combinations that corresponded most closely to key methods currently in use. In particular, the methods tested include those in use by the ISOs in California, New York, New England, and PJM, except for some details on data selection criteria.

### **4.1.1 Data Selection Criteria**

#### ***Initial Selection***

The initial selection of days for the ISO programs all involve something like the last 2 weeks of business days. Methods used by utilities for program evaluation tend to involve data for a full season. Variations we considered are the following:

- previous 10 business days beginning on d0-1 (California and New England ISOs)
- previous 10 business days beginning on d0-2
- highest 10 of the last 11 business days, beginning d0-1
- highest 5 of the last 10 business days, beginning d0-2 (New York and PJM ISOs)
- previous 20 business days beginning d0-1
- 20 business days from d0-10 to d0+10.
- entire season that includes the control day
- entire season from the previous year that includes the control day

where day d0 indicates the curtailment day.

#### ***Exclusions***

All existing methods delete from the data selection any days that had a control event. Some replace these excluded days by going farther back in time as needed. Similarly, some methods screen out days of low or extreme output based on varying criteria and with or without replacement. For this analysis all excluded control days were replaced with the next eligible day. No extreme output exclusions were tested. If extreme output exclusions were used they would likely affect high variability account results.

### **4.1.2 Estimation Method**

The two broad types of estimation methods are averaging and regression. We describe these methods more specifically below. In the analysis conducted, all load data were available on an hourly basis, and the analysis was conducted on this basis. In some markets, load data are collected and demand response is calculated on a finer time interval, such as half-hour or 15-minute. Our discussion refers to analysis of hourly data. However, the same principles would apply with data at a finer time increment.

#### ***Averages***

Averaging means that the baseline for each time interval of the curtailment day is calculated as the simple average, across all the days chosen by the data selection criteria, of the loads at that

time interval. For example, the baseline for the hour ending 1 pm is the average over all the selected days of the loads on those days for the hour ending 1 pm.

### ***Regression Models***

#### **Types of Models Considered**

Regression can take a wide variety of forms. Regression models are used to construct models that can develop a baseline load curve based on dependent variables related to weather, building operation or other factors. It's beyond the scope of this work to attempt to determine the best general regression model for this application.

In the context of calculating demand response baselines, the regression model uses the data selected for a particular account and event. The model is fit to those data, and applied to the conditions during the event, to estimate the load that account would have in the absence of the control or curtailment, at each time increment in the event. In all applications reviewed and all methods tested, the model is fit separately for each account.

In most cases, the model is also fit separately for each event, because different data are selected. The exception is model fitting based on a full season of data. In these cases, the same model fit applies to all events. The estimated loads vary by event because the control-day conditions vary.

In these models, each observation corresponds to a particular day and hour (or finer time interval). The dependent variable is the account's load at that day and hour. In almost all the applications reviewed, a different set of coefficients is estimated for each hour of the day. The predictor variables are typically weather variables and possibly daytype. Thus, each observation consists of the account's load for a particular day and hour together with the corresponding weather variables.

The purpose of the regression model is to provide a reliable estimate of what the load for a particular customer would have been on a particular day in the absence of a control event. This is somewhat different from contexts where a model must yield reasonable results across a population of customers and over a broader time span. Inaccuracies for an individual customer and event have financial consequences for the customer, and in the long run may affect the customer's willingness to participate in a demand response program.

As noted in Section 2, factors affecting a customer's load on a particular day include the daytype, weather, and activity level. For some customers, activity level may vary from day to day in ways that have substantial effects on load. Thus, data on factors such as production output, occupancy, or number of shifts operated could potentially be useful predictors for some accounts, particularly those that are not weather-sensitive. However, meaningful, objective customer-specific variables that track activity by day are typically not available. Daytype is readily available. However, we assume that attention is restricted to business days within a season. Daytype was therefore fixed within the models tested. Thus, the models tested include only weather terms.

Differences among regression models for this application include the following.

#### *The Type of Weather Variable(s) Included*

Typically, temperature, degree-days, and/or temperature-humidity index are used. Some load research analysts incorporate additional weather terms such as precipitation, cloud cover, sunshine, and wind speed in load models, but these were not used in the primary demand-response estimation methods reviewed. Temperature and humidity are the dominant drivers of cooling loads.

If the facility is consistently in cooling (or heating) mode across the span of the data used in the regression, degree-day variables offer no advantage over temperature variables. However, if the data include milder conditions when cooling or heating is not required, degree-day variables generally perform better. In effect, degree-days “count” temperature only when it is high enough to require cooling or low enough to require heating.

#### *Whether the Degree-Day Base is Fixed in Advance*

If degree-day variables are used, the degree-day base may be fixed in advance or may be determined from the regression. The base or reference temperature for a building is the temperature at which cooling or heating is first required in the building. Cooling or heating degree-days for a day are the difference between this reference temperature and the outside air temperature.

Degree-days calculated at the appropriate temperature are more closely correlated with load than degree-days at other bases. If too low a reference temperature is used for cooling, the model will tend to under-estimate load in hot weather, and overstate load in cooler weather. If too high a reference temperature is used, the opposite occurs.

The appropriate degree-day base varies substantially across buildings. The reference temperature depends on building thermal mass, solar gain, and internal loads. The only meaningful way to determine the best base temperature for a given building is by analysis of load data in relation to temperature data. Models that allow the degree-day base to vary tend to have lower systematic error, but also are more complex, and more time consuming to fit.

These models are also less well determined if data are limited. Thus, if the data selection rules require use of only 10 days of data in calculating the baseline, erratic results might be obtained if the degree-day base is determined separately for each of these 10-day fits. However, it may be effective to estimate the appropriate reference temperature based on a longer history, possibly including the previous year, and use this reference temperature for all baseline calculations for a season.

### *Whether Lagged Weather Terms are Included*

Lag temperature or degree-day terms are used to account for heat build-up over time in a building. This is the effect of “thermal mass.” An approach the authors have used includes as a predictor the weighted average of degree-days for the past 48 hours, with the weights exponentially decreasing. Simpler approaches put multiple temperature or degree-day variables into the model, at different lags. Lagging humidity is not highly meaningful, as buildings do not store humidity in the way that they store heat.

### *Whether the Predictor Variables are Hourly or Daily*

Although the coefficients are almost always allowed to vary by hour of the day, the predictors may vary only daily. Because buildings store heat, the cooling load in a building does not respond instantaneously to the outside temperature, but depends on the temperature over recent hours. Explicit incorporation of lag weather variables can account for this effect. However, modeling load in a given hour as a function of the average temperature over the day can often work as well.

In part, this approach works because the variation in temperature over the course of the day is similar from day to day. Thus, the 10 am coefficients of daily average temperature tend to be smaller than the 4 pm coefficients. This is partly because there has been less heat build-up by 10 am and partly because the actual outdoor temperature at 10 am for a given daily average is lower than that at 4 pm.

### **Models Tested**

All the models we tested had hourly varying coefficients including an hourly intercept. That is, 24 sets of hourly coefficients were fit. If no terms but the intercept were included in the model, the model reduced to the average, by hour of the day, of the loads on the days included in the model fit.

The following models were tested.

- A. Average. No variables besides the intercept term.

$$L_{dh} = \alpha_h$$

- B. Daily temperature.

$$L_{dh} = \alpha_h + \beta_h T_d$$

- C. Hourly temperature

$$L_{dh} = \alpha_h + \beta_h T_{dh}$$

- D. Daily heating and cooling degree-days

$$L_{dh} = \alpha_h + \beta_h HDD_d + \gamma_h CDD_d$$

E. Hourly heating and cooling degree-hours

$$L_{dh} = \alpha_h + \beta_h HDH_{dh} + \gamma_h CDH_{dh}$$

F. Hourly heating and cooling degree-hours with lagged degree-hours

$$L_{dh} = \alpha_h + \beta_{1h} HDH_{dh} + \gamma_{1h} CDH_{dh} + \beta_{2h} LHDH_{dh} + \gamma_{2h} LCDH_{dh}$$

G. Hourly temperature-humidity index

$$L_{dh} = \alpha_h + \beta_h THI_{dh}$$

In the formulas above, for a given account,

$L_{dh}$  = load at hour  $h$  on day  $d$

$T_d$  = daily average temperature (average of daily minimum and maximum) on day  $d$

$HDD_d$  = heating degree-days base 65°F on day  $d$

$CDD_d$  = cooling degree-days base 65°F on day  $d$

$HDH_{dh}$  = heating degree-hours base 65°F at hour  $h$  on day  $d$

$CDH_{dh}$  = cooling degree-hours base 65°F at hour  $h$  on day  $d$

$LHDH_{dh}$  = lagged heating degree-hours base 65°F at hour  $h$  on day  $d$

$LCDH_{dh}$  = lagged cooling degree-hours base 65°F at hour  $h$  on day  $d$

$THI$  is the temperature-humidity index for hour  $h$  on day  $d$ .

$\alpha_h, \beta_h, \gamma_h$  are coefficients determined by the regression,  $h = 1, 2, \dots, 24$ .

The lag degree-day terms are based on lagged temperature calculated as

$$LT_{dh} = \frac{\sum_{k=1}^{48} T_{d,h-k} e^{-k/48}}{\sum_{k=1}^{48} e^{-k/48}},$$

where

$LT_{dh}$  is lagged hourly temperature and  $T_{dh}$  is hourly temperature and  $e$  is the natural base.

The temperature-humidity index is calculated by PJM's method as:

$$THI_{dh} = T_{dh} - .55(1 - RH_{dh}/100)(T_{dh} - 58), T_{dh} > 58,$$

$$T_{dh}, T_{dh} \leq 58.$$

where  $RH_{dh}$  is relative humidity at hour  $d$  of day  $h$ . The temperature-humidity index increases with humidity as well as with temperature and therefore may be a better predictor of load increases related to cooling.

As the definitions indicate, a fixed degree-day base was used despite the caveats indicated above under “Whether the Degree-Day Base is Fixed in Advance.” This simplification was made to allow fitting of weather models for a large number of accounts, each for several actual or simulated control periods, and using several different data selection rules. However, as described above, a model with the reference temperature fitted to each account (based on an adequate length of data) would be expected to perform somewhat better.

### *Conditional Weather Models*

Each of the weather models B through G was fit as a “conditional weather model.” That is, the weather terms were kept in the model only if certain model diagnostics indicated that these terms were meaningful and well determined.

The full set of cooling heating coefficients were either all retained or all dropped from the model. Likewise, the full set of hourly heating coefficients were either all retained or all dropped from the model.

The requirements for retaining the cooling (or heating) terms in the model were the following:

1. Although some negative coefficients were allowed, the full set of cooling (or heating) coefficients must have a positive sum. That is, the overall heating or cooling effect identified in the model must at least be physically meaningful.
2. The F-statistic for including the set of cooling (or heating) coefficients must be significant at the 0.10 significance level. That is, the data must indicate that there is a consistent and reasonably well determined relationship between load and the weather terms.

If both the heating and cooling terms were dropped from the model based on these criteria, the model reduced to a simple average by hour of the day.

### **4.1.3 Adjustment Method**

Adjustment methods tested are additive or scalar, as described in Section 2. Common adjustments are to some combination of the load in the hours between 1 and 4 hours prior to curtailment. Adjustments tested were:

- additive to load at hours h0-1 and h0-2
- scalar to load at hours h0-1 and h0-2
- additive to load at hours h0-3 and h0-4
- scalar to load at hours h0-3 and h0-4
- weather-based adjustment of all loads based on the difference or ratio of regression-estimated load using curtailment period and baseline period THI (in scalar form, the PJM approach). PJM requires a minimum of one month’s data or a full previous season. Because of limited previous season data the THI adjustment for this analysis is based on

the present season of data. This adjustment is tested only with averages, not with weather models.

In the descriptions above,  $h_0$  indicates the hour beginning the curtailment period.

## 4.2 DAYS AND HOURS TO BE EXAMINED

Each account for which data were provided was classified as either curtailed or uncurtailed. Curtailed accounts were those that were participants in a curtailment or demand-response program. Uncurtailed accounts were not program participants. Some curtailed accounts had data provided for years in which no curtailment occurred.

The time periods for which measure performance was tested depended on the data set, and whether the load data were for curtailed or uncurtailed accounts.

### 4.2.1 *Uncurtailed Accounts*

For uncurtailed accounts, certain days were set aside as test days. The baseline calculation methods were then used, with the non-test days' data as input, to calculate the load on the test days. Differences between actual and estimated load on the test days indicate the accuracy of the estimation method.

Selection of test days was as follows:

1. For data sets that included both curtailed and uncurtailed accounts on actual control days, the days when the curtailed accounts were curtailed defined the test days for uncurtailed accounts.
2. For data sets that included uncurtailed customers only, test days were selected based on extreme temperature.
3. For data sets that included some years with no curtailment for customers in a curtailment program, the test days for years with no curtailment were determined in the same way as for data sets with only uncurtailed accounts.

For each of the test days, method performance was tested for each of two 4-hour periods, one from 7 AM to 11 AM, the other from 11 AM to 3 PM.

### 4.2.2 *Curtailed Accounts*

For curtailed accounts (i.e., accounts in curtailment or demand-response programs) in years when curtailments occurred, the performance was tested during the hours of actual curtailment periods. Curtailment periods were determined from the program records of when curtailment was called, not based on whether an individual customer curtailed or not.

There is no correct baseline against which to assess method performance for these accounts on these days. The preferred method(s) was selected based on the results of the tests on uncurtailed accounts. Other methods were assessed in comparison with the preferred method.

### 4.3 DATA USED FOR TESTING

Interval load data were provided for this study from several parts of the U.S., for both curtailed and uncurtailed accounts. A total of 646 accounts were used in the analysis. For some accounts, multiple years of data were used. The total number of accounts used in the study by region, year, and curtailment category is shown in the table below.

**Table 4-1**  
**Interval Load Data Used in the Study**  
**by Region, Year, and Curtailment**

Region	Year	Total Number of Accounts	Non-Interruptible Accounts	Interruptible Accounts
California	2000	3	2	1
California	2001	1		1
Mid Atlantic	2001	33	17	16
Midwest	1998	28		28
Midwest	1999	37		37
Midwest	2000	39		39
Midwest	2001	61	11	50
Northeast	2001	15	5	10
Northwest	2000	16	10	6
Northwest	2001	16	10	6
Southeast	1992	66	24	
Southeast	1998	66		66
Southeast	1999	62		62
Southeast	2000	63		63
Southwest	1997	24	17	7

All the regions had accounts with summer curtailment data. Only the Midwest, Northwest, and Southeast had nonsummer curtailment data.

The table shows that only 2 interruptible and 2 non-interruptible accounts in the study were from the state of California, which sponsored the work. While a greater representation of California experience would have been desirable, we feel that the results developed here have broad applicability and can be useful guide for California practice. Our investigation of differences by region indicated that most differences across data sets provided appeared to be related to the types of accounts included rather than to regional variations. For this reason, we have provided results separately by weather-sensitivity and degree of load variability in an account, as well as by season.

## 4.4 ACCOUNT TYPE CLASSIFICATION

The results in the next section are displayed separately by account type. Account types are weather-sensitive and non-weather-sensitive, each with low variability and high variability.

Initially, we examined results separately by location. The key difference across locations appeared to be extreme errors that occurred for certain data sets that had very large accounts with wide swings in load. For this reason, we developed the account type classifications.

### *Weather Sensitivity*

Accounts were classified as weather-sensitive or not based on the diagnostics from a weather model fit. The weather model used was an hourly degree-hour model based on a full year of load data, with the degree-day bases estimated as part of the model. This is model “E” as defined above, except that the degree-day bases are parameters estimated by the model.

This “classification” model was used only for this purpose, and was not used as one of the tested methods. Because of the optimized selection of degree-day base, this model requires extensive processing time when applied to large numbers of accounts. In addition, its performance can be unreliable if restricted to short time periods.

The classification model diagnostics determined if the heating and/or cooling coefficients should be dropped from the model. This determination was made in the same way as described above for all the conditional weather models. As noted, these diagnostics required

1. The full set of cooling (or heating) coefficients must have a positive sum.
2. The F-statistic for including the set of cooling (or heating) coefficients must be significant at the 0.10 significance level.

If cooling coefficients were retained the account was considered weather sensitive for the summer analysis. If heating coefficients were retained the account was considered weather sensitive for the nonsummer analysis.

For all the models tested, these same diagnostic criteria were used for each model fit. Thus, an account classified as non-weather-sensitive based on the classification model might have heating and/or cooling terms included for one or more of the tested models. Likewise, an account classified as weather-sensitive by the classification model might have neither set of terms for a particular tested model.

An alternative way of classifying an account as weather sensitive or not would be in terms of the fraction of its maximum load or total energy use is for cooling and/or heating. That type of information is not typically available for an account. The weather-related fraction could be estimated from the fitted classification model. However, that calculation would depend on having a reliable estimate of the cooling and heating coefficients.

The approach taken here is to classify an account as weather-sensitive if there is a positive relationship between load and the weather drivers that is discernible above the other variations in load level. Thus, an account that in fact has a large cooling load but for which other variations swamp the variations due to weather would be classified as non-weather-sensitive for the summer analysis.

### ***Load Variability***

Accounts were also classified as high or low variability. Variability was assessed not in terms of how “flat” the load was across the day, but how much the load at a given hour varied from day to day. For loads that are more highly variable in this sense, any projection based on previous days is likely to have greater error. That is, baselines and corresponding demand reduction estimates for these accounts will be subject to greater uncertainty.

The account variability was measured in terms of the root-mean-square deviation of load in each hour from the corresponding mean for that hour. This root-mean-square deviation was calculated across all curtailment hours, and normalized by dividing by the root-mean-square load during these hours. This is a version of Theil’s U statistic, described in Section 4.5.1, applied to the load level during curtailment periods. This statistic is similar to a coefficient of variation for load during peak hours. Because we are looking at deviations relative to the mean for each hour of the day, systematic differences across hours in the day do not affect this measure of variability, but differences in load from day to day do.

Within each season and curtailment type (summer or nonsummer, curtailed or noncurtailed) the cut-off between high and low variability was set so that approximately one quarter of the accounts were in the high variability group. The cut-offs are indicated in the table below.

**Table 4-2**  
**Cut-Offs of Theil’s U for High Variability Accounts**

	Cutoff
Summer Uncurtailed	0.29
Summer Curtailed	0.40
Nonsummer Uncurtailed	0.32
Nonsummer Curtailed	0.42

The cut-offs used were in the neighborhood of 30 to 40 percent for each group. For summer curtailed accounts, for example, high variability accounts are those for which the day-to-day variation from the average for each hour is greater than 40 percent. Thus, if the average weekday 4 pm load is 600 kW, the typical day-to-day variation in the 4 pm load would be more than 240 kW.

### ***Data-Base Classification Compared with Account Identifiers***

We asked the data donors to provide an indication if possible as to whether each account was weather-sensitive or not. Some donors indicated that all accounts were industrial, therefore non-weather-sensitive. Others provided SIC or NAICs codes for each account. Some provided no information.

The table below shows the proportion of industrial and non-industrial accounts studied for each of the account types. While there is a general perception that industrial accounts are non-weather-sensitive and commercial accounts such as office are weather-sensitive, the classification based on the data put many industrial accounts in the weather-sensitive category. This finding is consistent with observations in previous work by members of the study team. However, the table also shows that the curtailed accounts were more likely to be classified as non-weather-sensitive than the uncurtailed accounts.

**Table 4-3**  
**Account Type Compared with Industrial/Nonindustrial Classification**

Analysis Account Type	Industrial/Nonindustrial Classification									
	Summer Noncurtailed			Summer Curtailed		Nonsummer Noncurtailed			Nonsummer Curtailed	
	Non-Ind.	Ind.	Unknown	Non-Ind.	Ind.	Non-Ind.	Ind.	Unknown	Non-Ind.	Ind.
Weather Sensitive Low Variability	28	25	77	19	29	12	12	46	3	11
Weather Sensitive High Variability	4	4	13		8	3	2	7		5
Non-Weather Sensitive Low Variability	14	20	17	4	41	22	23	54	2	43
Non-Weather Sensitive High Variability	1	11	14	1	25		17	14	1	14

The next tables show the numbers of accounts in each category, and their size distribution. The distributions are all quite skewed, with the mean kW greater than the 75<sup>th</sup> percentile (3<sup>rd</sup> quartile) in almost all cases. Though we attempted to get similar size accounts in the curtailed and uncurtailed groups, the tables show that the uncurtailed accounts tended to be larger.

**Table 4-4**  
**Summer Uncurtailed Account Size Distribution (kW) by Account Type Classification**

Account Type	Number of Accts	Mean	1st Quartile	Median	3rd Quartile
Weather Sensitive Low Variability	130	1,839	285	539	1,354
Weather Sensitive High Variability	21	1,132	223	412	782
Non-Weather Sensitive Low Variability	51	4,679	581	1,337	3,948
Non-Weather Sensitive High Variability	26	4,232	426	591	1,408

**Table 4-5**  
**Summer Curtailed Account Size Distribution (kW) by Account Type Classification**

Account Type	Number of Accts	Mean	1st Quartile	Median	3rd Quartile
Weather Sensitive Low Variability	48	5,374	844	1,868	4,072
Weather Sensitive High Variability	8	8,064	582	1,229	5,781
Non-Weather Sensitive Low Variability	45	12,607	1,880	4,915	9,922
Non-Weather Sensitive High Variability	26	10,689	1,142	2,819	5,933

**Table 4-6**  
**Winter Uncurtailed Account Size Distribution (kW) by Account Type Classification**

Account Type	Number of Accts	Mean	1st Quartile	Median	3rd Quartile
Weather Sensitive Low Variability	70	1,313	263	495	1,060
Weather Sensitive High Variability	12	550	103	276	639
Non-Weather Sensitive Low Variability	99	3,844	504	986	2,462
Non-Weather Sensitive High Variability	31	3,603	412	1,158	4,166

**Table 4-7**  
**Winter Curtailed Account Size Distribution (kW) by Account Type Classification**

Account Type	Number of Accounts	Mean	1st Quartile	Median	3rd Quartile
Weather Sensitive Low Variability	14	11,710	1,354	2,381	8,849
Weather Sensitive High Variability	5	2,991	1,142	1,416	1,561
Non-Weather Sensitive Low Variability	45	11,626	1,625	3,852	8,623
Non-Weather Sensitive High Variability	15	11,268	1,313	3,870	6,967

The next table shows the numbers of accounts, account-day combinations, and account-hour combinations for which baseline errors were calculated, by season, curtailment, and account type. For each account, only actual curtailment days and hours, or those defined as test periods for uncurtailed accounts, are included in the account-day and account-hour totals.

**Table 4-8  
Number of Observations in the Study**

	Weather Sensitivity	Variability	Accounts	Account-Days	Account-Day Hours
<b>Summer Uncurtailed Accounts</b>	WS	Low	130	334	1,336
	NWS	Low	51	121	484
	WS	High	21	59	236
	NWS	High	26	47	188
	<b>TOTAL</b>		<b>228</b>	<b>561</b>	<b>2,244</b>
<b>Summer Curtailed Accounts</b>	WS	Low	48	292	1,591
	NWS	Low	45	365	2,410
	WS	High	8	49	227
	NWS	High	26	192	973
	<b>TOTAL</b>		<b>127</b>	<b>898</b>	<b>5,201</b>
<b>Nonsummer Uncurtailed Accounts</b>	WS	Low	70	166	664
	NWS	Low	99	263	1,052
	WS	High	12	18	72
	NWS	High	31	76	304
	<b>TOTAL</b>		<b>212</b>	<b>523</b>	<b>2,092</b>
<b>Nonsummer Curtailed Accounts</b>	WS	Low	14	96	890
	NWS	Low	45	320	2,356
	WS	High	5	25	106
	NWS	High	15	120	459
	<b>TOTAL</b>		<b>79</b>	<b>561</b>	<b>3,811</b>
<b>All Accounts</b>			<b>646</b>	<b>2,543</b>	<b>13,348</b>
WS=Weather Sensitive, NWS=Non-Weather Sensitive					
Account/Day/Hours for Uncurtailed Accounts represent only one of the two simulated four hour control periods.					

The number of accounts is the number of distinct customers for which the methods were tested. To a certain extent, method performance will be a characteristic of the customer, related to the customer's operating practices and associated load patterns. The number of account-days is the number of distinct combinations of customers and control events. Finally, the number of account-hours is the number of individual observations of method error in the analysis.

## 4.5 PERFORMANCE MEASURES

The tests were run for several alternative methods on several different data sets for several hours on several days. Developing meaningful measures of method performance is essential to provide a basis for conclusions. Performance measures provided are somewhat different for uncurtailed and curtailed accounts.

### 4.5.1 Performance Measures for Uncurtailed Test Periods

#### Key Calculations

For each account used as an uncurtailed test case, the estimated load for each hour and several measures of error were calculated and reviewed for each method. Hours included in the calculations were actual curtailment hours for curtailed accounts, and test period or “simulated curtailment” hours for uncurtailed accounts. The key calculations used and displayed in this report are shown in Table 4-9.

**Table 4-9**  
**Key Calculations for Each Estimation Method and Account**

Description	Formula
estimated load	$L_{jdh}^{\wedge}$ = estimated load for account $j$ on day $d$ at hour $h$
hourly error	$e_{jdh} = L_{jdh}^{\wedge} - L_{jdh}$
relative hourly error	$r_{jdh} = e_{jdh}/L_{jdh}$
account root-mean-square hourly error	$RMSEH_j = \sqrt{[\sum_{d=1}^{n_j} \sum_{h=1}^{n_{jd}} e_{jdh}^2 / \sum_{d=1}^{n_j} n_{jd}]}$
account root-mean-square hourly load	$RMSLH_j = \sqrt{[\sum_{d=1}^{n_j} \sum_{h=1}^{n_{jd}} L_{jdh}^2 / \sum_{d=1}^{n_j} n_{jd}]}$
account Theil's U hourly, or relative root-mean-square hourly error	$TUH_j = RMSEH_j / RMSLH_j$
Theil's U daily, or relative root-mean-square daily error	$TUD_j = RMSED_j / RMSLD_j$
account average error	$e_{j..} = \sum_{d=1}^{n_j} \sum_{h=1}^{n_{jd}} e_{jdh} / \sum_{d=1}^{n_j} n_{jd}$
relative account error	$r_{j..} = e_{j..}/L_{j..}$

In the equations above,

$L_{jdh}$  = actual load for account  $j$  on day  $d$  at hour  $h$ .

$n_{jd}$  = number of hours in curtailment period for account  $j$  on day  $d$

$n_j$  = number of test days for account  $j$ .

### ***Key Indicators of Method Accuracy***

The goal of the performance tests is to assess the accuracy of the various baseline measures tested. As discussed in Section 3.3, accuracy has two components, bias and variability. Bias is the systematic tendency to over- or under-state baselines and corresponding load reductions. Variability is how widely the baseline is likely to vary from its typical or expected level.

#### **Bias**

As a key measure of bias, we focus on the median relative hourly error. Because accounts in this study are of widely varying sizes, when looking at the range of errors across accounts we need to normalize them. Thus, the error for each hour for each account is expressed as a fraction of the actual load for that hour and account. If the median, across all accounts and curtailment hours, of these relative hourly errors is positive, then more often than not the baseline is overstated, and the magnitude of demand response is overstated. If the median of the relative hourly errors is negative, then more often than not the baseline is understated and the magnitude of demand response is understated.

#### **Overall Error Magnitude**

As a key measure of the total magnitude of error, we consider Theil's U statistic for each account. This statistic is a "relative root-mean-square error." It is calculated for each account as the ratio of the root-mean-square error to the root-mean-square load.

The root-mean-square error is like a standard deviation, and represents the typical error magnitude for the account. This root-mean-square error reflects both systematic error, or bias, and the level of variability around the typical error.

The root-mean-square load is a corresponding "typical" load level. Normalizing the root-mean-square error by the root-mean-square load is something like calculating a correlation coefficient. However, the U statistic may be greater than 1, since errors can be greater than the loads they estimate.

The denominator of the U statistic will be weighted toward larger loads. That is, for a given account, relative errors at higher-load hours will tend to count more heavily than those at lower-load hours.

Theil's U statistic calculated for a given account indicates the typical relative error magnitude for that account. The distribution of this statistic across accounts indicates the range of performance. We look at this distribution in terms of both the median and an extreme, the 95<sup>th</sup> percentile. The median Theil's U indicates the typical relative error magnitude for a typical account. The 95<sup>th</sup> percentile indicates typical performance for the accounts where the performance is generally worse. Because the U statistic for each account is normalized by the typical account load, the distributions of U across accounts treat large and small accounts equally.

Descriptive statistics and graphical displays of distributions of the error measures are presented in Section 5.

#### 4.5.2 Performance Measures for Curtailment Days

For the curtailed load during curtailment periods, an approximate error  $e_{jdh}^{\sim}$  was calculated for each method as the difference between the load estimate from that method and the preferred method. That is,

$$e_{jdh}^{\sim} = \hat{L}_{jdh} - L_{jdh}^*,$$

where

$L_{jdh}^*$  = estimated load for account  $j$  on day  $d$  and hour  $h$  using the preferred method.

This calculation was performed only for day-hour combinations  $dh$  included in called curtailment periods for account  $j$ . All of the error measures used for the uncurtailed tests were then calculated for the curtailment periods.

In addition, for the curtailment periods the load reduction was calculated for the preferred method and for each other tested method:

$$D_{jdh} = L_{jdh}^* - L_{jdh}$$

$$\hat{D}_{jdh} = \hat{L}_{jdh} - L_{jdh}.$$

The error in the demand response is the same as the error in the load estimate:

$$\hat{D}_{jdh} - D_{jdh} = (\hat{L}_{jdh} - L_{jdh}) - (L_{jdh}^* - L_{jdh}) = \hat{L}_{jdh} - L_{jdh}^* = e_{jdh}^{\sim}.$$

However, relative errors are of interest not just relative to the load level but also relative to the demand response  $D$ . Two types of relative errors were calculated for the curtailed accounts. The first is the same as for uncurtailed accounts, expressing the hourly error  $e_{jdh}^{\sim}$  as a fraction of the hypothetical load in the absence of curtailment (based on the preferred method). The second type of relative error is the hourly error as a fraction of the curtailment amount determined using the preferred method.

## 5.1 INTRODUCTION

This section presents the results of the tests described in Section 4. The purpose of the tests is to examine the accuracy of baselines determined by various methods, under a wide range of conditions. The baseline methods tested and the data sets on which they were tested are described in Section 4.

For each method tested, the key measures we use to examine the method performance are the following.

**Bias: Median relative hourly error**, across all accounts, test days, and hours.

The relative hourly error  $r_{jdh}$  is calculated for each account-day-hour combination. The median of all these relative hourly errors is the key indicator of method bias. Median relative hourly error greater than 0 indicates a systematic tendency to overstate baselines and load reductions. Median relative hourly error less than 0 indicates a systematic tendency to understate baselines and load reductions.

**Typical error magnitude: Median U statistic**, across all accounts.

This measure reflects both bias and variability. For each method, for each account, Theil's U is calculated across all test days and hours. The U statistic is similar to a coefficient of variation. It indicates the typical error magnitude relative to a typical load level. The median of U across accounts indicates the typical relative error for a typical account.

**Error magnitude for extreme accounts: 95<sup>th</sup> percentile U statistic**, across all accounts.

The extremes of Theil's U indicate how far off the baseline tends to be for the less well-behaved accounts. The focus is not on individual problematic hours, but on accounts for which the method error tends to be high across hours.

For curtailed accounts, the same types of error measures are calculated as for noncurtailed accounts, except that each of these is calculated for errors relative to estimated load and also for errors relative to estimated curtailment amounts. As described in Section 4, the errors calculated for curtailed accounts are the difference between the estimate for a particular method and that of the "best" method, a full season weather model. Thus, these errors are not a perfect measure of performance, and are not entirely comparable to the error measures for noncurtailed accounts. They are nonetheless informative.

## 5.2 A FIRST LOOK AT THE COMPARISONS

Before considering these performance measures across the full range of methods explored, we illustrate the types of comparisons being made. For purposes of this illustration, we consider two combinations of estimation method and data selection rule:

- A1 is the average, by hour of the day, of the past 10 uncurtailed business days.
- D8 is a regression model using a full season of data, and daily heating and/or cooling degree-days as the predictor variables for each hour. Like all the weather models tested, it is a “conditional” model, with heating or cooling degree-days included in the model for a particular account only if the diagnostic screens are passed.

Formal specifications of these methods are given in Section 4.

For each of these combinations of estimation method and data selection criteria, each of the possible adjustments was applied.

- Additive adjustment to hours h0–1 to h0–2
- Scalar adjustment to hours h0–1 to h0–2
- Additive adjustment to hours h0–3 to h0–4
- Scalar adjustment to hours h0–3 to h0–4
- Additive adjustment based on the THI regression model using the previous season’s data.
- Scalar adjustment based on the THI regression model using the previous season’s data.

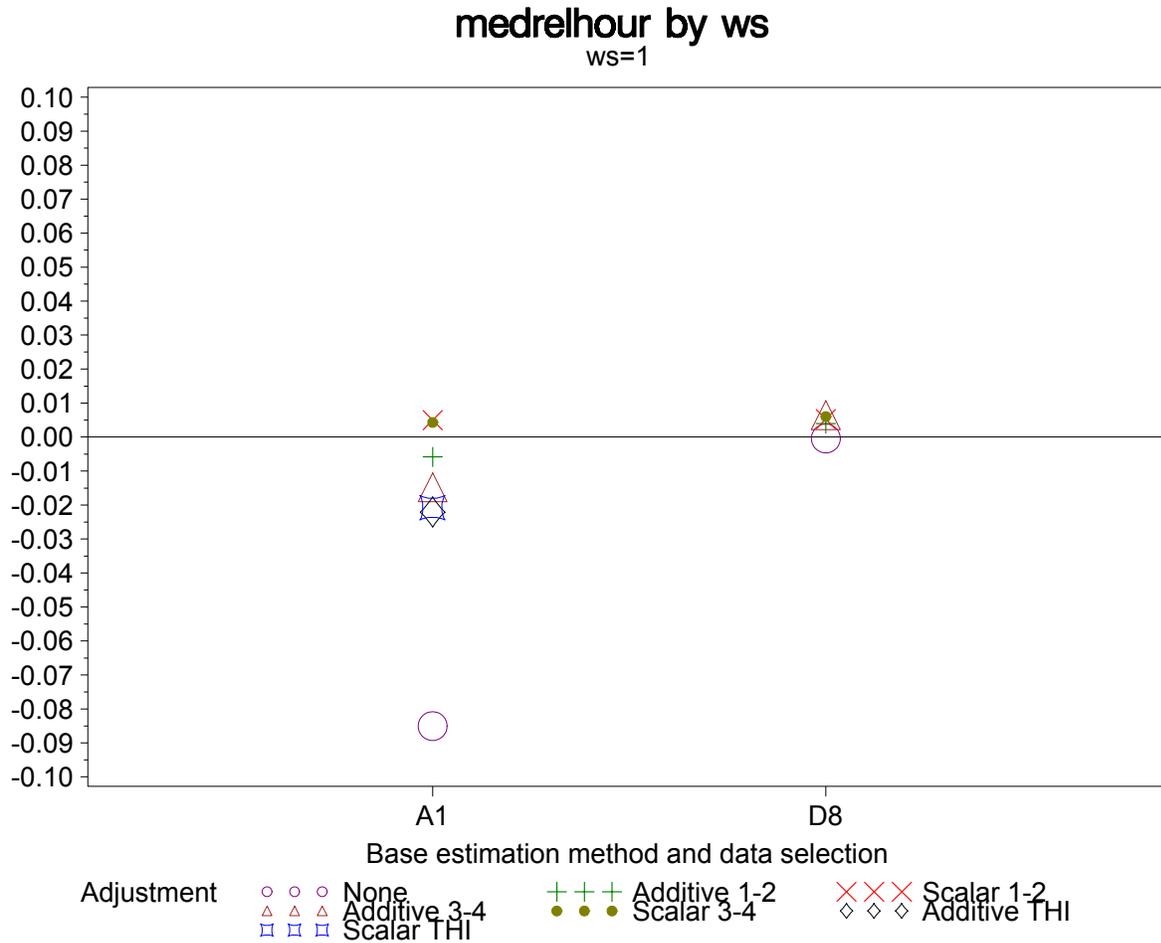
These adjustments are described and illustrated in Section 2.

### 5.2.1 Looking at Bias

We focus on the median relative hourly error as the key measure of bias, that is, systematic tendency to over- or understate load. The median rather than mean relative hourly error is used because relative errors can be quite large if the true load is small, and these occasional explosive values can distort the mean without indicating typical behavior.

Figure 5-1 shows the median relative hourly error for the average A1 together with each of the adjustments. The results for the different adjustments are plotted in a vertical line, and indicated with different symbols. The figure shows that the unadjusted method A1 (circle) has a median relative hourly error around –8 percent. That is, the simple average of the last 10 uncurtailed business days tends to understate the baseline by about 8 percent.

**Figure 5-1**  
**Median Relative Hourly Error**  
**Simple 10-Day Average and Full-Season Degree-Day Regression**  
**Summer Uncurtailed Weather-Sensitive Low-Variability Accounts**



With the additive adjustment to the last two hours before curtailment ('+') the median relative error is still negative, but only about half a percent. With an additive adjustment to the third and fourth hour before (triangle) yields a relative error of -1.5 percent. Using the more complicated THI adjustment in additive (diamond) or scalar (square) gives about -2 percent. Scalar adjustment to the last two hours ('x') or to the third and fourth hour (black dot) before gives a slightly positive bias.

Overall, then, any of the adjustments seem to reduce substantially the negative bias of using a simple average of the past 10 days. That is, use of these adjustments mitigates the average's understatement of baselines and demand reductions for weather-sensitive accounts.

Also shown in the figure is the same set of results for method D8, the full-season daily degree-day model. The figure shows that the unadjusted weather model ('o') has only slight negative bias, -0.5 percent. With any of the adjustments, the model has a slight positive bias, about +0.5

percent. The THI adjustments were not tested with the regression models, on the assumption that the models themselves should capture whatever effect is captured in the THI adjustment. Thus, for weather-sensitive accounts, use of the full-season model substantially eliminates any systematic tendency to over- or under-state the baseline.

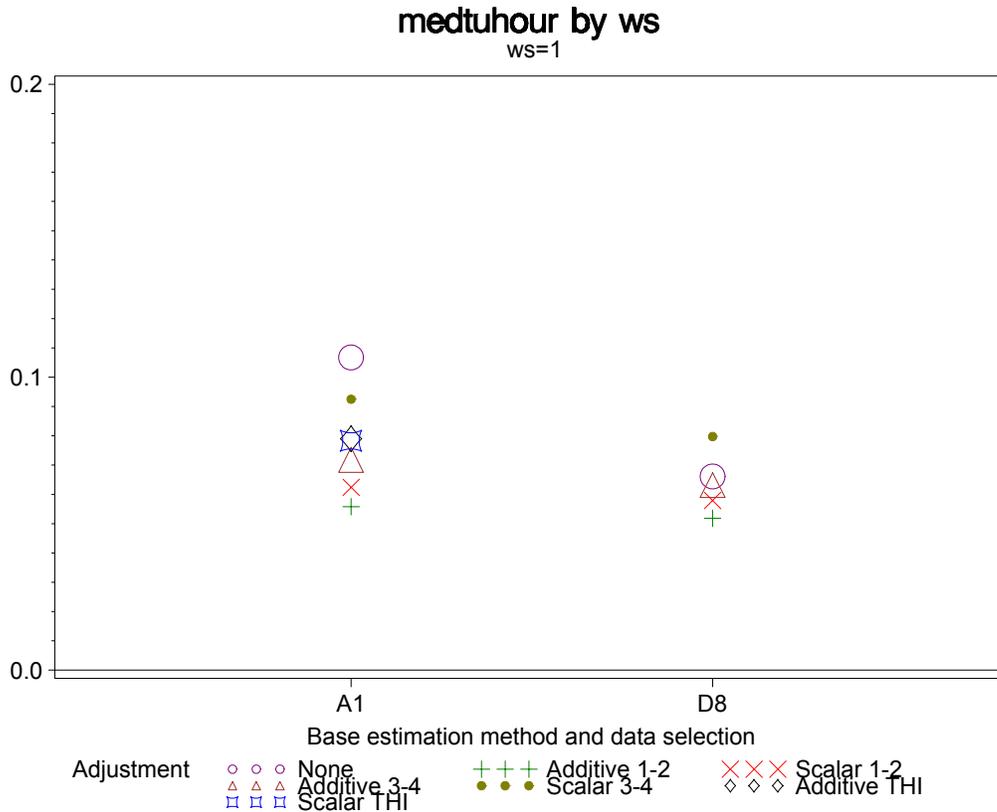
### **5.2.2 Looking at Overall Error Magnitude**

The key indicator of error magnitude we use is the median, across all accounts, of Theil's U statistic for the account. Theil's U is the root-mean-square error, relative to the root-mean-square load. Thus, high relative errors for hours when the load is small contribute little to U. Relative errors at hours when the load is high count most heavily. The median of Theil's U across accounts indicates what the typical hourly error is for a typical account. Theil's U reflects both systematic error and variability.

Figure 5-2 shows the medians of Theil's U for the same cases whose median relative errors are plotted in Figure 5-1. For the unadjusted average A1, the median account U is about 11 percent. All of the adjustment methods reduce U. The lowest U for method A1 is with the additive and scalar adjustments to hours -1 to -2, at 5.4 and 5.8 percent, respectively.

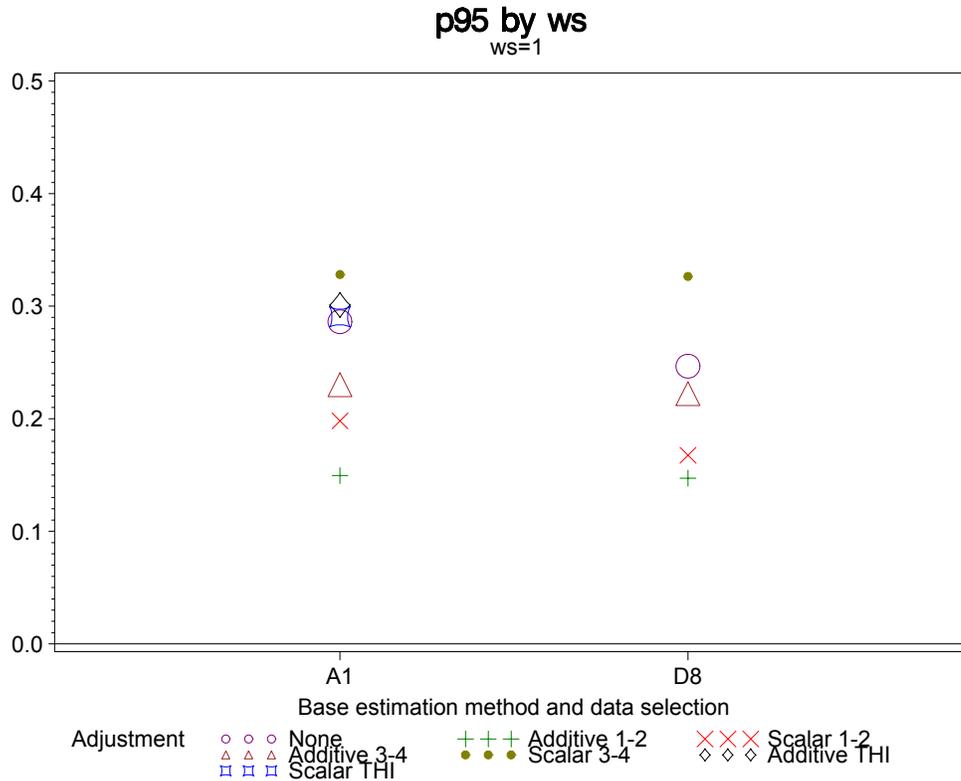
For the weather model D8, the unadjusted method has Theil's U of 6.2 percent, only slightly worse than the best adjusted average. The additive and scalar adjustments to the last two hours are slightly better, at 4.9 and 5.7 percent, respectively. The scalar adjustment to hours -3 to -4 is somewhat worse, at 7.5 percent.

**Figure 5-2**  
**Median Account Theil's U**  
**Simple 10-Day Average and Full-Season Degree-Day Regression**  
**Summer Uncurtailed Weather-Sensitive Low-Variability Accounts**



In addition to looking at the median of Theil's U, we also looked at the 95<sup>th</sup> percentile. This measure indicates how bad the errors tend to be for the less predictable accounts. Figure 5-3 shows these results for the same cases as in Figures 5-1 and 5-2. Because we are looking at the extremes, the scale of the plot is changed to accommodate the values.

**Figure 5-3**  
**95<sup>th</sup> Percentile Account Theil's U**  
**Simple 10-Day Average and Full-Season Degree-Day Regression**  
**Summer Uncurtailed Weather-Sensitive Low-Variability Accounts**



The figure shows that the extreme cases show typical error in the range of 15 to 35 percent, depending on the adjustment method and estimation method. The 95<sup>th</sup> percentiles of Theil's U show much more spread across adjustment methods than do the medians. Nevertheless, some of the same patterns observed for the medians still hold:

- Without adjustment, the full-season weather model performs better than the 10-day average.
- For both average and regression, the additive adjustment to the last two hours has smallest errors, and the scalar adjustment the next smallest.
- With the additive adjustment to the last two hours, the simple average method is nearly as good at estimating the base load as the weather model.

However, the difference between the better- and worse-performing adjustments is more pronounced for the extreme cases than for the medians.

### 5.2.3 Preliminary Indications

Based on these illustrative results, some preliminary indications are the following:

1. A relatively simple adjustment to a simple method may yield a method that performs nearly as well as a more complicated weather model.
2. Even for a complicated weather model, there may still be some bias if no adjustment is made.
3. The weather model appears to be less sensitive to the type of adjustment made than is the simple average.
4. The additive adjustment to the two hours before curtailment appears to perform best in terms of both bias and variability.
5. In general, the patterns in the 95<sup>th</sup> percentile are qualitatively similar to those for the median, though the magnitudes are greater, and the corresponding difference between the better and worse methods is greater.

As will be seen, these patterns are borne out in other comparisons. While we might not have anticipated all these results, they do make sense.

Some of the reasons that adjustment to the hours just before curtailment could improve baseline accuracy were discussed conceptually in Section 2. These hours are most reflective of actual operations just prior to curtailment. Thus, to the extent operations are different from those in the baseline days, the adjustment to the pre-curtailment hours captures some of that difference. These hours also reflect the actual weather on that day, at least up to the time of the curtailment. As a result, this adjustment can also serve to correct for weather differences, to an extent.

It is not surprising that adjustment to the two hours just before curtailment would perform somewhat better than the adjustment to the third and fourth hour before. The later hours are more likely to be past the morning ramp-up, reflect more of the weather and heat build-up for the day, and be indicative of operations for the main part of the day.

Not necessarily expected was the finding that the additive adjustment does slightly better than the scalar adjustment overall. This result appears to be due to the scalar adjustment's becoming very large if the baseline load was very low compared to the actual during the adjustment hours.

Also not necessarily expected was the finding that the THI adjustments tend to be worse in terms of both bias and overall error magnitude than the adjustment to recent hours. This result suggests there are important curtailment-day differences apart from weather, which are captured in the other adjustments. The THI adjustment has the advantage of being "ungamable," because it does not utilize recent loads. Its disadvantage is that it is therefore not informed by differences in these loads when they might be meaningful indicators of operations on the curtailment day.

Particularly intriguing is the performance of the full-season weather model with additive adjustment to the last two hours. The unadjusted model has near zero bias, but the adjustment noticeably reduces the variability of the method, bringing the error magnitude down from 6.2 percent to 4.9 percent in terms of median account U, and from 25 percent to 15 percent for the extreme (95<sup>th</sup> percentile) accounts.

While it might have been expected that the weather model would not benefit from the simple adjustments, this result does make sense. It is also consistent with the finding that the weather-based THI adjustments don't do as well as the adjustment to the last two hours. That is, there are non-weather effects that are difficult to model explicitly, but that are reflected in the earlier load on the day being predicted.

Another way to say this is that the prior hours capture some of the random effects that are left unexplained by the weather model. Load forecasters often include the most recent data available as explicit terms in prediction models. Rather than including the adjustment as an extra tweak on the weather model, the load in the hours prior to curtailment could be included as predictors in the model. Model diagnostics could then determine whether to retain these terms, while the model coefficients would determine the relative weight given to the prior data and the current-day information.

### 5.3 A BRIEF GUIDE TO THE DISPLAYS

In the remainder of this chapter, we present the same types of figures as Figures 5-1 through 5-3. However, in each figure we include all tested combinations of estimation method, data selection criteria, and adjustment.

#### *Combinations Tested*

In the displays, each combination of an estimation method and data selection criteria is indicated by a letter code for the method together with a number code for the selection criteria. Brief definitions of the codes are indicated in the table below. These method components are described more fully in Section 4.

**Table 5-1**  
**Codes for Estimation Methods and Data Selection Criteria**

Method Code	Estimation Method	Selection Code	Data Selection Rule
A	Average	1	Previous 10
B	Daily Temperature	2	Previous 11
C	Hourly Temperature	3	Previous 10 starting d0-2
D	Daily Degree-Day	4	Previous 20
E	Hourly Degree-Day	5	Previous 10 and Next 10
F	Lagged Hourly Degree-Day	6	High 10 of 11
G	THI	7	High 5 of 10, starting d0-2
		8	Full season
		9	Full previous season

Each estimation method and data selection criteria was tested with each of the possible adjustments listed in Section 4 and displayed in Figures 5-1 through 5-3. The exception is that the THI adjustments were applied only to averages, not to weather models.

The component methods selected were designed to include the main ISO methods in use. The codes corresponding to each of these methods are indicated in the table below. Also indicated are ways the data selection rule tested differs from the details of the ISO method.

**Table 5-2  
Correspondence of Tested Methods to ISO Baseline Methods**

ISO	ISO Baseline Methodology					Closest Method Tested							Differences between Tested method and ISO
	Data Selection			Estimation Method	Adjustment	Estimation Selection Code	Shorthand Descriptions			Full Data Selection Description			
	Initial	Final	Exclusions				Estimation Method	Selection Method	Adjustment	Initial	Final	Exclusions	
California #1	Previous 10 business days beginning on d0-1	Same	Control days, with replacement	Average	None	A1	Average	Last 10	None	Previous 10 business days beginning on d0-1	Same	Control days, with replacement	
California #2	Previous 11 business days beginning on d0-1	Days with top 10 average loads for control period	Control days, with replacement	Average	None	A2	Average	High 10 of 11	None	Previous 11 business days beginning on d0-1	Days with top 10 average loads for control period	Control days, with replacement	
New England	Previous 10 business days beginning on d0-1	Same	Control days and extreme load days, without replacement (min. 7 days)	Average	Additive 1-2	A1	Average	Last 10	Additive 1-2	Previous 10 business days beginning on d0-1	Same	Control days, with replacement	Control days are replaced with replacement (always ten days). No extreme load day exclusions.
New York	Previous 10 business days beginning on d0-2	Days with top 5 average loads for control period	Control days and extreme load days, with replacement	Average	Optional Scalar 3-4 (limited to .8 to 1.2)	A7	Average	High 5 of 10	Scalar 3-4	Previous 10 business days beginning on d0-2	Days with top 5 average loads for control period	Control days, with replacement	No extreme load day exclusions. Unbounded adjustment.
PJM	Previous 10 business days beginning on d0-2	Days with top 5 average loads for control period	Control days and extreme load days, with replacement	Average	Optional Scalar THI adjustment	A7	Average	High 5 of 10	Scalar THI	Previous 10 business days beginning on d0-2	Days with top 5 average loads for control period	Control days, with replacement	No extreme load day exclusions. THI adjustment parameters are estimated on full same season rather than previous season or partial same season.

**Organization of the Displays**

Each display consists of a plot similar to one of Figures 5-1 through 5-3. Combinations of estimation method and data selection criteria are indicated by horizontal position in the graph. The adjustment method is indicated by the plotting symbol.

**Bias Plots**

Each plotted point is the median relative hourly error for a different combination of method features. From left to right, different combinations of estimation method and data selection criteria are shown. For each of these combinations, the median relative hourly error is plotted for each of the adjustment methods tested.

**Typical Error Magnitude Plots**

The median of the U statistic across accounts is plotted for each method. The different methods are displayed in the same way as for the median relative hourly error.

**Error Magnitude for Extreme Accounts**

This display is the same as the median account U, except that the 95<sup>th</sup> percentile is plotted instead of the median.

A different set of figures is presented for each combination of

- curtailment classification (curtailed or uncurtailed accounts)
- account type (weather-sensitive or non-weather-sensitive accounts, with high or low variability)
- season (summer or non summer).

Thus, a total of 16 sets of the three figures are presented. We begin with summer uncurtailed accounts. We first look at weather-sensitive accounts, low and then high variability. We then examine non-weather-sensitive accounts. This same sequence is then followed for non summer uncurtailed, summer curtailed, and non summer uncurtailed.

## 5.4 TEST RESULTS FOR UNCURTAILED ACCOUNTS, SUMMER

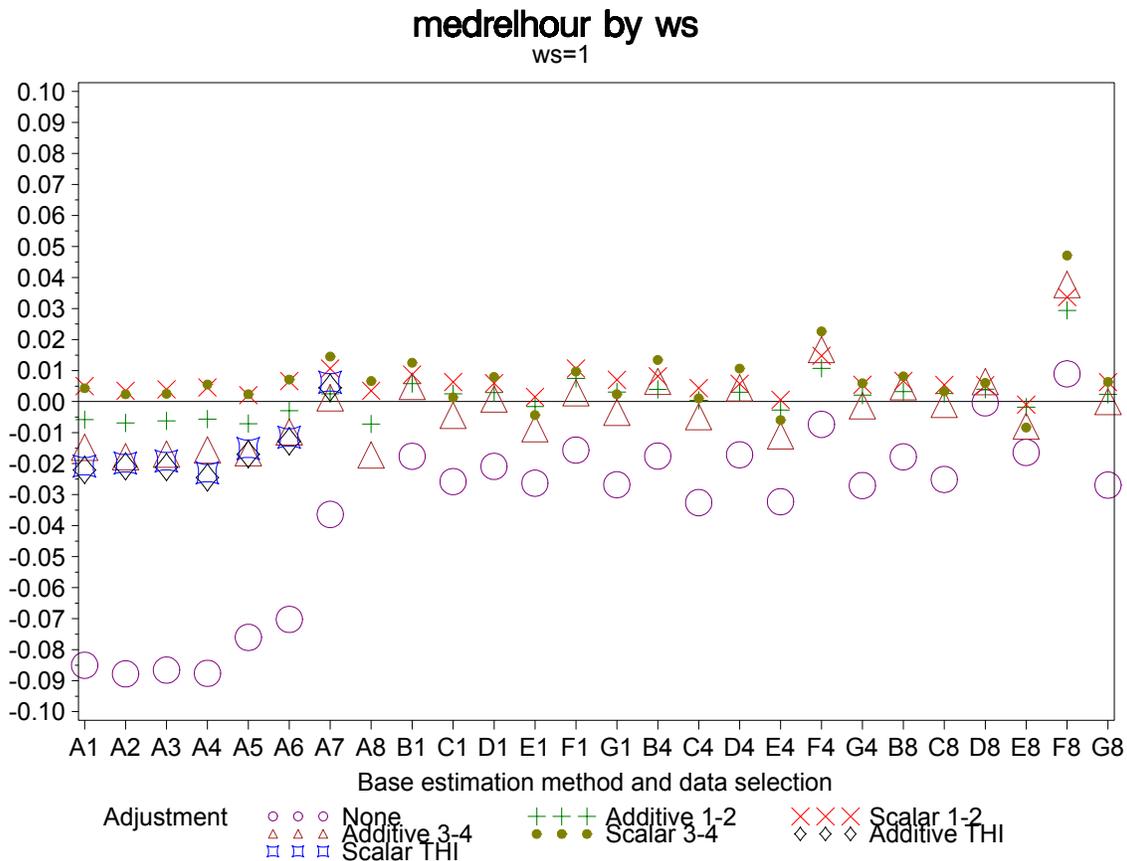
We begin with the uncurtailed accounts, summer season. For uncurtailed accounts, the actual load during the test period is known. Thus, the estimation methods can be tested against actual loads. Method performance based on these cases can be used to select the best method. For the curtailed accounts, performance of each method can then be assessed relative to “truth” as defined by this best method. We focus first on the summer because the majority of load reduction programs are aimed at reducing summer peaks.

### 5.4.1 *Weather-Sensitive Accounts*

#### *Low-Variability Accounts*

Figure 5-4 shows the median relative hourly errors for all tested methods, for weather-sensitive low-variability accounts. Starting from the left, the first group of methods shown are the various averages, based on different data selection criteria. Next are the different weather models, all using the last 10 uncurtailed business days. Next is the same sequence of models, all using the last 20 uncurtailed business days. Finally, the same sequence of models use a full season of data. For each estimation method and data selection criteria, the results with the different adjustments are plotted using the same symbols as in Figures 5-1 through 5-3.

**Figure 5-4**  
**Median Relative Hourly Error**  
**Summer Uncurtailed Weather-Sensitive Low-Variability Accounts**



### Bias

While there are a large number of factors being compared in the figure, some patterns can be observed.

1. With no adjustment, the weather models all have lower magnitude bias than any of the averages. However, the “High 5 of 10” method (A7, highest 5 of the last 10 uncurtailed business days) is nearly as good.
2. Except for the High 5 of 10 method, the averages all have much worse bias (-6 to -10 percent) than the weather models (on the order of -3 percent or smaller).
3. With no adjustment, almost all the weather models still have some negative bias. The one exception is the full-season lag model (F8). This method becomes slightly positively biased when adjustments are incorporated.
4. With adjustment to the hours h0-1 and h0-2, all the methods have bias within  $\pm 1$  percent, except the full-season lag model.
5. The adjustment to hours h0-3 to h0-4 are slightly worse than to the hours h0-1 to h0-2, and, the THI adjustments a little worse than these. The exception is the High 5 of 10

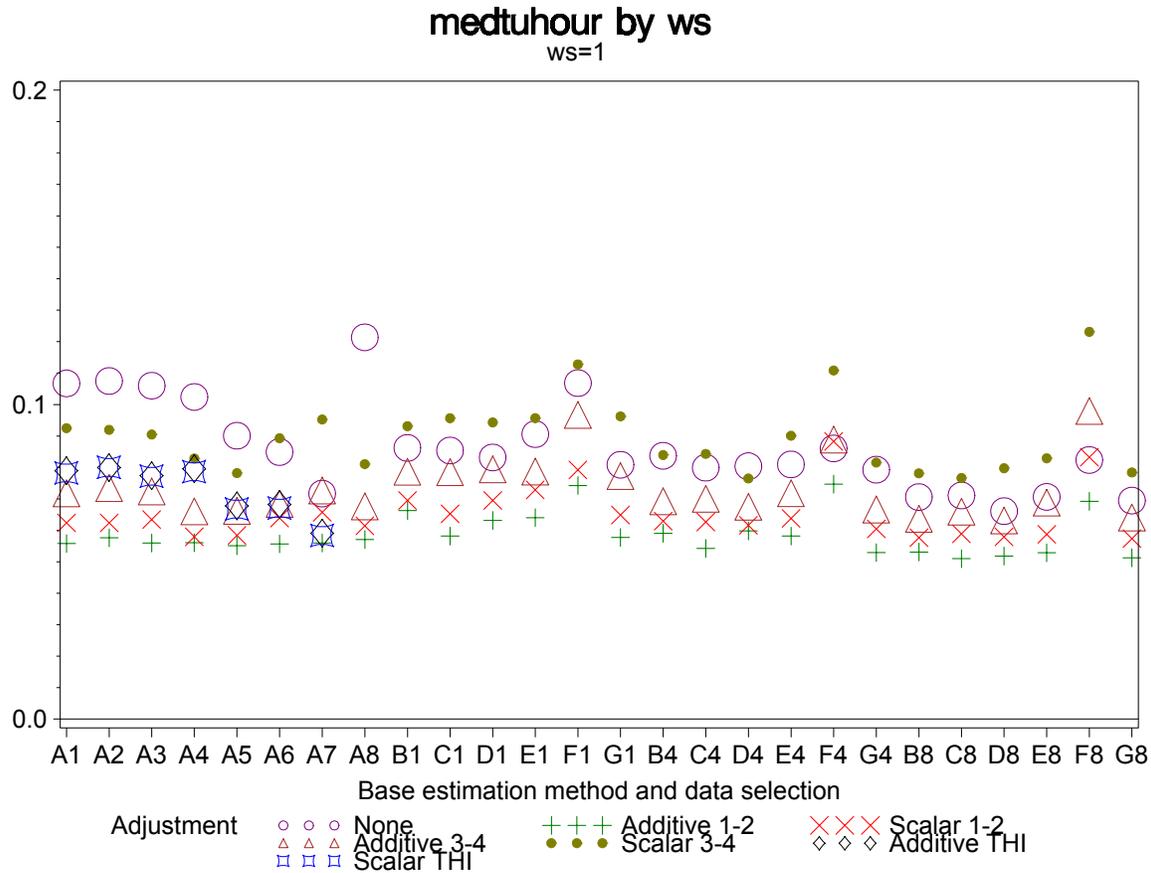
method, where the additive adjustment to hours  $h_0-1$  to  $h_0-2$  and the additive and scalar THI adjustments all give near 0 bias.

### Typical Error Magnitude

Figure 5-5 shows the median account U for the same methods and accounts. Observations from this figure are the following.

1. For each estimation-selection method, the additive adjustment to the last 2 hours has the smallest median Theil's U. That is, this combination tends to yield the smallest magnitude relative error for each account. Next best is the scalar adjustment to the last 2 hours.
2. With this additive adjustment, there is little difference among the averages A1 through A8.
3. For any adjustment and any selection rule, there is little difference among the different weather models B through G, except that the lag models F tend to have higher median Theil's U. That is, the inclusion of the lag terms in the models tends to increase the model variance.
4. With the best adjustment a1, the 20-day weather models (other than the lag F) have slightly lower error magnitude than the 10-day averages, and the full-season models still lower. However, the 10-day weather models tend to have slightly higher errors than the averages.
5. For the unadjusted methods, the averages are generally worse than the weather models. The exceptions are that the High 5 method is better than the 10- and 20-day regressions, and the lag models are as bad as some of the averages.
6. For all the weather models, the scalar adjustment to hours  $h_0-3$  to  $h_0-4$  has worse U than the unadjusted model.

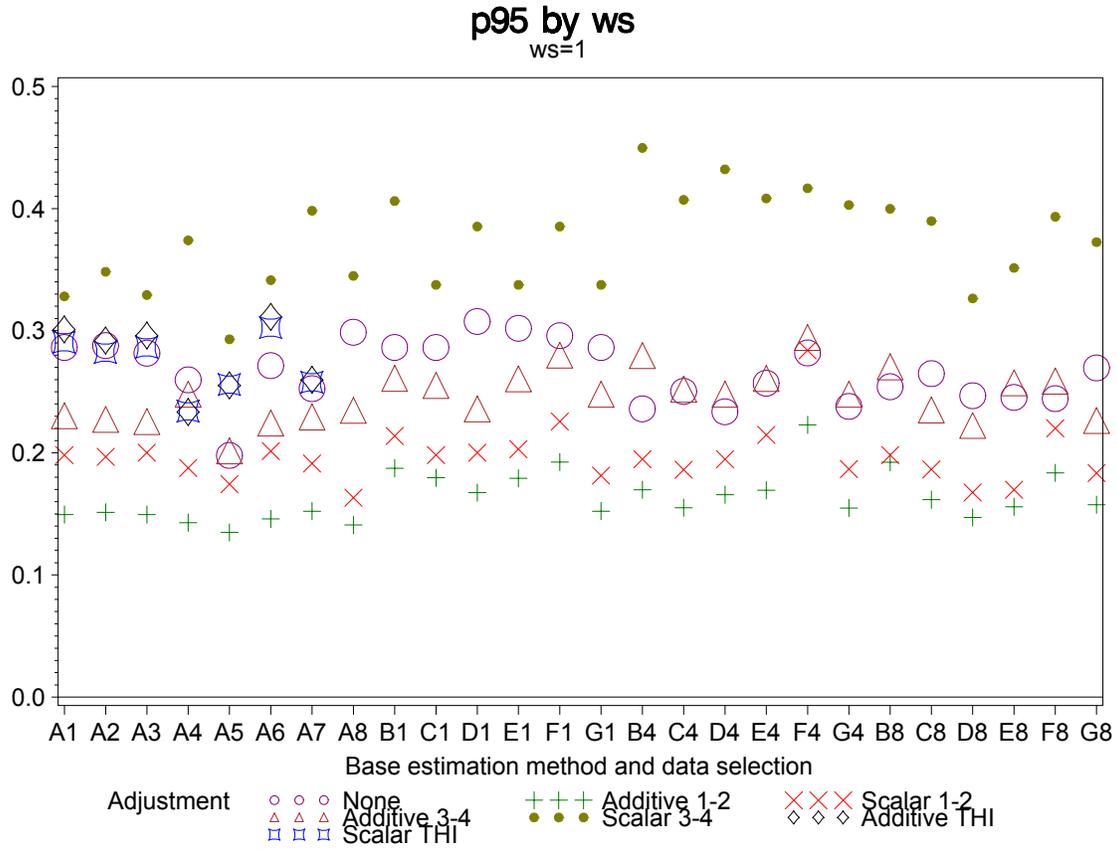
**Figure 5-5**  
**Median Account Theil's U**  
**Simple 10-Day Average and Full-Season Degree-Day Regression**  
**Summer Uncurtailed Weather-Sensitive Low-Variability Accounts**



**Error Magnitude for Extreme Accounts**

Figure 5-6 shows the 95<sup>th</sup> percentile of Theil's U for the same cases. For these extreme error magnitudes, the weather models are not dramatically better than the averages, even without adjustment. The additive adjustment to the two hours prior to curtailment performs best in almost all cases. The improvement between the unadjusted and this adjustment is substantial even for the weather models, from around 30 percent down to 15 to 20 percent typical relative error. Thus, while the adjustment choice seems to make little difference in performance for the typical account, it does make a difference to how bad the worse accounts get.

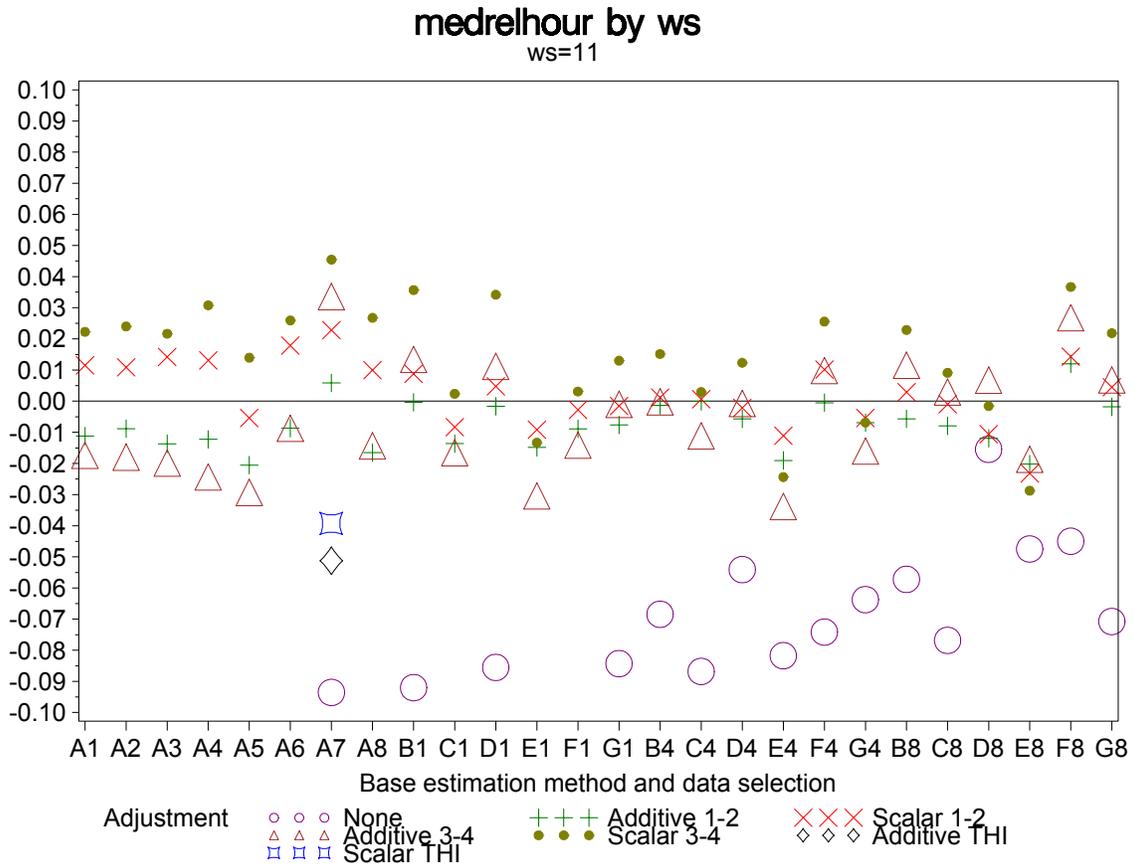
**Figure 5-6**  
**95<sup>th</sup> Percentile Account Theil's U**  
**Simple 10-Day Average and Full-Season Degree-Day Regression**  
**Summer Uncurtailed Weather-Sensitive Low-Variability Accounts**



**High-Variability Accounts**

Figures 5-7 through 5-9 show the same plots for the weather-sensitive accounts with high variability. Note that a wider scale is used for the Theil's U plots than for the corresponding plots for the low-variability accounts.

**Figure 5-7**  
**Median Relative Hourly Error**  
**Summer Uncurtailed Weather-Sensitive High-Variability Accounts**



**Figure 5-8**  
**Median Account Theil's U**  
**Summer Uncurtailed Weather-Sensitive High-Variability Accounts**

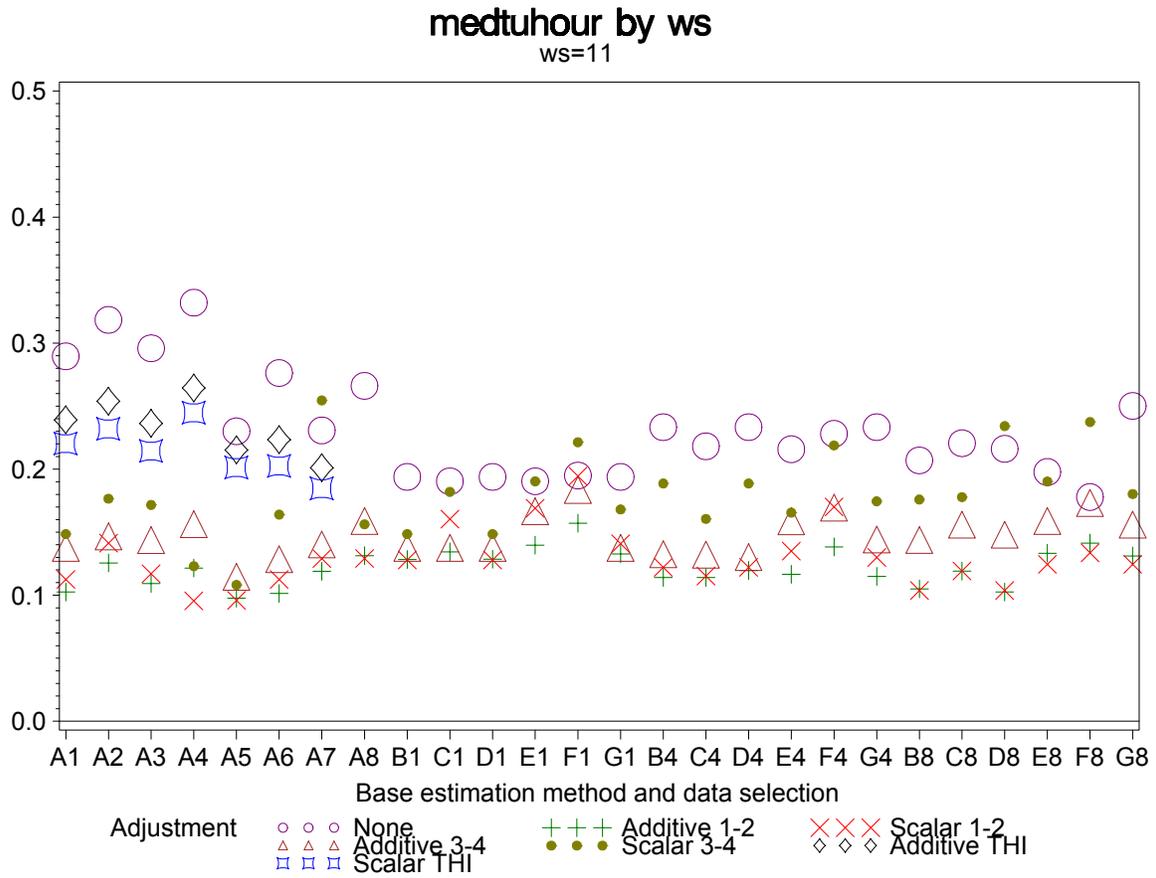
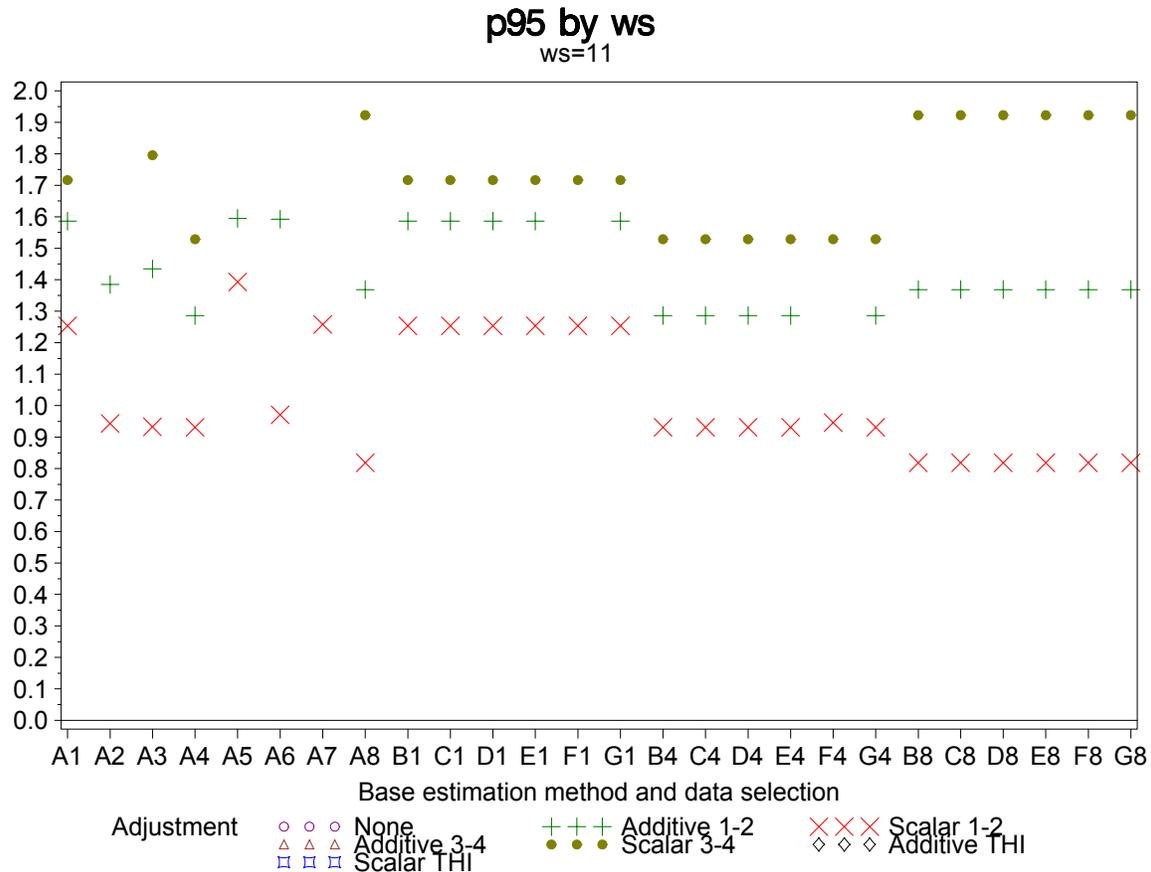


Figure 5-9  
 95<sup>th</sup> Percentile Account Theil's U  
 Summer Uncurtailed Weather-Sensitive High-Variability Accounts



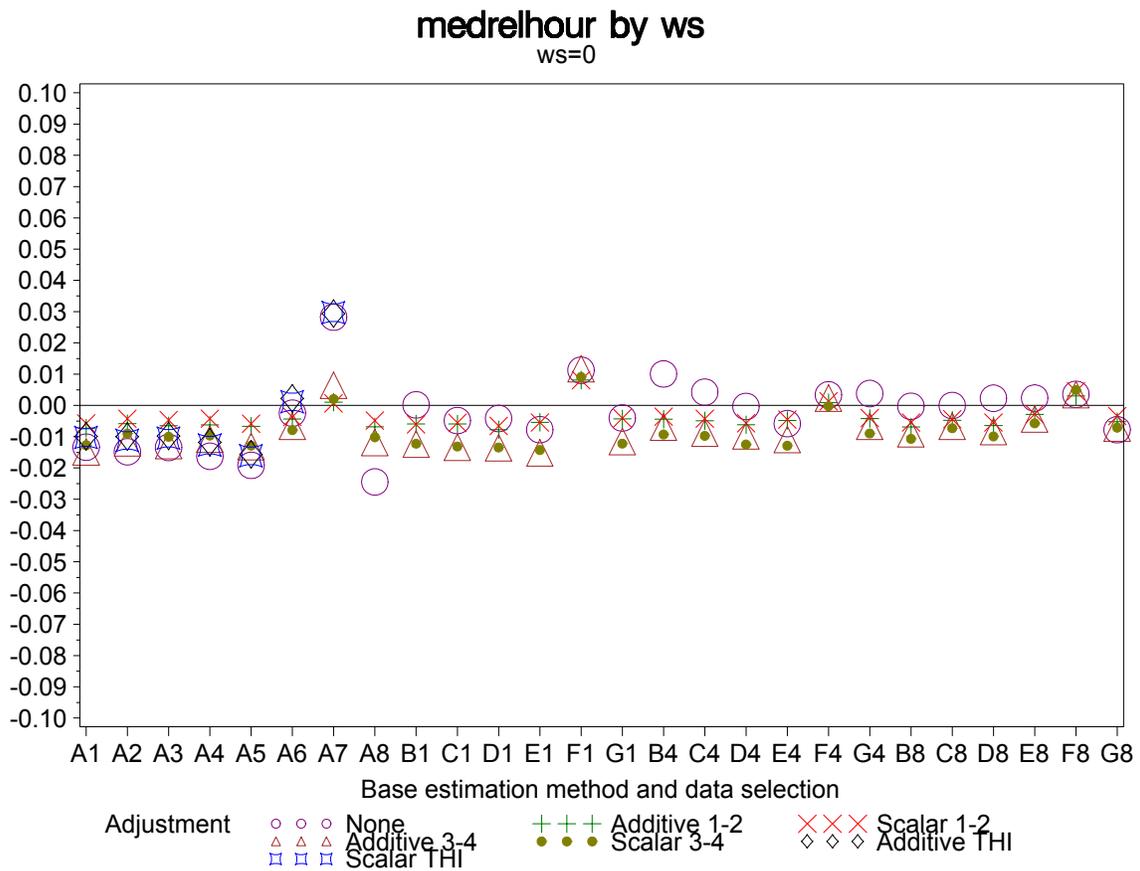
Not surprisingly, these plots show that accounts with high variability are generally more difficult to predict accurately, even when they are weather-sensitive. Median relative errors are farther from zero for all methods, and are more than 10 percent off for the unadjusted averages. Median Theil's U is around 20 percent for the unadjusted weather models, and closer to 30 percent for the unadjusted averages. The additive adjustment to the last two hours still tends to minimize both bias and median Theil's U for each estimation-selection combination, though in some cases the scalar adjustment does somewhat better. In terms of the extreme Theil's U, the scalar adjustment always does best. For the averages, the THI adjustments are better than no adjustment, but worse than any of the adjustments to the pre-curtailment hours. Without adjustment, the weather models have smaller bias than the averages, but with adjustment to pre-curtailment hours the averages perform about as well as the weather models.

5.4.2 Non-Weather-Sensitive Accounts

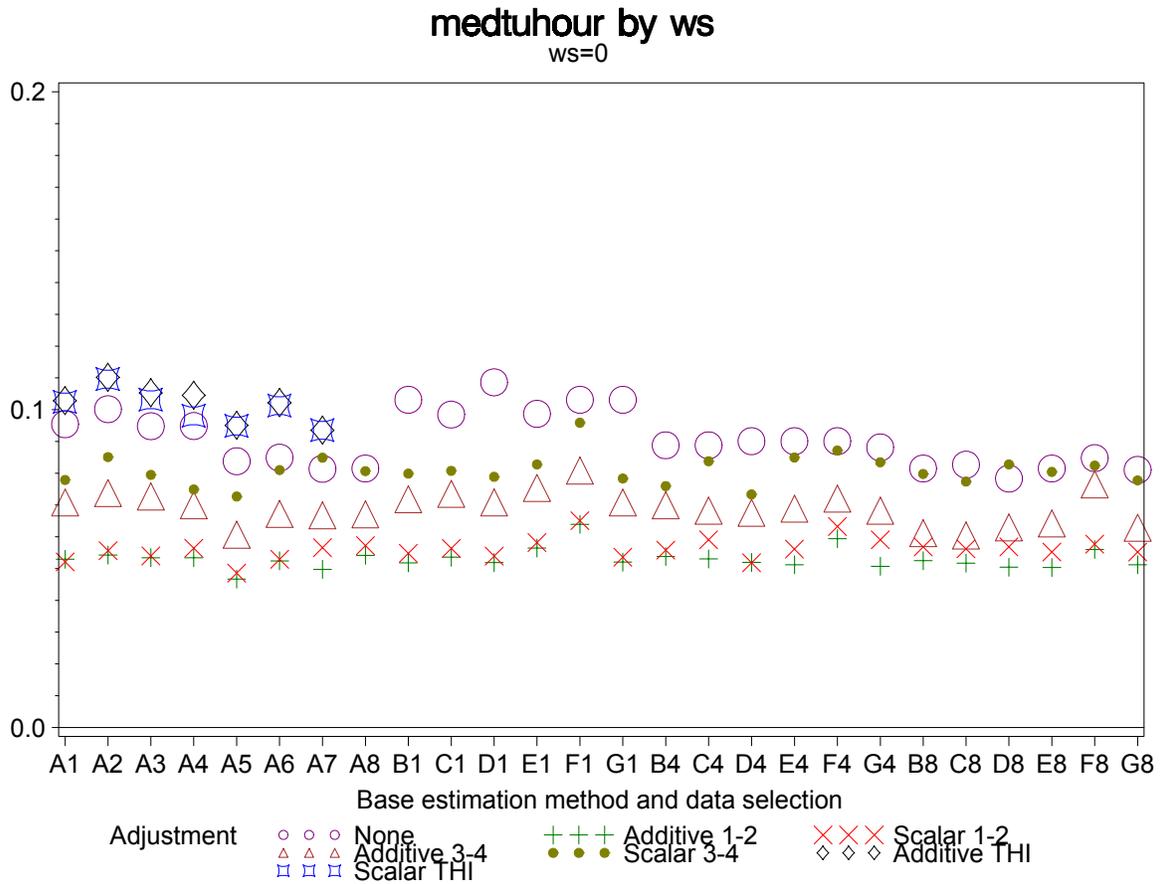
Low-Variability Accounts

Figures 5-10 through 5-12 show the performance for non-weather-sensitive low-variability accounts in the summer.

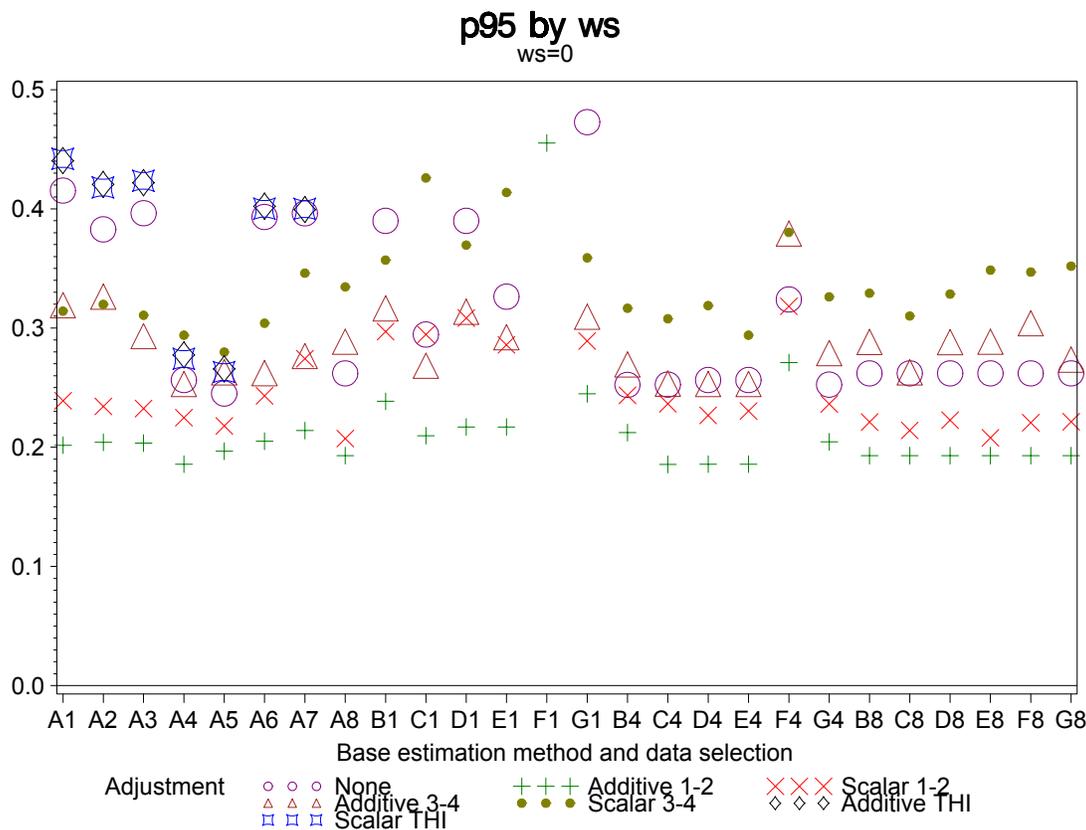
**Figure 5-10**  
**Median Relative Hourly Error**  
**Summer Uncurtailed Non-Weather-Sensitive Low-Variability Accounts**



**Figure 5-11**  
**Median Account Theil's U**  
**Summer Uncurtailed Non-Weather-Sensitive Low-Variability Accounts**



**Figure 5-12**  
**95<sup>th</sup> Percentile Account Theil's U**  
**Summer Uncurtailed Non-Weather-Sensitive Low-Variability Accounts**



Observations from these plots include the following.

1. Most of the unadjusted averages (A1 through A5) show some negative bias (around -1 percent) even for these non-weather-sensitive accounts. The reason may be that these accounts do have some weather-sensitive load components, but the diagnostics classify the account as non-weather-sensitive because other variations generally dominate the weather-sensitive load components.
2. The unadjusted High 5 average (A7) tends to over-adjust, with a median +3 percent relative error.
3. With adjustments, all the methods come within  $\pm 1$  percent median relative error.
4. For all estimation-selection methods, the adjustment to the last two hours again has the lowest median Theil's U of all the adjustment methods, and in most cases has the smallest or nearly smallest median relative hourly error.
5. The THI adjustments have the worst bias and worst median Theil's U for all the averages.
6. The conditional weather models perform about the same as the averages. However, the lag models have somewhat worse variability indicated by higher median Theil's U. For

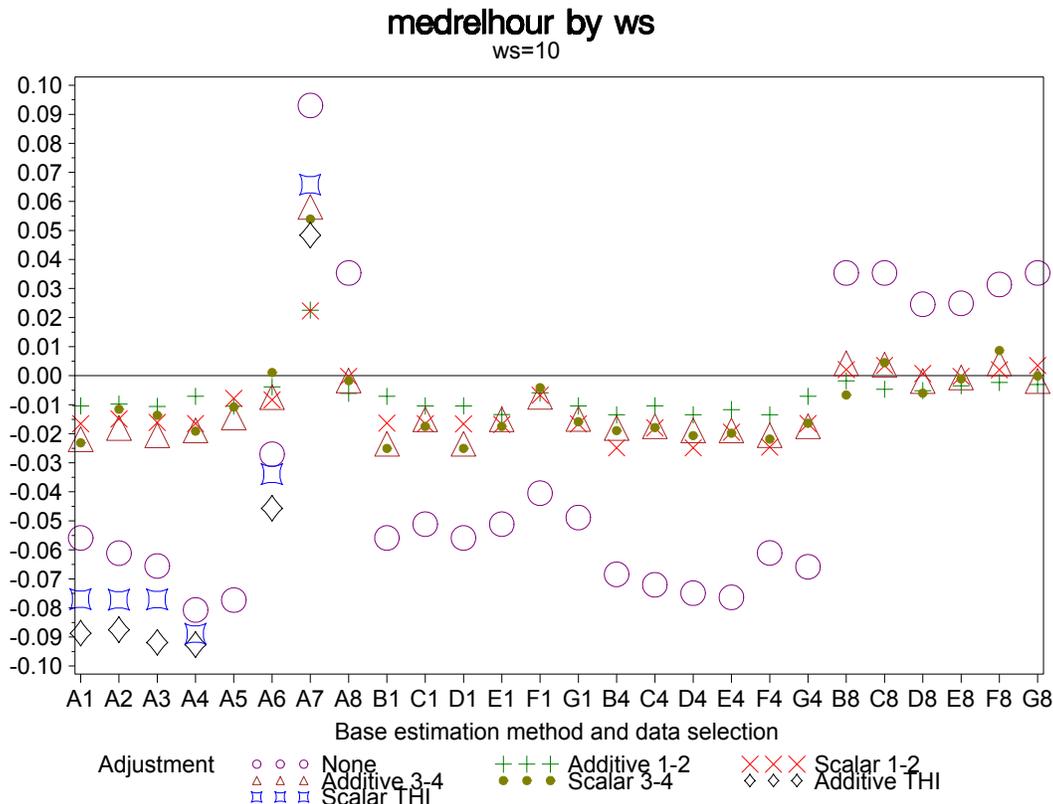
weather models based on less than a full season, the extremes (indicated by 95<sup>th</sup> percentile Theil's U) are much worse with the lag model.

**High-Variability Accounts**

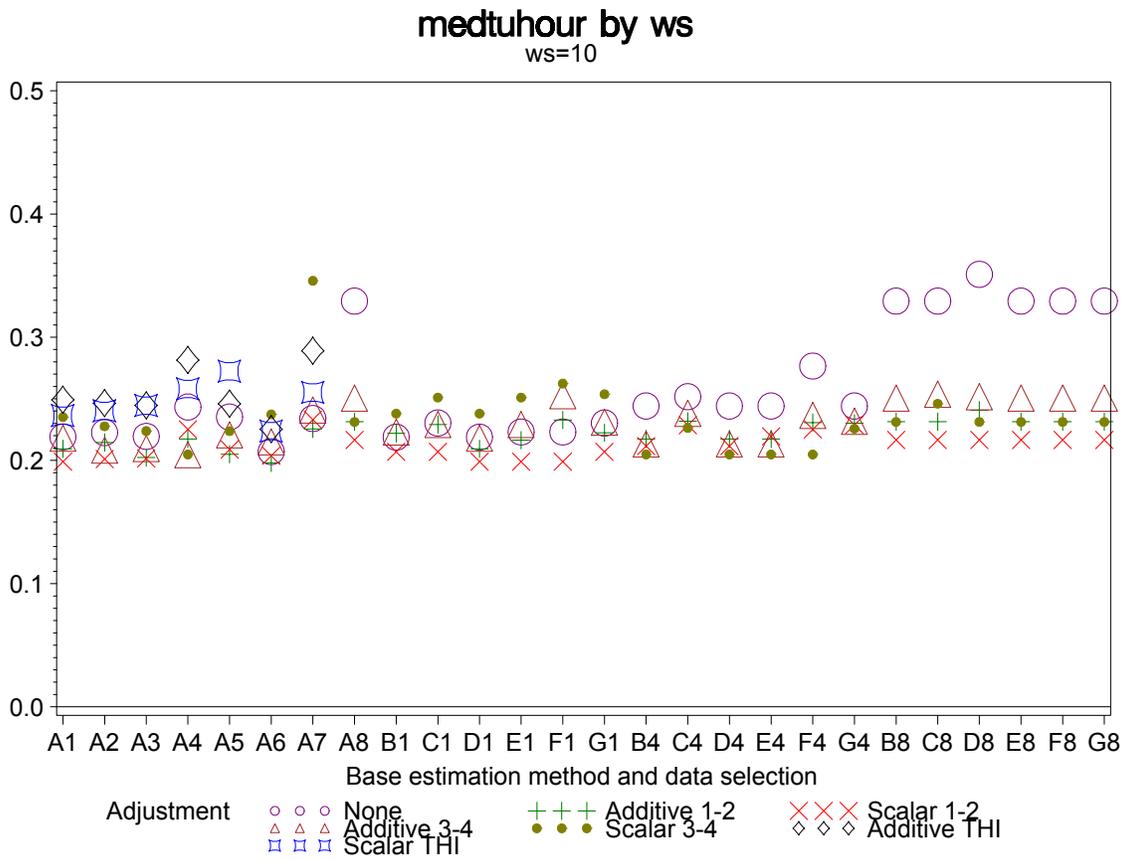
The final set of figures for tests of uncurtailed accounts are for the non-weather-sensitive high-variability accounts. As for the weather-sensitive accounts, the high-variability accounts show median relative errors farther from zero and larger median and 95<sup>th</sup> percentiles of account Theil's U. That is, both systematic errors and overall error magnitudes are larger than for the low-variability accounts.

For each adjustment method, the full-season weather models have slightly less bias but much worse variability than the averages, indicated by higher median and 95<sup>th</sup> percentile Theil's U. Thus, for high-variability accounts without weather drivers, using a closer set of days is more helpful than having a longer data series. The 10- and 20-day weather models perform comparably to the averages. The additive adjustment to the last two hours is still the best performer in terms of Theil's U and median relative error. However, the other adjustments, other than the THI, are nearly as good.

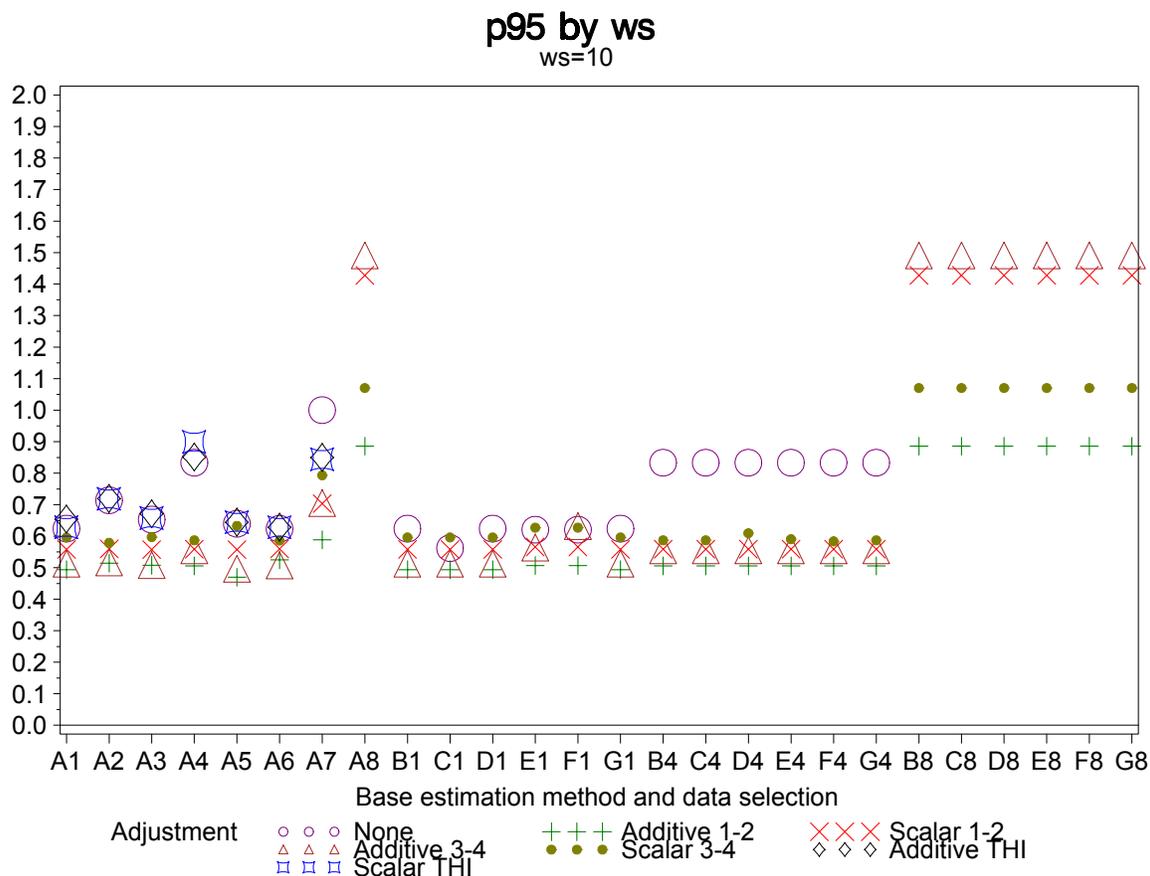
**Figure 5-13**  
**Median Relative Hourly Error**  
**Summer Uncurtailed Non-Weather-Sensitive High-Variability Accounts**



**Figure 5-14**  
**Median Account Theil's U**  
**Summer Uncurtailed Non-Weather-Sensitive High-Variability Accounts**



**Figure 5-15**  
**95<sup>th</sup> Percentile Account Theil's U**  
**Summer Uncurtailed Non-Weather-Sensitive High-Variability Accounts**



### 5.4.3 Summary

Based on the results for uncurtailed accounts above, it appears that the following can be recommended for summer baselines:

1. Additive adjustment to the two hours before curtailment appears to be the best adjustment, in terms of minimizing both bias and overall error magnitude, for all methods, for weather-sensitive and non-weather-sensitive, high- and low-variability accounts.
2. For weather-sensitive accounts, weather models perform somewhat better than averages. However, adjusted averages (scalar or additive) can perform nearly as well. Longer input data series improves weather model performance, but only slightly.
3. For non-weather-sensitive accounts, conditional weather models (i.e., models that drop inappropriate weather variables based on diagnostic screening) do not increase variability compared to simpler averages. However, for high-variability non-weather-sensitive

accounts full-season weather models can be higher variability than either simple averages or weather models based on 10 or 20 days.

4. The High 5 of 10 selection rule (highest 5 of last 10 days) gives the best unadjusted average for weather-sensitive accounts. However, with additive adjustment to the last two hours the method is no better than the other averages. For non-weather-sensitive accounts the High 5 of 10 average has positive bias unless an adjustment is included.
5. The THI adjustments have higher variability and worse bias than the other adjustments to averages.

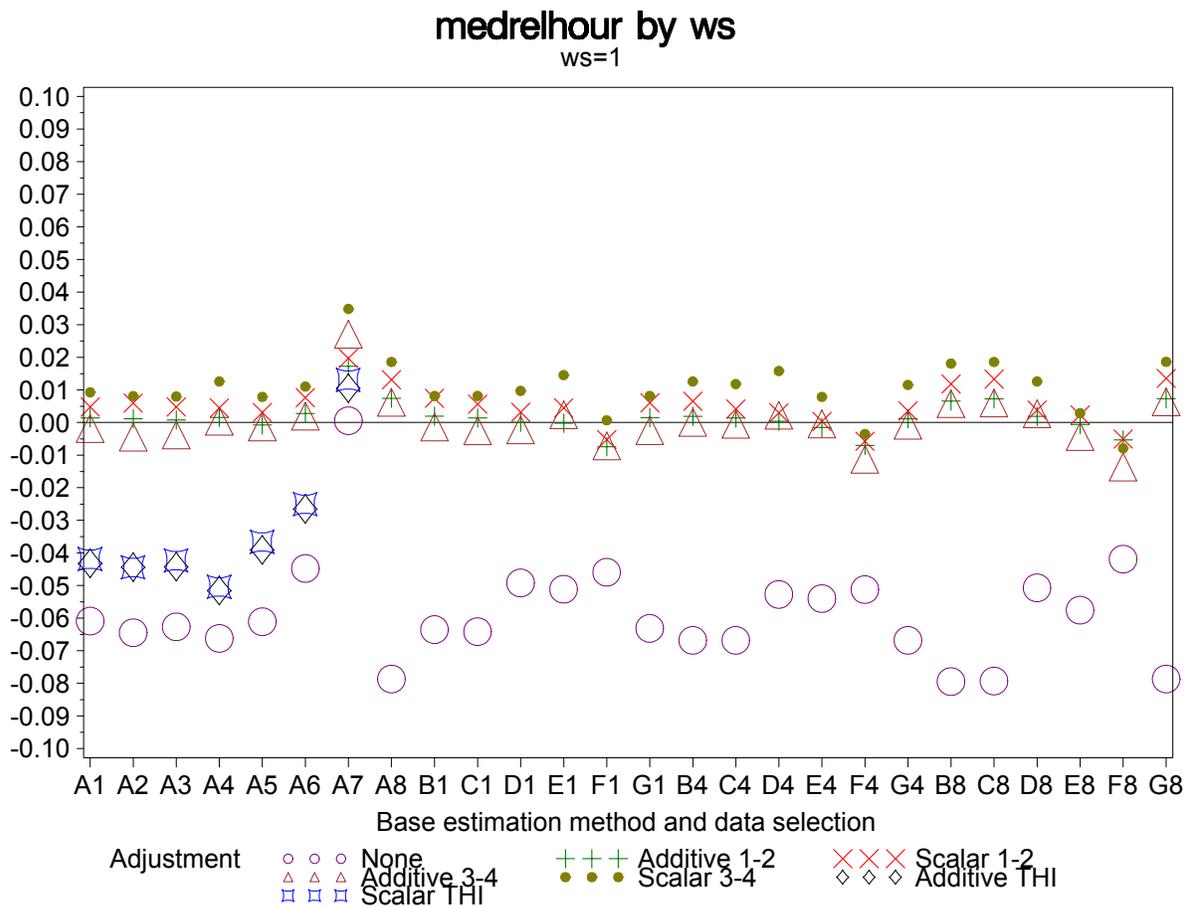
### 5.5 UNCURTAILED ACCOUNTS, NON SUMMER

Results for weather-sensitive accounts in the non summer period corresponding to those shown above are shown in the next series of figures. Observations for all non summer results are provided at the end.

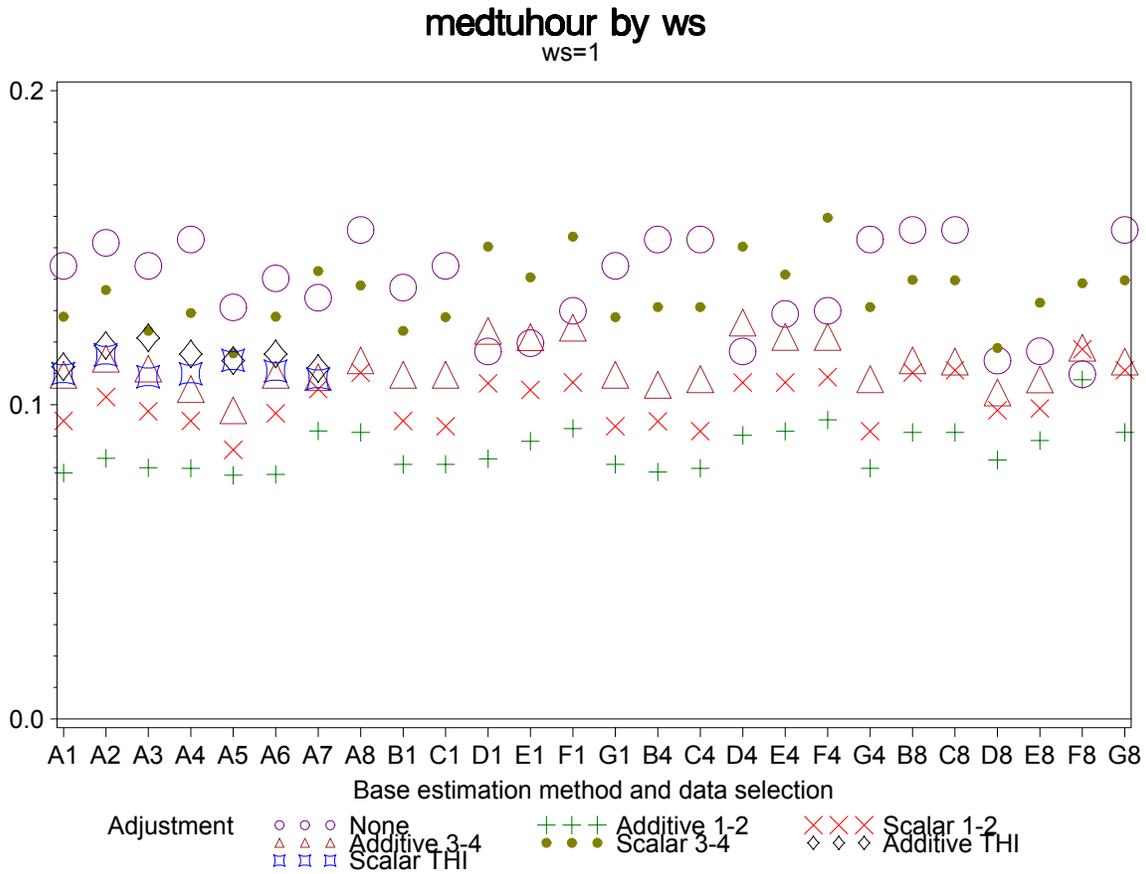
#### 5.5.1 Weather-Sensitive Accounts

##### Low-Variability Accounts

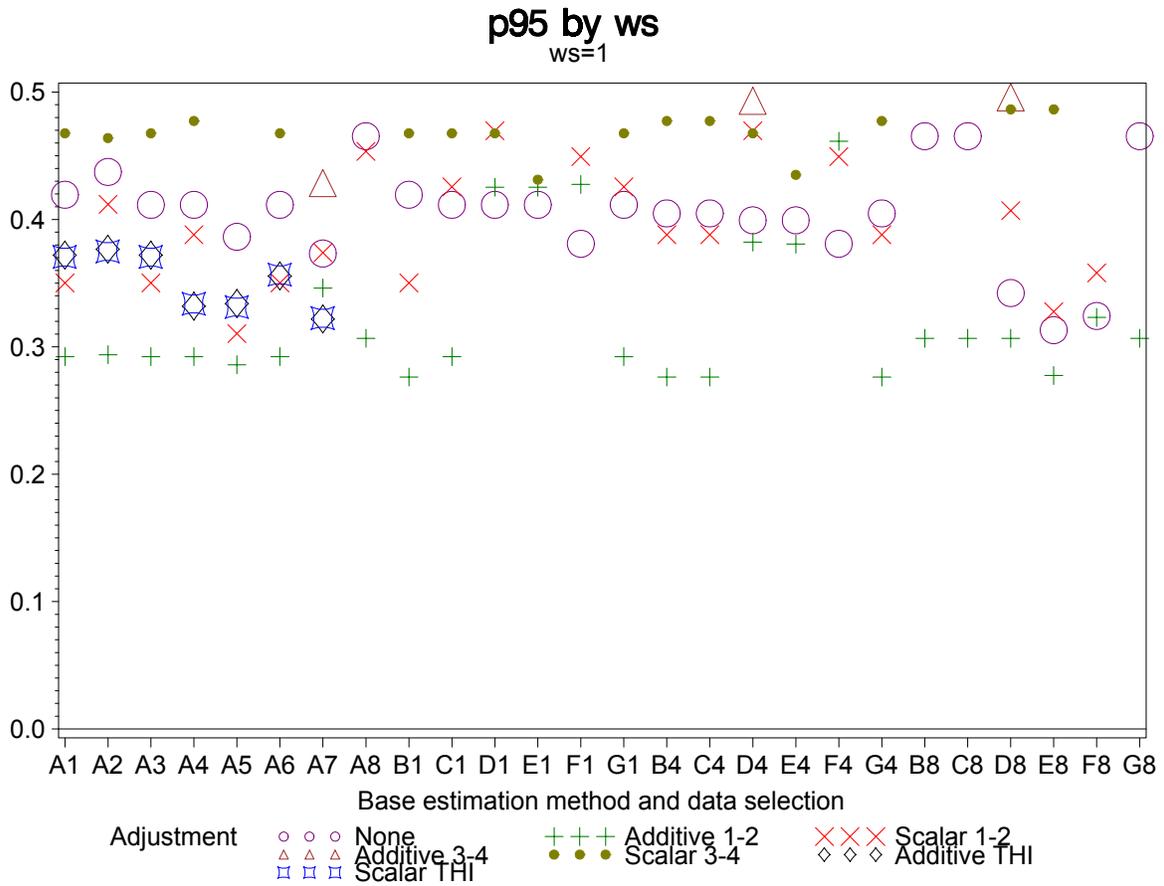
**Figure 5-16**  
**Median Relative Hourly Error**  
**Nonsummer Uncurtailed Weather-Sensitive Low-Variability Accounts**



**Figure 5-17**  
**Median Account Theil's U**  
**Nonsummer Uncurtailed Weather-Sensitive Low-Variability Accounts**

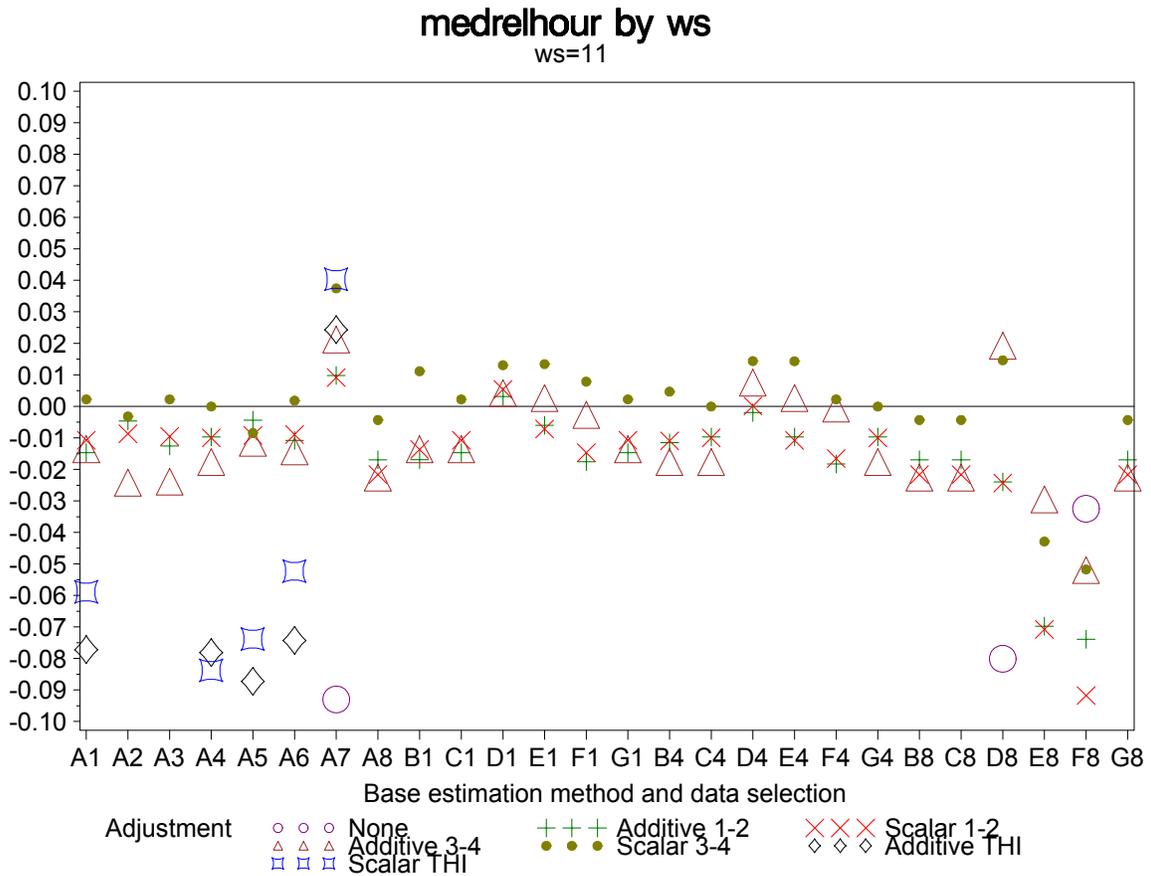


**Figure 5-18**  
**95<sup>th</sup> Percentile Account Theil's U**  
**Nonsummer Uncurtailed Weather-Sensitive Low-Variability Accounts**

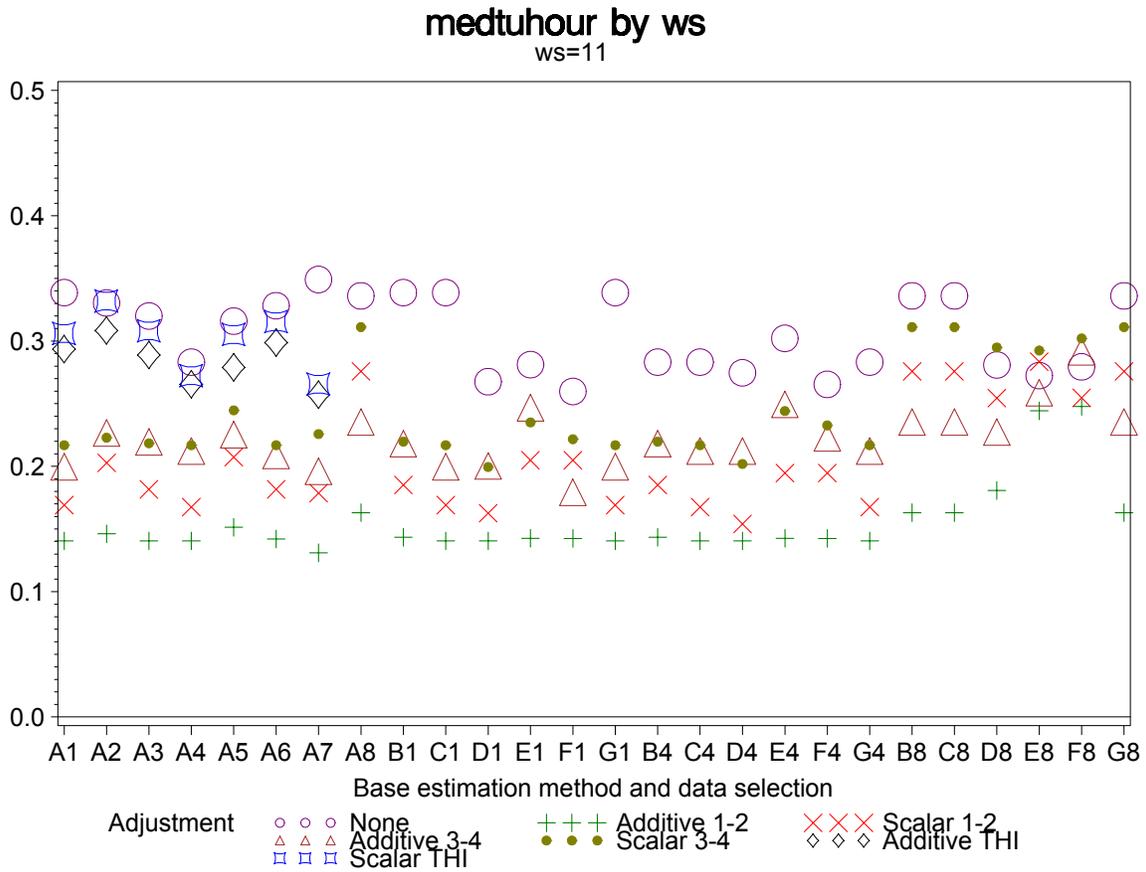


**High-Variability Accounts**

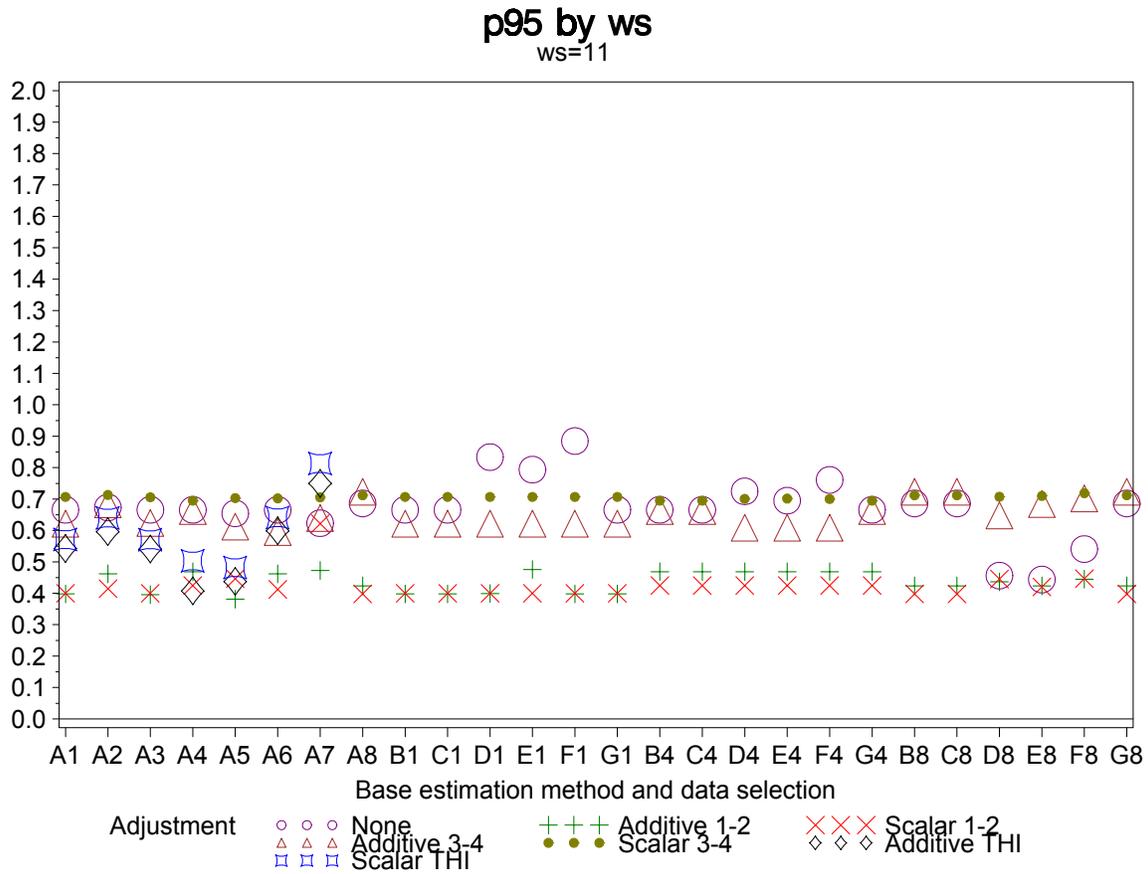
**Figure 5-19**  
**Median Relative Hourly Error**  
**Nonsummer Uncurtailed Weather-Sensitive High-Variability Accounts**



**Figure 5-20**  
**Median Account Theil's U**  
**Nonsummer Uncurtailed Weather-Sensitive High-Variability Accounts**



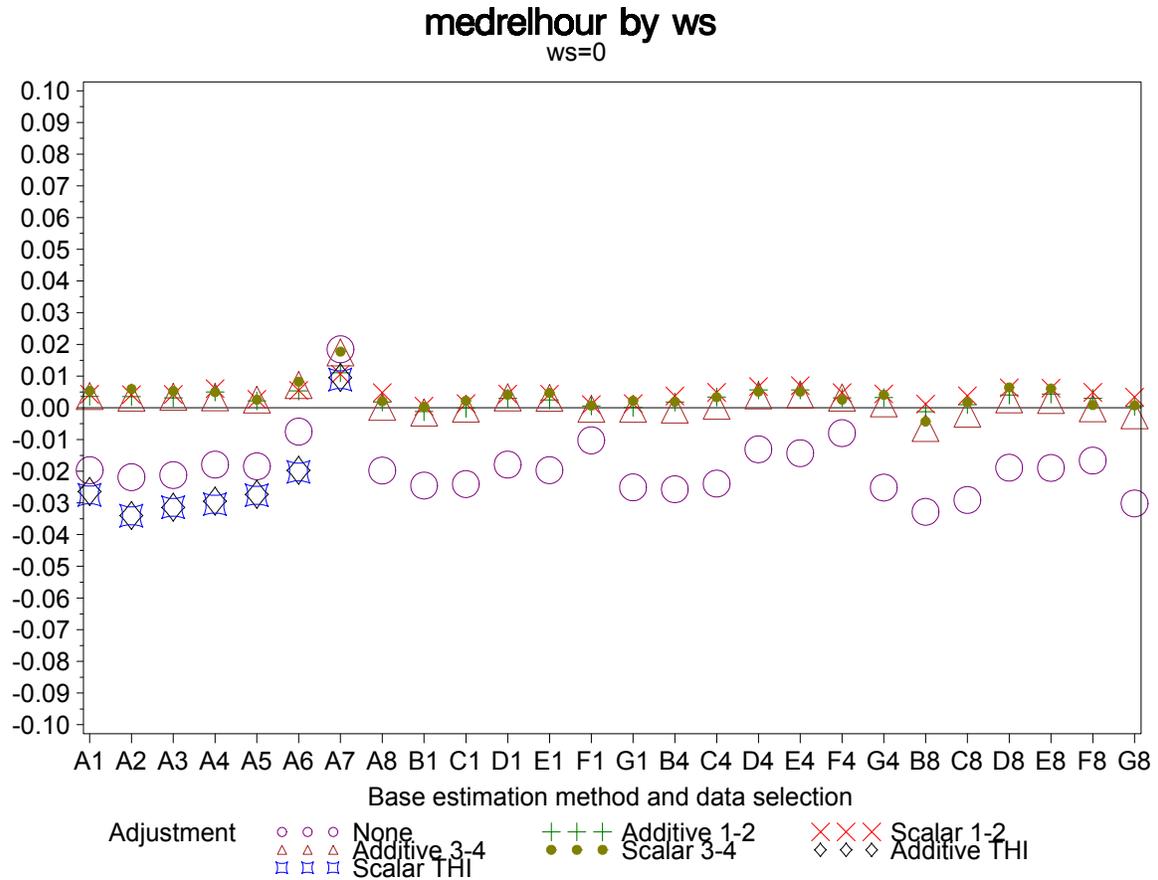
**Figure 5-21**  
**95<sup>th</sup> Percentile Account Theil's U**  
**Nonsummer Uncurtailed Weather-Sensitive High-Variability Accounts**



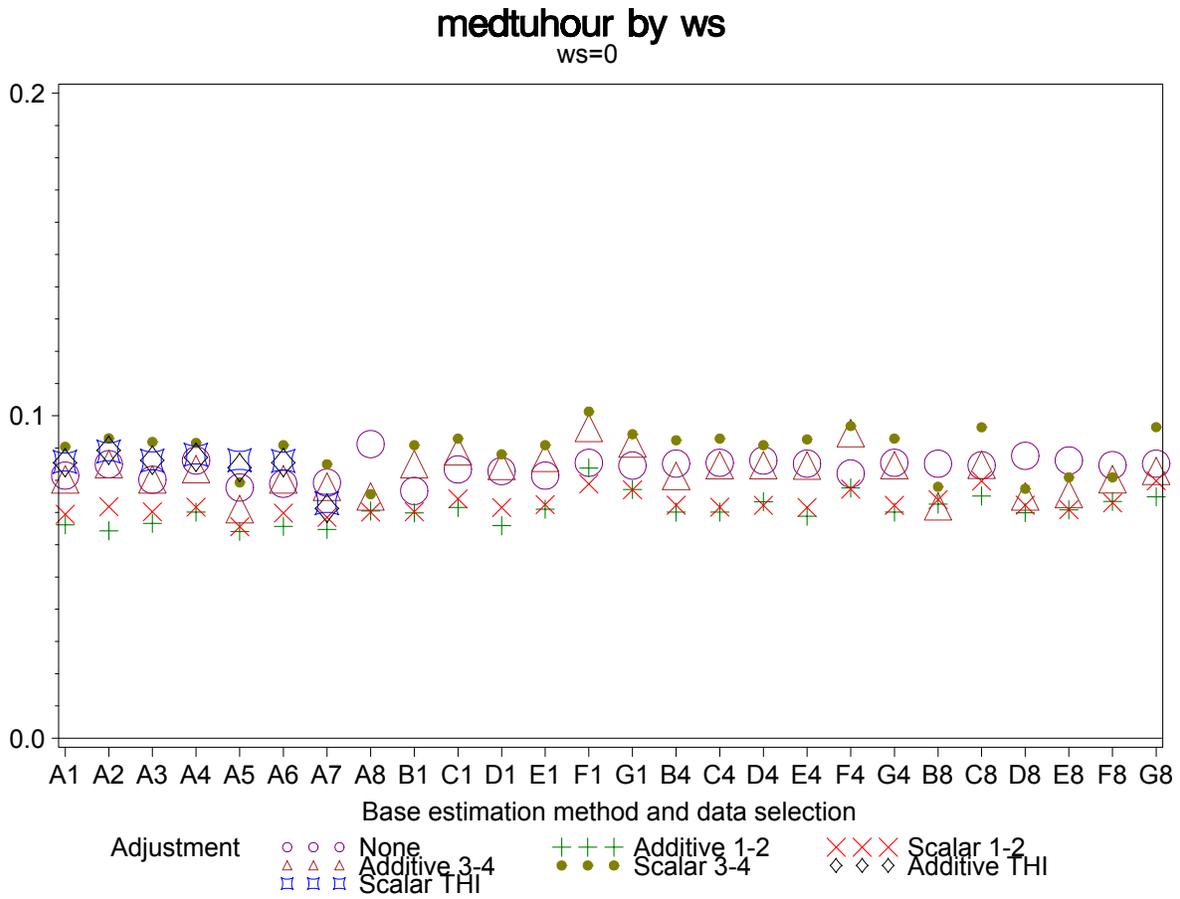
5.5.2 Non-Weather-Sensitive Accounts

Low-Variability Accounts

Figure 5-22  
 Median Relative Hourly Error  
 Nonsummer Uncurtailed Non-Weather-Sensitive Low-Variability Accounts



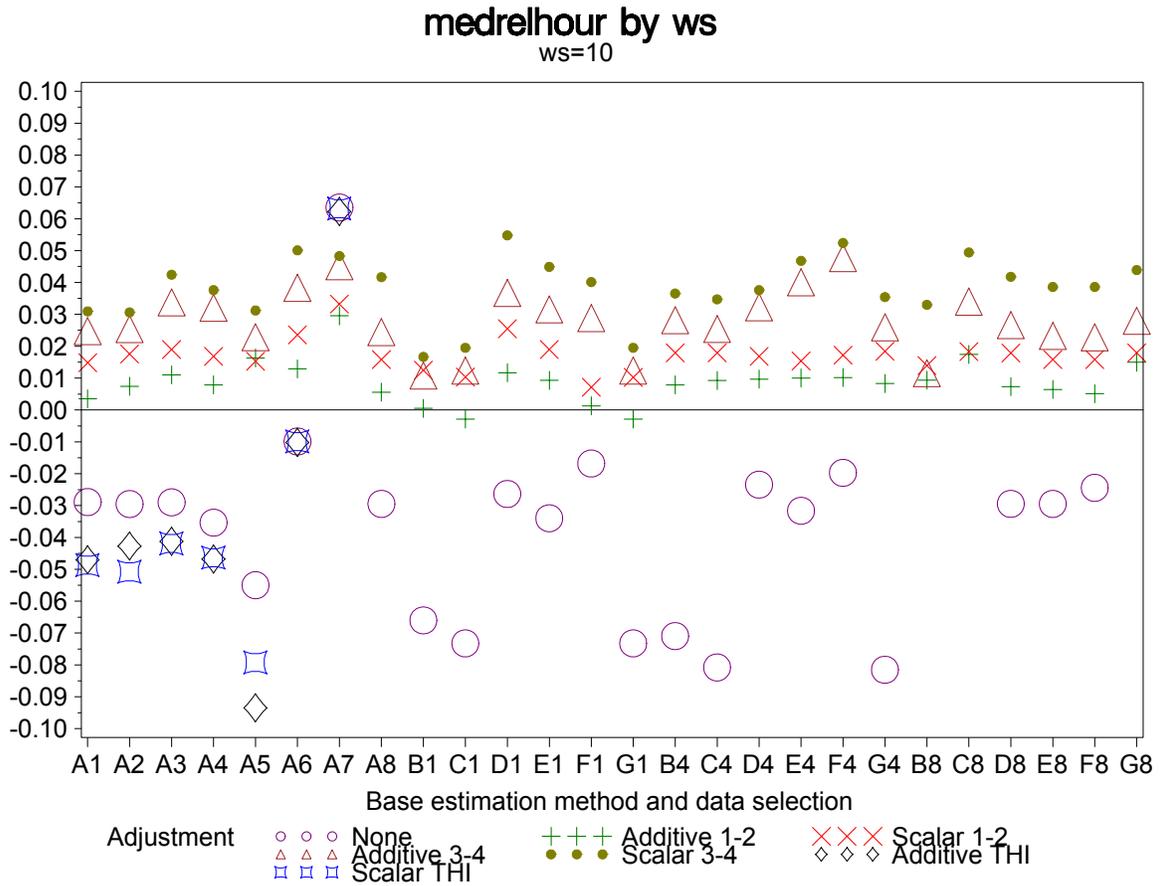
**Figure 5-23**  
**Median Account Theil's U**  
**Nonsummer Uncurtailed Non-Weather-Sensitive Low-Variability Accounts**



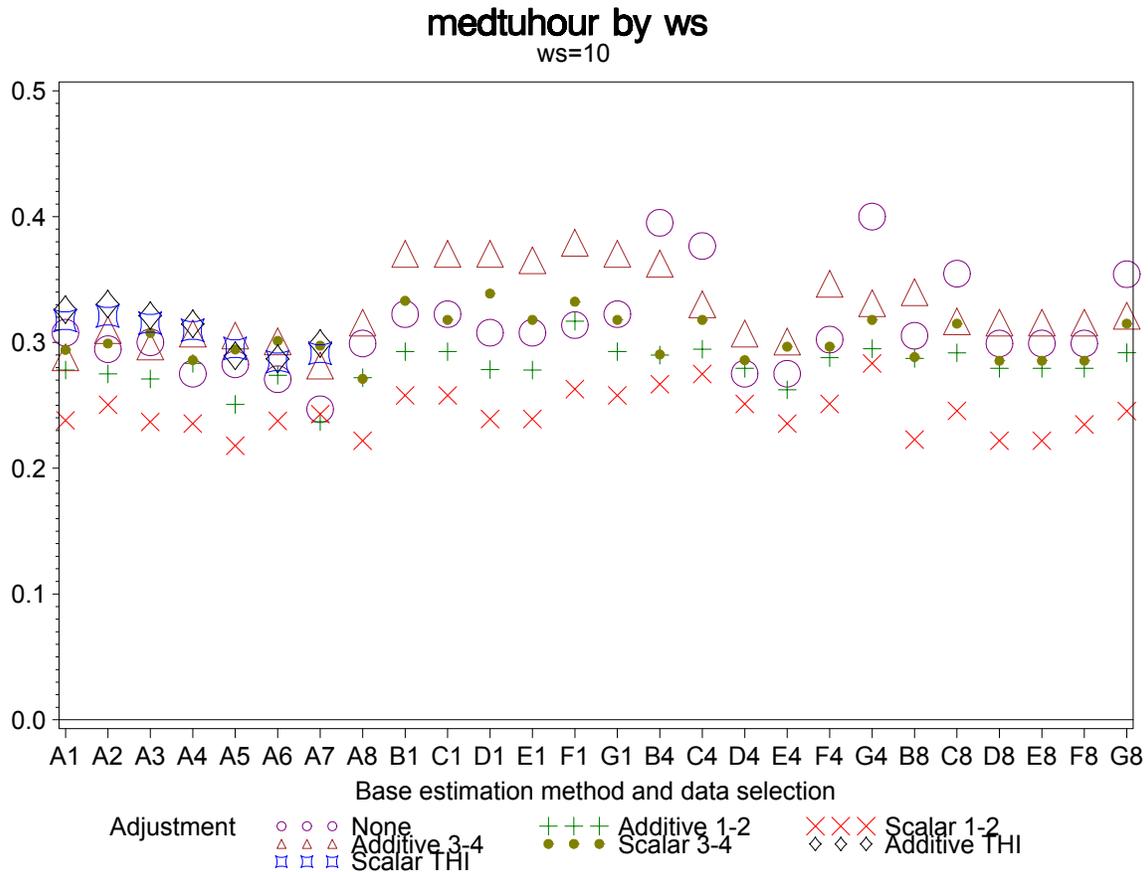


**High-Variability Accounts**

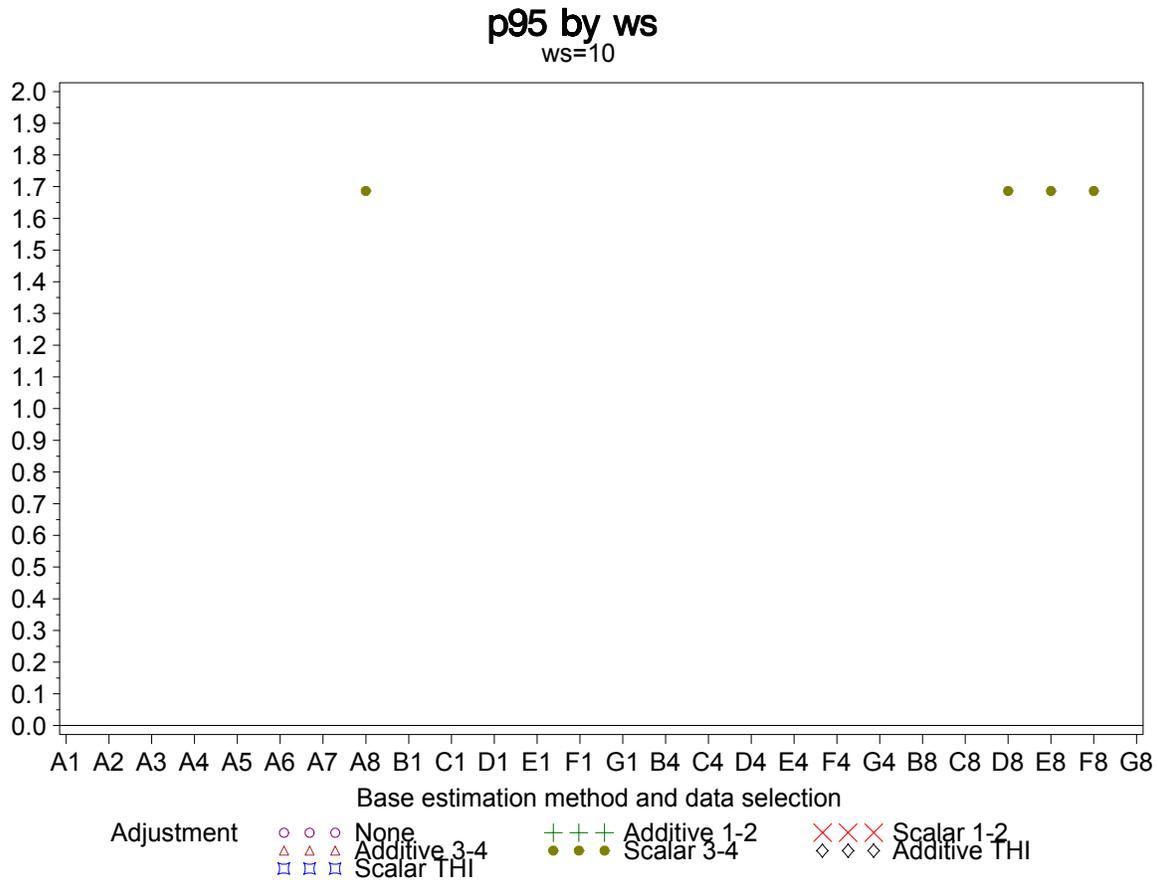
**Figure 5-25**  
**Median Relative Hourly Error**  
**Nonsummer Uncurtailed Non-Weather-Sensitive High-Variability Accounts**



**Figure 5-26**  
**Median Account Theil's U**  
**Nonsummer Uncurtailed Non-Weather-Sensitive High-Variability Accounts**



**Figure 5-27**  
**95<sup>th</sup> Percentile Account Theil's U**  
**Nonsummer Uncurtailed Non-Weather-Sensitive High-Variability Accounts**



### 5.5.3 Observations for Non Summer Accounts

Observations for the uncurtailed non summer accounts are as follows:

- Accurate weather modeling is more difficult than for summer loads. The performance of weather models is not clearly better than that of the use of average day methods even for low-variability weather-sensitive accounts. For high-variability weather-sensitive accounts the adjusted averages do better in terms of both bias and overall error magnitude.
- For low-variability weather-sensitive accounts, the unadjusted High 5 of 10 average method performs best in terms of small bias and low variability. For high-variability and/or non-weather-sensitive accounts, the unadjusted High 5 method does not perform as well as adjusted methods.
- For all estimation-selection rules and three of the four account types, the additive adjustment to the last two hours has smallest median Theil's U, and smallest or close to

smallest bias. However, for high-variability non-weather-sensitive accounts, the scalar adjustment has slightly worse bias but somewhat lower Theil's U.

- For non-weather-sensitive accounts there is little difference across estimation methods and selection rules in either bias or overall error magnitude.
- Unadjusted averages and weather models tend to understate baseline load profiles and peak savings estimates.

## 5.6 CURTAILED SUMMER ACCOUNTS

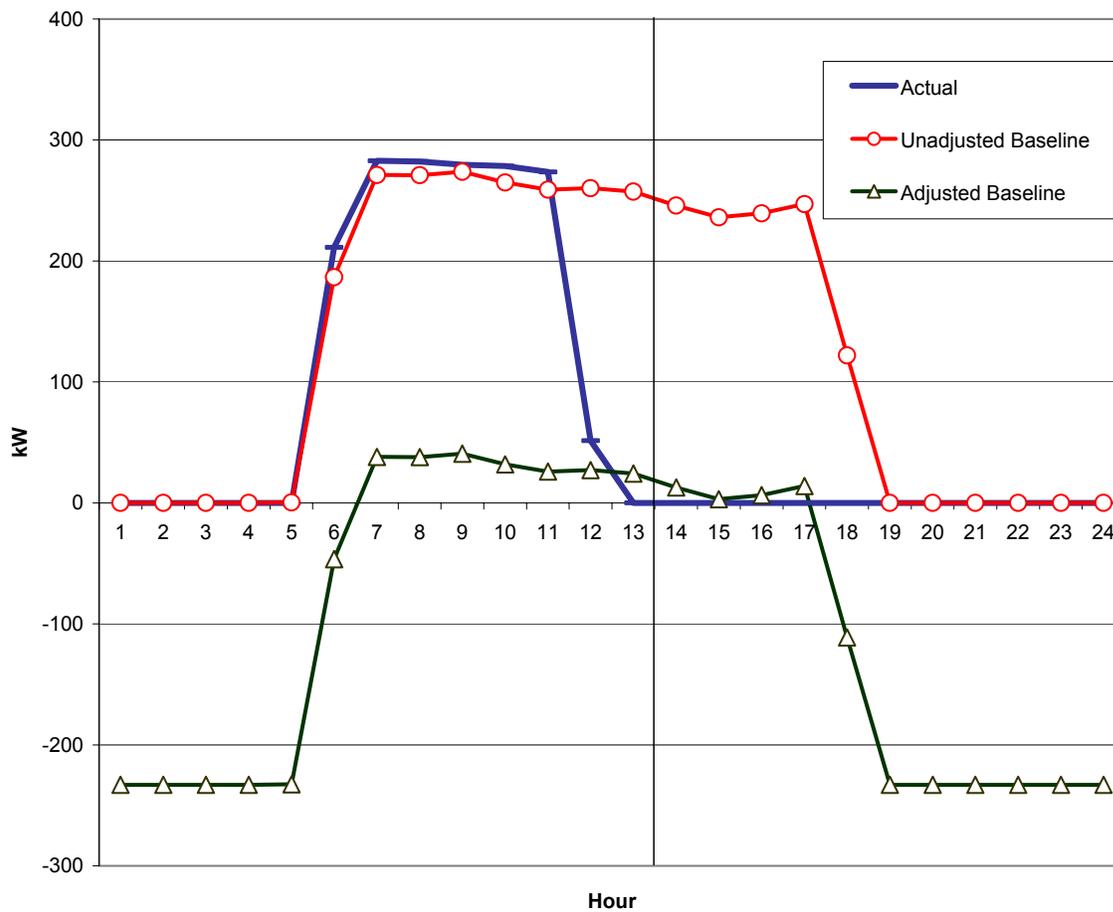
### 5.6.1 *Reference Case for Comparisons*

To provide similar method comparisons to those presented above for actual curtailment events, it was necessary to select a method to represent the best estimate of the true load that would have occurred in the absence of curtailment. Based on the results for the uncurtailed accounts, we initially selected the conditional full-season degree-day model with additive adjustment to the last two hours.

However, the comparative results immediately illustrated a key shortcoming of this method in actual curtailment situations. Many operations will send a shift home early or cancel a shift entirely when faced with a curtailment notice or the likely prospect of one. When this happens, the load in the two hours before curtailment is near zero, and the adjustment of the average or modeled load to these two hours produces a negative or zero baseline for the duration of the curtailment period.

An example of such an account is shown in the next figure. Although the actual load was reduced to zero in hour 13, the curtailment did not begin until hour 14. The adjusted baseline was near zero during usual operating hours, and became substantially negative after the hours when load customarily dropped to zero.

**Figure 5-28**  
**Adjustment to Last Two Hours for Account That Curtailed before Required Time**



To avoid this type of problem, we defined the “true” load for curtailed cases as the unadjusted full-season daily degree-day model.

### 5.6.2 Findings for Curtailed Accounts

#### *Errors in Baseline Estimation*

The displays for the curtailed accounts are shown in Appendix B. With the true load in the absence of curtailment defined as indicated above, the results for the curtailed cases generally followed similar patterns to those seen for the uncurtailed cases, with the following differences.

1. All the full-season weather models show very little bias and low variability. This is because there is little difference among the models, as indicated by the uncurtailed results. Thus, the relative errors, defined as the relative difference between a method and

the reference method, which is one of the full season models, are small. For the model chosen as the reference (unadjusted D8), all the errors are necessarily 0.

2. The unadjusted methods tend to show smaller biases and smaller Theil's U than for the same account types with uncurtailed accounts. This result makes sense given the similarity between the weather models and the averages, with a weather model defined as "truth." That is, the errors are reduced because part of the natural variability in actual loads is eliminated by defining truth as the result of the weather model.
3. The adjustment to the last two hours, rather than looking like the best method in most cases, shows substantial negative bias, and large overall error magnitude.
4. The adjustment to the third and fourth hours prior to curtailment generally has greater negative bias and worse overall error magnitude than for the same account type with uncurtailed accounts. This result indicates that some of the "pre-event" curtailment effects are seen in these hours as well as in the immediate last two hours.

Thus, the methods that work best in the abstract case of accounts that were not actually subject to a curtailment process can be very problematic in practice. The recommendations in Section 6 address this problem.

### ***Errors in Estimating Demand Reduction***

In addition to looking at errors relative to estimated actual loads, we also looked at errors relative to the estimated load reduction, as noted in Section 4. These results are also included in Appendix B.

In terms of program operations, the important question is how far off the estimated reduction is from the customer's actual load shed. While the magnitudes are greater, the qualitative patterns of errors relative to reduction amounts are similar to those for errors relative to load levels. Very roughly, the medians and Theil's U statistics for errors relative to estimated reductions are about three times as large as the errors relative to estimated load. This relationship corresponds to reductions being on the order of one-third of total load. Of course, for an individual account and hour the reduction may be anywhere from a small fraction to 100 percent of the load.

This study has examined methods of calculating customer baseline loads for the purpose of estimating peak load reductions from demand response programs. The examination began by defining a vocabulary of method features as a basis for describing and comparing alternative methods. Using this foundation, the study has considered:

- qualitative issues related to calculation methods that are of concern to stakeholders
- conceptual pros and cons of different method features in terms of these issues
- quantitative performance tests related to accuracy and bias for a range of methods combining various features.

In this section, we review the issues that are important for baseline calculation methodologies. We then summarize the advantages and disadvantages of different method features in terms of both qualitative considerations and the quantitative results of the performance tests conducted. We provide further detail on the quantitative test results for different types of customer accounts. Finally, taking into account both the qualitative and quantitative findings, we offer general recommendations for baseline calculation methods for different types of accounts and conditions, and provide guidance on choosing among methods.

## **6.1 GENERAL FINDINGS**

Important considerations in defining a baseline calculation method include:

- simplicity of calculation
- minimizing burden on participants and operators, in terms of costs, ease of understanding, and ease of operation
- limiting the potential for gaming
- limiting the potential for distortion if load is curtailed early
- ability to know the baseline immediately after a curtailment
- ability to know the baseline before making a curtailment decision
- minimizing method bias: systematic tendency to over- or under-state
- minimizing method variability: tendency to wide swings in estimates.

Specific concerns that have been addressed by developers of existing baseline methods for demand response programs include:

- providing accurate baselines for weather-sensitive accounts
- avoiding windfall credits for cool weather

- avoiding windfall credits for planned shut-downs.

Advantages and disadvantages of key method features in terms of these concerns are summarized in the table below. This table expands the qualitative summary provided in Section 3 with findings from the test results presented in Section 5.

**Table 6-1  
Advantages and Disadvantages of Key Baseline Method Features  
Based on Qualitative Considerations and Test Results**

Baseline Method	Variant	Pros	Cons	
Average	Any	Simple, easy to use and understand, low cost	Tends to understate baseline for weather-sensitive loads, especially if unadjusted	
	High 5 of last 10 days	Partial adjustment for weather-sensitive loads	Still tends to understate baseline for weather-sensitive loads	
			Can allow windfall load reduction credit on cool days	
Regression	Any	Provides baseline corresponding to particular weather conditions of curtailment day	More complex, harder to understand, higher cost	
			If observations don't include conditions as extreme as the curtailment day, model estimate may be inaccurate	
			If account isn't weather-sensitive, may be less accurate than simpler methods	
	Full Season	Adequate data and range of variation to yield accurate coefficients	Operating conditions from the period data are taken from may be different from curtailment day	
	Recent 10 days	Operating conditions more likely to be similar to curtailment day	Model based on limited data may be inaccurate	
	Lag temperature/degree-day	Tends to reduce bias for weather-sensitive accounts	Tends to increase variability of baseline estimate.	
Adjustment to precurtailment hours	Any	Simple, easy to use and understand, low cost	May be potential for gaming behavior during day-of-curtailment adjustment period	
			Adjusts to weather and operating conditions of curtailment day	Appropriate pre-curtailment increase in load (e.g., pre-cooling) will result in overstated baseline
			Limits potential for collecting windfall credits for planned shut-downs	Pre-curtailment decrease in load in response to curtailment request (e.g., long ramp-down, canceling a shift) will result in understated baseline
	Additive	May adjust well for load change that is constant throughout day (e.g., industrial processes)	May not be appropriate if load changes during curtailment period (ratio adjustment may be better suited)	
	Scalar	May adjust well for load change that is function of exogenous factor throughout day (e.g., higher levels of occupancy)	May not be appropriate if the day-to-day load variation is constant over the day (additive adjustment may be better suited)	
	to last 2 hours before curtailment period	If load in these hours is unaffected by anticipated or initiated curtailment, provides best accuracy	If substantial curtailment is initiated in these hours, severely understates baselines	
	to 3rd and 4th hour before curtailment period	Less potential for understated baseline due to pre-curtailment-period demand response	More variability than adjustment to last 2 hours	
Weather-Based Adjustment	Any	Explicitly takes into account weather conditions	Adjustment may not be known to customer until after curtailment period (i.e., until after weather conditions are known for the day)	
			No opportunity for gaming as with adjustment to precurtailment hours	If no observations are available for extreme conditions, estimates used for adjustment may be outside range of model
				Will badly predict load reductions if the buildings are dominated by internal loads
				Less accurate than alternative adjustments or weather model for both weather-sensitive and non-weather-sensitive accounts

Further details on the test results are provided below. Recommendations based on both the practical design considerations and the test results are then presented.

## 6.2 FINDINGS FROM TESTS ON UNCURTAILED ACCOUNTS

Test results for both weather-sensitive and non-weather-sensitive summer accounts for the best performing methods are summarized in Table 6-2. Qualitative conclusions from the test findings for both summer and nonsummer are described below.

### 6.2.1 *Weather Models*

#### ***Summer Weather-Sensitive Accounts***

- For summer weather-sensitive accounts, best overall performance (low bias and low variability) is a weather model with adjustment.
- Performance is not dramatically different for different models tested, except that the model with lagged degree-day term showed higher variability than the others.
- The unadjusted lag model based on a full season of data had the lowest bias of any unadjusted method, about 0.2 percent. But with adjustment the bias was higher than with almost any other method (+ 3 to 4 percent).
- Simple models based on daily temperature or daily degree-days performed about as well as a model with hourly degree-days.
- Adjusted averages can perform nearly as well as weather models, but tend to have either worse bias or worse variability or both.
- Without adjustment, all the weather models except the full-season lag model still tend to understate the baseline, though not by as much as the unadjusted averages.
- Both bias and variability are reduced by longer input data series.

#### ***Summer Non-Weather-Sensitive Accounts***

- Use of a “conditional” weather model (that drops weather variables for an account if they’re not statistically significant or tend to have the wrong sign) doesn’t increase variability compared to using an average, and appears to reduce some potential for bias.
- For high variability accounts, the lowest variability and bias is for the full season conditional weather models. With less than a full season of data, many of the adjusted averages perform about as well. However, the “high 5” (highest 5 of the last 10) has higher variability than the other averages.
- Adjustment to the hours before curtailment is important for both averages and weather models.

**Table 6-2**  
**Summary of Test Results for Summer Accounts**

Load Type	Estimation	Data Selection	Adjustment	Median Relative Hourly Error			Median Relative Root-Mean Square Error			Extreme Relative Root-Mean Square Error			
<b>Weather-Sensitive Low Variability</b>	Weather Model	last 10	add 1-2	-0.2%	to	0.7%	5.8%	to	7.4%	15.2%	to	19.2%	
		last 20	add 1-2	-0.3%	to	1.1%	5.3%	to	7.5%	15.5%	to	22.3%	
		full season	add 1-2	-0.2%	to	2.9%	5.1%	to	6.9%	14.7%	to	19.2%	
	Average	High 5 of 10	add 1-2										
		last 10	add 1-2		0.3%			5.6%			15.2%		
	Weather Model	last 10	none		-2.7%	to	-1.6%	8.1%	to	10.7%	28.6%	to	30.7%
		last 20	none		-3.3%	to	-0.7%	7.9%	to	8.6%	23.4%	to	28.2%
		full season	none		-2.7%	to	0.9%	6.6%	to	8.2%	24.4%	to	26.9%
	Average	High 5 of 10	none										
		High 10 of 11	none										
		last 10	none		-4%			7%			25%		
	Average	High 5 of 10	add THI										
High 5 of 10		add THI		0.6%			5.8%			25.8%			
Average	High 5 of 10	add 3-4											
	last 10	add 3-4		0.1%			7.3%			22.9%			
	last 20	add 3-4		-1.5%			7.2%			23.0%			
<b>Weather-Sensitive High Variability</b>	Weather Model	last 10	add 1-2	-1.5%	to	0.0%	12.8%	to	15.7%	158.6%	to	208.5%	
		last 20	add 1-2	-1.9%	to	0.0%	11.4%	to	13.8%	128.6%	to	207.6%	
		full season	add 1-2	-2.0%	to	1.2%	10.3%	to	14.1%	136.8%	to	136.8%	
	Average	High 5 of 10	add 1-2										
		last 10	add 1-2		0.6%			11.9%			283.4%		
	Weather Model	last 10	none		-11.6%	to	-8.4%	19.0%	to	19.5%	272.0%	to	272.0%
		last 20	none		-8.7%	to	-5.4%	21.6%	to	23.3%	240.5%	to	240.5%
		full season	none		-7.7%	to	-1.5%	17.8%	to	25.0%	264.5%	to	264.5%
	Average	High 5 of 10	none										
		High 10 of 11	none										
		last 10	none		-9.4%			23.1%			551.7%		
	Average	High 5 of 10	add THI										
High 5 of 10		add THI		-3.9%			18.5%			546.7%			
Average	High 5 of 10	add 3-4											
	last 10	add 3-4		3.4%			14.0%			325.4%			
	last 20	add 3-4		-1.7%			13.7%			222.0%			
Average	High 5 of 10	add 3-4											
	last 10	add 3-4		-2.4%			15.6%			217.2%			
	last 20	add 3-4											

**Table 6-2 (cont)**  
**Summary of Test Results for Summer Accounts**

Load Type	Estimation	Data Selection	Adjustment	Median Relative Hourly Error			Median Relative Root-Mean Square Error			Extreme Relative Root-Mean-Square Error		
<b>Nonweather-Sensitive Low Variability</b>	Weather Model	last 10	add 1-2	-0.8%	to	0.8%	5.2%	to	6.4%	21.0%	to	45.5%
		last 20	add 1-2	-0.6%	to	0.1%	5.1%	to	5.9%	18.6%	to	27.1%
		full season	add 1-2	-0.7%	to	0.3%	5.0%	to	5.6%	19.3%	to	19.3%
	Average	High 5 of 10 last 10	add 1-2 add 1-2	0.1%			5.0%			21.4%		
				-0.7%			5.3%			20.2%		
	Weather Model	last 10	none	-0.8%	to	1.1%	9.8%	to	10.9%	29.5%	to	51.1%
		last 20	none	-0.6%	to	1.0%	8.8%	to	9.0%	25.2%	to	32.4%
		full season	none	-0.8%	to	0.4%	7.8%	to	8.5%	26.2%	to	26.2%
	Average	High 5 of 10 High 10 of 11 last 10	none none none	3%			8%			40%		
				0%			8%			39%		
-1.3%						9.5%			41.5%			
Average	High 5 of 10	scalar THI add THI	3.0%			9.4%			40.0%			
			2.9%			9.4%			39.9%			
Average	High 5 of 10 last 10 last 20	add 3-4 add 3-4 add 3-4	0.6%			6.7%			27.6%			
			-1.5%			7.1%			31.9%			
			-1.1%			7.0%			25.3%			
<b>Non-Weather-Sensitive High Variability</b>	Weather Model	last 10	add 1-2	-1.3%	to	-0.6%	20.9%	to	23.3%	49.4%	to	50.7%
		last 20	add 1-2	-1.3%	to	-0.7%	21.7%	to	23.2%	50.5%	to	50.5%
		full season	add 1-2	-0.5%	to	-0.2%	23.1%	to	24.1%	88.6%	to	88.6%
	Average	High 5 of 10 last 10	add 1-2 add 1-2	2.3%			22.6%			58.8%		
				-1.0%			20.9%			49.4%		
	Weather Model	last 10	none	-5.6%	to	-4.0%	21.9%	to	23.0%	56.2%	to	62.4%
		last 20	none	-7.6%	to	-6.1%	24.4%	to	27.7%	83.3%	to	83.3%
		full season	none	2.5%	to	3.5%	32.9%	to	35.1%	260.0%	to	260.0%
	Average	High 5 of 10 High 10 of 11 last 10	none none none	9.3%			23.4%			100.0%		
				-2.7%			20.7%			62.3%		
				-5.6%			21.9%			62.4%		
	Average	High 5 of 10	scalar THI add THI	6.6%			25.5%			84.4%		
				4.8%			28.9%			85.0%		
Average	High 5 of 10 last 10 last 20	add 3-4 add 3-4 add 3-4	5.8%			24.1%			70.5%			
			-2.2%			21.8%			51.2%			
			-1.9%			20.5%			55.5%			

### ***Nonsummer Accounts***

#### **Weather-Sensitive Accounts**

- Accurate weather modeling is more difficult than for summer accounts. The performance of weather models is not clearly better than that of the averages.
- For low-variability accounts, an additive adjustment with any of the averages except the “high 5 of 10”, and any of the models has a median relative error close to zero.
- For high-variability accounts, the adjusted averages have median relative error close to zero, while the weather models show some negative bias. The averages also show somewhat lower variability than the weather models.

#### ***Nonsummer Non-Weather-sensitive***

- For nonsummer non-weather-sensitive accounts there is little difference across estimation methods and selection rules in either bias or variability.
- For both weather models and averages, additive adjustment to the two hours before curtailment tends to produce the lowest bias and variability of any of the possible adjustments.
- Unadjusted averages and weather models tend to understate load.

### **6.2.2 Adjustments**

- Some kind of adjustment to hours before curtailment helps to reduce bias and variability even with weather models.
- Additive adjustment to two hours before generally performed best of the adjustments tested, in terms of both bias and variability reduction.
- Scalar adjustment to two hours before was often as good or better, but in some cases blew up and produced much higher variability.
- PJM’s THI-based adjustment generally had worse variability than the other adjustments, and was not superior in bias reduction.

### **6.2.3 Data Selection**

- Bias and variability of weather models is reduced by longer input data series, but not dramatically.
- The increased variability with shorter input series is more noticeable for conditional weather models applied to non-weather-sensitive accounts, particularly high variability accounts.

- The different averages compared performed similarly in terms of bias and variability, except for those that select a subset of days based on high load. For summer loads, the High 5 of 10 average reduces the otherwise negative bias. For summer loads using additive adjustment, High 5 of 10 gives the lowest bias of any of the averages, for both weather-sensitive and non-weather-sensitive accounts, and comparable variability. The 10 of 11 average gives some bias reduction, but not as much. For nonsummer loads, however, the High 5 of 10 average inflates an already positive bias. The other averages perform better, and roughly comparably to each other, in terms of both bias and variability, for both weather-sensitive and non-weather-sensitive accounts.

### 6.3 FINDINGS FROM TESTS ON CURTAILED ACCOUNTS

A key finding from testing curtailed accounts is the practical challenge of using adjustments to the hours just before curtailment. For uncurtailed accounts, adjustment to the last two pre-curtailment hours reduced both bias and variability for every estimation method and selection rule, except in some cases for the high 5 of 10 average. In most cases, this adjustment had lowest bias and lowest variability. This result makes sense because the hours closest to the curtailment period are likely to be most indicative of both weather and operating conditions for that day, in the absence of curtailment.

However, many of the actual curtailed accounts indicated curtailment, often to close to zero load, by the start of the two hours prior to the official start of the curtailment period. These are not cases of plant shut-down, since the earlier hours are at typical high loads. Rather, the operations appeared to be curtailed rapidly after a curtailment notification. In these cases, the adjustment to the two hours before the curtailment period produced very low, sometimes negative, baselines, with severe understatement of curtailment amounts.

For this reason, the additive adjustment is not a practical choice for accounts that are likely to implement load reductions in this way. As discussed in Section 3, this adjustment is also a concern because of the possibility that customers will deliberately boost load in the hours prior to curtailment to produce an artificially high baseline. Pre-cooling the building, without intent to “game” the system, can produce a similar distortion.

Thus, while the additive adjustment to the last two hours is very effective for accounts that will not change operations substantially outside of the curtailment period, this method has problems for other accounts. A different method is needed for accounts whose operations outside of curtailment periods is substantially affected by a notification or anticipation of a curtailment event.

Alternatives include the following:

1. Adjust to the third and fourth hours prior to curtailment. This approach reduces, but does not eliminate, the problem related to reductions before the start of the formal curtailment period, such as sending a shift home. The adjustment to earlier hours also reduces the potential for manipulation of the baseline, if notification is typically less than three hours from curtailment start. On the other hand, earlier hours are less indicative of what load would have been for the rest of the day absent curtailment. Test results for averages on uncurtailed accounts found that the adjustment to hours  $-3$  and  $-4$  adds some negative bias, and increases the variability compared to the adjustment to hours  $-1$  and  $-2$ . For weather-sensitive accounts, if the adjustment to hours  $-3$  and  $-4$  is used, regression models will mostly eliminate the bias, but will also add additional variability unless at least a 20-day period is used for the regression.
2. Use a full-season regression model without adjustment. This method is essentially unbiased and has minimal variability for weather-sensitive accounts. The practical

difficulty is waiting until a full season of data are available, or relying on a previous season. In addition, if operating practices have changed since the previous season, or change within the current season, the full-season model may not be a good representation of load on the curtailment day.

3. Use the “High 5 of 10” average with THI adjustment. This adjustment is not dependent on actual behavior in the hours immediately before curtailment. As a result, it is subject neither to manipulation by the customer nor to severe distortion due to curtailment in advance of the required time, nor to inflation due to pre-cooling. This combination has variability no worse than that of unadjusted averages, and for low-variability weather-sensitive accounts, it is essentially unbiased. For non-weather-sensitive accounts, it produces some positive bias and increases variability compared to unadjusted averages.

The THI adjustment for this analysis was based on a full season of load and weather data from the season in which the curtailment occurred. Actual implementation of the THI adjustment by PJM requires the THI regression would be based on a full season of data from the previous year or a minimum of a month of data from the current season.

Practical considerations are the following.

- It either requires load history from the prior year or must rely on shorter data spans from the ongoing season.
- Using previous year data, if the load pattern has changed it can produce erroneous results. Using limited data from earlier in the summer, regression results may be forced to make predictions outside of the range of the data.
- It involves an adjustment that is difficult to explain succinctly and may be difficult to understand.

## 6.4 RECOMMENDATIONS

The choice of a baseline method needs to balance a number of practical considerations as well as prediction accuracy. These considerations, listed at the beginning of this section, are:

- simplicity of calculation
- minimizing burden on participants and operators, in terms of costs, ease of understanding, and ease of operation
- limiting the potential for gaming
- limiting the potential for distortion if load is curtailed early
- ability to know the baseline immediately after a curtailment
- ability to know the baseline before making a curtailment decision
- minimizing method bias: systematic tendency to over- or under-state
- minimizing method variability: tendency to wide swings in estimates.

Different methods are appropriate for different types of accounts, and according to the importance assigned to each of the above considerations. In developing our recommendations, we did not attempt to score each method or feature with respect to each of these criteria or assign explicit weights to the criteria. In general, our approach is

1. allow for options that recognize different circumstances
2. favor simplicity if the potential accuracy gains of greater complexity appear to be slight
3. indicate alternatives and trade-offs with respect to the criteria.

### ***Adjustments***

For almost all basic methods, an additive adjustment to the two hours prior to curtailment can reduce both bias and variability. The problems with this approach are the potential for gaming, and the potential for understatement of load reduction if a customer curtails prior to the formal curtailment period. The additive adjustment to the last 2 hours should be considered as an option for accounts that are considered unlikely to be subject to either of these distortions.

For weather-sensitive accounts, alternatives to this adjustment include:

- PJM's High-five average with THI adjustment
- Adjust to the third and fourth hour prior to curtailment.
- For summer loads, weather model using a full season of data, with no adjustment.

In general, scalar and additive adjustments perform similarly well, except that scalar adjustments sometimes blow up resulting in higher variability. If scalar adjustments are used, some procedure to avoid extreme adjustment ratios should be incorporated. On the other hand,

additive adjustments can produce negative baselines; the baseline should be truncated at zero if additive adjustments are used.

### ***Weather Modeling***

If more complex methods are acceptable, weather models are recommended for summer weather-sensitive accounts. Weather models may also be useful for winter weather-sensitive accounts, but are not as clearly superior to simple averages, particularly if adjustments to the current day are also used. As noted in Section 4, weather models with a variable degree-day base would be expected to perform somewhat better than those tested in this study; that improved performance might justify the greater complexity.

No single model structure offers a clear preference for all situations. Models relying on daily temperature or degree-day variables appear to perform as well as those using hourly weather inputs. However, these models are likely to behave less well on days when there are unusual changes in the weather, or in regions where such changes are likely. Likewise, models incorporating humidity and/or lag degree-day variables did not perform better across the cases examined in this study, but these terms may be important for some regions and customer types.

If weather models are used, screening criteria should be included to eliminate weather terms that are not statistically significant or physically meaningful for a particular account. This screening can be done once, at the beginning of the curtailment season or at initial enrollment in a program, and may be based on a full season of data if available. Without such screening, high variability can result for some accounts. Use of such screening procedures can allow a single general procedure, including this screening, to be applied to all accounts, without pre-classifying the accounts by weather sensitivity. Even if the weather modeling is restricted to accounts believed to be weather-sensitive, use of the screening procedure can still eliminate extreme anomalous results.

Models based on a full season of data tend to be more reliable than those based on shorter periods. However, waiting until the season has ended to determine baselines is impractical for most programs. Models based on the previous 20 business days perform slightly better than those based on the previous 10. In most cases, the difference is not dramatic, but reliance on only 10 days of data will increase the potential for anomalous events to skew results.

An alternative to using an additive or scalar adjustment after applying the weather model is to include load at hours just before curtailment as predictors in the model. This approach was not tested in the study but should be considered.

### ***Averages***

If simpler models are a priority, hourly averages with adjustment to the hours prior to curtailment can be used with good results even for weather-sensitive accounts. For non-weather-sensitive accounts, averaging methods make more sense than weather models. However, adjustment to

hours prior to curtailment, subject to the concerns discussed above, can improve method performance for both types of account. With this adjustment, averages based on different selection rules (last 10, last 11, highest 10 of last 11, highest 5 of last 10, or last 20) tend to perform similarly. For summer loads, the High 5 of 10 average with additive adjustment performed somewhat better than averages using other selection rules. Averages based on a full season can do somewhat better, if this much delay in results is acceptable.

### ***Proposed Approaches by Account Type***

#### **Offering Options**

A general recommendation is that baseline calculation protocols should provide for alternatives based on customer account types and operating practices. One way to simplify the provision of options is to establish a default method, and allow certain deviations.

The basis for the selection of method should be not just the business type, but also the load patterns evident in the data as well as the customer's description of operating practices. Thus, for example, a customer who indicates a desire to be able to cancel a shift in advance of the control period should have access to a baseline calculation method that is not distorted by this practice.

At the same time, the program operator should have some discretion to bar customers from using an approach that they appear to have manipulated in the past. Thus, if there is evidence that a particular customer tends to inflate load after notification, beyond what would reasonably be expected for pre-cooling, that customer might not be able to use a method that includes adjustment to the two pre-curtailment hours.

#### **A Practical Default Baseline Calculation Method**

A method that generally works well for a range of account types is the simple average of the last 10 days, with additive adjustment to the two hours prior to the curtailment period. This method can be recommended for both weather-sensitive and non-weather-sensitive accounts, with both low and high variability, for summer and nonsummer curtailments.

This method is not recommended for accounts that tend to begin load curtailment substantially in advance of the formal curtailment period. It is also not recommended for situations where the potential for gaming is a strong concern, whether across the program or for particular customers.

#### **Alternatives for Summer Weather-Sensitive Accounts**

For summer programs, practical alternatives for weather-sensitive accounts include the following:

- unadjusted weather models. Longer input time periods are preferable, particularly for high-variability accounts
- the High 5 of 10 average with THI adjustment.

Simpler methods with less desirable but potentially acceptable performance include

- Unadjusted averages, particularly the High 5 of 10
- Averages or weather models adjusted to the third and fourth hour before curtailment.

#### **Alternatives for Summer Non-Weather-Sensitive Accounts**

For non-weather-sensitive summer accounts, the unadjusted High 10 of 11 average performs nearly as well as the recommended default, particularly for low-variability accounts. Next best is the simple average of the last 10 days with additive adjustment to the third and fourth hours before curtailment.

For low-variability accounts, unadjusted weather models, with weather terms retained only if indicated by the data, actually perform slightly better than the recommended default. However, unlike the case for weather-sensitive accounts, these models perform better if based on shorter periods of data. For high-variability accounts, unadjusted weather models tend to be worse than the unadjusted high 10 of 11 average.

#### **Alternatives for Nonsummer Accounts**

For nonsummer accounts, modeling is more challenging and there are fewer alternatives. For weather-sensitive accounts, the High 5 of 10 average with THI adjustment can be used. For low-variability accounts, the unadjusted High 5 of 10 average appears to perform slightly better, but for high-variability accounts it is worse.

For non-weather-sensitive nonsummer accounts, the unadjusted High 10 of 11 appears to be the best alternative. Any of the averages with additive adjustment to the third and fourth hour before curtailment perform not quite as well.

#### **Summary of Recommended Methods and Alternatives**

The recommended methods, alternatives, and operational considerations for different account types are summarized in Table 6-3.

**Table 6-3  
Recommended Methods and Alternatives**

Season	Weather Sensitivity	Variability	Recommended Default			Recommended Alternatives		
			Estimation	Data Selection	Adjustment	Estimation	Data Selection	Adjustment
Summer	Weather-Sensitive	Low	Average	last 10	add 1-2	weather models	any	none
						Average	High 5	THI
Summer	Weather-Sensitive	High	Average	last 10	add 1-2	weather models	longer is better	none
						Average	High 5 of 10	THI
Summer	Non-Weather-Sensitive	Low	Average	last 10	add 1-2	weather models	shorter is better	none
						Average	High 10 of 11	none
						Average	last 10	add 3-4
Summer	Non-Weather-Sensitive	High	Average	last 10	add 1-2	Average	High 10 of 11	none
						Average	last 10	add 3-4
Nonsummer	Weather-Sensitive	Low	Average	last 10	add 1-2	Average	High 5 of 10	none
Nonsummer	Weather-Sensitive	High	Average	last 10	add 1-2	Average	High 5 of 10	THI
Nonsummer	Weather-Sensitive	Low	Average	last 10	add 1-2	Average	High 10 of 11	none
						Average	last 10	add 3-4
Nonsummer	Weather-Sensitive	High	Average	last 10	add 1-2	Average	High 10 of 11	none
						Average	last 10	add 3-4

## 6.5 AREAS FOR FUTURE DEVELOPMENT

Reviewers of a draft of this report offered a number of valuable suggestions. Many of these suggestions have been incorporated in the final version. Others, while of considerable merit, were beyond the scope of what could be accomplished in this study.

Most of the suggestions that could not be addressed were in the following categories:

1. Test additional methods
2. Examine results by finer categories of customer type
3. Provide more explicit rules and clear-cut bases for choosing among alternatives, including methods for identifying gaming.

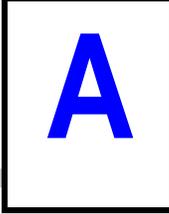
These issues will be explored in further work by the IPMVP Technical Committee. The committee will be building on this study to develop a DR baseline protocol that can be adopted as part of the IPMVP document. The Protocol itself will include the establishment of consistent terminology, guidance on appropriate methods for different situations, and rationale for that guidance. The technical analysis that forms a major portion of this report will not itself be part of the Protocol, but will be referenced as part of the rationale for the guidance.

As part of the further work by the IPMVP, some additional methods may be tested. Candidates for testing include:

- ASHRAE load forecasting models
- variable degree-day models
- use of a single hour or two hours prior to curtailment as a flat baseline.

The additional testing may also examine results by finer segments. Customer type is not known for most of the data sets examined in this study. However, customers can be classified by size, and possibly by other patterns in the load data.

An IPMVP Protocol by its nature will offer options and guidance rather than being prescriptive. However, this Protocol can serve as the basis for establishing specific rules and procedures within a jurisdiction, and provide a common language for understanding these procedures.



## ***DESCRIPTION OF METHODS REVIEWED***

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### **A.1 CA ISO SUMMER 2001 DRP – FIRST RFP BASELINE METHOD TYPE<sup>1</sup>**

**Data Selection Criteria:**

**Time Frame** Immediately preceding 10 business days.

**Exclusions** Control days.

**Extensions** None.

**Estimation Method:** Interval averages.

**Adjustment Methods:** None.

### **A.2 CA ISO SUMMER 2001 DRP – SECOND RFP BASELINE METHOD TYPE<sup>1</sup>**

**Data Selection Criteria:**

**Time Frame** Top 10 of immediately preceding 11 business days.

**Exclusions** Control order or request days, days of involuntary service interruptions, single day with lowest event period usage.

**Extensions** None.

**Estimation Method:** Interval averages.

**Adjustment Methods:** None.

### **A.3 CALIFORNIA MANUFACTURERS AND TECHNOLOGY ASSOCIATION (CMTA) PROPOSED OPTIONAL BINDING MANDATORY CURTAILMENT (OBMC) PLAN<sup>2</sup>**

**Data Selection Criteria:**

**Time Frame** Immediately preceding 10 business days.

**Exclusions** Control days.

**Extensions** None.

**Estimation Method:** Interval averages.

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<sup>1</sup> Second Request for Bids to Provide Demand Relief (Load) for Summer 2001, March 30, 2001, California Independent System Operator Corporation, <http://www.caiso.com/docs/2001/03/30/2001033009195918940.pdf>.

<sup>2</sup> CMTA's Proposed Program Details For OBMC Pilot Program (R.00-10-002)

**Adjustment Methods:** Additive adjustment using hours h-1 through h-4.

#### A.4 NY ISO 2001 DADRP/EDRP BASELINE METHOD<sup>3</sup>

**Data Selection Criteria:**

**Time Frame** Top 5 of previous 10 business days, starting n-2.

**Exclusions** Before counting begins – Immediately preceding day (if weekday).

AFTER ten previous weekdays identified – Exclude Emergency DR program days and days on which a Day-Ahead DR program bid was accepted. Exclude all days not in top five of average event period usage.

AFTER top 5 average usage days chosen – Exclude included day if found to have 4 consecutive hours within the hours of implementation that have usage less than 75% of the average of the top 5 for each of those hours.

**Extensions** If fewer than 5 days are available after exclusions then eligible days are considered in reverse chronological order starting with day n-12 and with respect to all above exclusions. Only days within 30 days of the event may be considered. If there are not five eligible days in the last 30 days, the baseline load is calculated as an average of those eligible days that do exist.

**Estimation Method:** Interval averages.

**Adjustment Methods:** None.

#### A.5 NY ISO 2002 DADRP/EDRP BASELINE METHOD<sup>4</sup>

**Data Selection Criteria:**

**Time Frame** Top 5 of previous 10 business days, starting n-2.

**Exclusions** Immediately preceding day (if weekday), Emergency DR program days, days on which Day-Ahead DR program bid was accepted and low usage days. Days are added to the 10 day basis incrementally. The first weekday added (n-2, unless otherwise excluded) must have average daily event period usage greater than 25% of peak hourly load of the previous month, otherwise it is excluded as a low usage day. Subsequent days added to the basis must have average daily event period usage e greater than 25% of the average event period usage of the days already included in the basis.

Exclude all but 5 highest average daily event period usage days.

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<sup>3</sup> NYISO Day-Ahead Demand Response Program Manual. Revised May 24,2001. New York Independent System Operator.

<sup>4</sup> NYISO Day-Ahead Demand Response Program Manual. Revised March 13, 2002. New York Independent System Operator.

**Extensions** Basis should include 10 days unless there are fewer than 10 eligible days in the last thirty days.

**Estimation Method:** Interval averages.

**Adjustment Methods:** Optional Scalar adjustment using hours h-3 and h-4. Scalar is bound between .8 and 1.2.

## A.6 PJM ECONOMIC LOAD RESPONSE 2002<sup>5</sup>

**Data Selection Criteria:**

**Time Frame** Top 5 of previous 10 business days.

**Exclusions** Immediately preceding day (if weekday), PJM-declared control event day, days on which Day-Ahead DR program bid was accepted.

AFTER ten day basis has been created based on the above exclusions low input days are removed. Day is low input if average daily event usage is less than 75% of ten day event period usage. Low input days are replaced and process repeated.

Exclude all but 5 highest average daily event period usage days.

**Extensions** Basis should include 10 days unless there are fewer than 10 eligible days in the last thirty days.

**Estimation Method:** Interval averages.

**Adjustment Methods:** Optional Temperature-Humidity Index based (THI) scalar adjustment. A simple linear regression is fit with peak hour load as a function of the THI. Using the estimated intercept and slope, load can be estimated with a THI value. The adjustment uses an estimate of load based on the average control day peak hour THI and an estimate of load based on the baseline day peak hour average THI. It is the ratio of the control day estimated load over the baseline day estimated load.

To do the THI adjustment, a minimum of one month of load data from the present season is required. If available a full previous season data set is used.

## A.7 PJM EMERGENCY LOAD RESPONSE 2001/2002<sup>6</sup>

**Data Selection Criteria:**

**Time Frame** Hour before.

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<sup>5</sup> PJM Economic Load Response Program . Issued March 15th, 2002. Fourth Revise Volume No. 1.

<sup>6</sup> PJM 2001-2002 Load Response Pilot Program.

**Exclusions** None.

**Extensions** None.

**Estimation Method:** None.

**Adjustment Methods:** None.

## A.8 LBNL/KINNEY BASELINE METHOD TYPE<sup>7</sup>

### **Data Selection Criteria:**

**Time Frame** Previous ten days.

**Exclusions** Control days.

**Extensions** None.

**Estimation Method:** Explanatory model.

**Predictors** Average or maximum daily temperature.

**Time period Specificity** Hourly load data with daily temperature data.

**Estimation Criterion** OLS.

### **Full Model Specification**

$$L_{dh} = a_h + b_h T_d,$$

where  $L_{dh}$  is hourly load from the ten previous non-controlled business days.  $T$  is either average or maximum temperature.  $a_h$  and  $b_h$  are estimated parameters. Separate regression run for each hour.

**Adjustment Methods:** None.

## A.9 ISO NEW ENGLAND BASELINE METHOD TYPE<sup>8</sup>

### **Data Selection Criteria:**

**Time Frame** 10 previous business days.

**Exclusions** Control days are excluded AFTER selection of 10 previous days.

Shutdown days are days included in baseline average with 4 consecutive hours for which hourly load is either less than 75% or greater than 125% of the hourly baseline load for each hour.

**Extensions** If fewer than 7 days for average, days are considered in reverse chronological order until there are 7 eligible weekdays in the simple average.

**Estimation Method:** Interval averages.

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<sup>7</sup> Kinney, Saki, Lawrence Berkeley National Laboratory. Personal communication.

<sup>8</sup> DRAFT ISO-NE Load Response Program Manual. 05-07-2002.

**Adjustment Methods:** Additive adjustment using hours h-1 and h-2.

## A.10 XENERGY WEATHER BASELINE METHOD TYPE

**Data Selection Criteria:**

**Time Frame** Minimum of one previous month (flexible).

**Exclusions** Weekends and holidays, Control days.

**Extensions** None.

**Estimation Method:** Explanatory model.

**Predictors** Heating and cooling degree days.

**Time period Specificity** Hourly load, cooling degree days based on daily average.

**Estimation Criterion** OLS, R-squared optimized over cooling degree base choices.

**Full Model Specification**

$$L_{dh} = \sum_{h=1}^{24} a_h D_h + \sum_{h=1}^{24} b_h D_h CDD_d + \sum_{h=1}^{24} c_h D_h HDD_d$$

where  $L_{dh}$  = load,  $CDD$  and  $HDD$  are cooling and heating degree days, respectively,  $D$  = Data time frame,  $a$  and  $b$  are estimated regression parameters.

**Adjustment Methods:** Additive adjustment using hours h-1 and h-2.

## A.11 NEXANT BASELINE METHOD TYPE

**Data Selection Criteria:**

**Time Frame** Immediately preceding 10 business days.

**Exclusions** Control days.

**Extensions** None.

**Estimation Method:** Interval averages.

**Adjustment Methods:** Scalar adjustment using hour h-1.

## A.12 UTILITY A – MATCH DAY

**Data Selection Criteria:**

**Time Frame** Previous Month.

**Match Criteria** Demand based (i.e. high demand days), or weather based (>75 degrees).

**Exclusions** Weekends and holidays, Control days.

**Extensions** If insufficient match days are found in previous month, match criteria is made more inclusive (i.e. high and medium demand days or >70 degrees).

**Estimation Method:** Interval averages.

**Adjustment Methods:** Scalar adjustment using one hour between 8am and 11am.

### **A.13 UTILITY B**

**Data Selection Criteria:**

**Time Frame** Previous five business days.

**Exclusions** Control days.

**Extensions** None.

**Estimation Method:** Interval averages.

**Adjustment Methods:** None.

### **A.14 UTILITY C – REGRESSION-BASED**

**Data Selection Criteria:**

**Time Frame** Flexible.

**Exclusions** Control days.

**Extensions** None.

**Estimation Method:** Multiple explanatory models.

**Predictors** Weather Parameters.

**Time period Specificity** Hourly load, hourly weather parameters.

**Estimation Criterion** Unknown. Model is a structural time series model.

**Full Model Specification** Actual specification is unknown. The approach has two steps. First, mean hourly load over the event period is estimated with the structural time series model.

Second, the Haar transform is used to estimate the load shape within the 8-hour event period conditional on average load.

**Adjustment Methods:** None.

### **A.15 UTILITY D**

**Data Selection Criteria:**

**Time Frame** June through September.

**Exclusions** Weekends, control days.

**Extensions** None.

**Estimation Method:** Explanatory model.

**Predictors** Lagged dry bulb temperature, 5am to 10am average load.

**Time period Specificity** Hourly load, hourly lagged dry bulb temperature.

**Estimation Criterion** OLS.

**Full Model Specification**

$$L_{dh} = a_h + b_h AMK_d + c_h LgDB_h$$

where  $L_{dh}$  is hourly load, June through September,  $AMK_d$  is the average load between 5am and 10am for that day, and  $LgDB_h$  is a lagged temperature measure.  $a_h$ ,  $b_h$  and  $c_h$  are estimated parameters. Separate regressions are estimated for each hour.

**Adjustment Methods:** None.

## A.16 UTILITY E

**Data Selection Criteria:**

**Time Frame** Full year.

**Match day Criteria** Match ten day-pairs to the control day day-pair. Control day day-pair consists of control day hours prior to event and the whole prior day. Ten days with the lowest sum of square errors relative to the control day pair are included in baseline calculation.

**Exclusions** None.

**Extensions** None.

**Estimation Method:** Interval averages.

**Adjustment Methods:** Control day-pair loads are regressed on their baseline counterparts.

$$L_{dq} = a_q + b_q L_{Dq}$$

where  $L_{dq}$  is fifteen-minute interval load during the control day-pair period and  $L_{Dq}$  is the average fifteen-minute interval load over the baseline day-pairs.  $a_q$  and  $b_q$  are estimated parameters. If the regression explains 50% of the variation (R-squared > .5) then the fit values for the control period hours are used as the baseline.

## A.17 UTILITY F

**Data Selection Criteria:**

**Time Frame** Previous two years.

**Match Criteria** Certain hot days.

**Exclusions** Anomalous loads.

**Extensions** None.

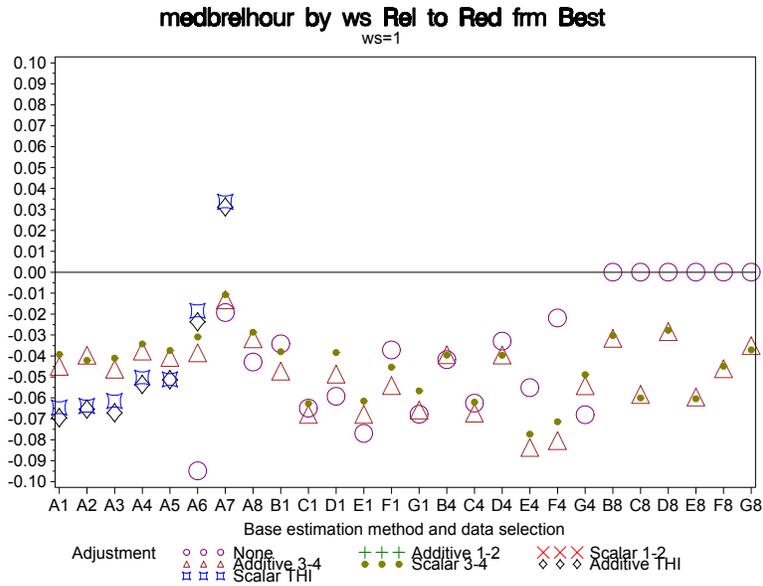
**Estimation Method:** Interval averages.

**Adjustment Methods:** Scalar adjustment using hours h-1 and h-2.

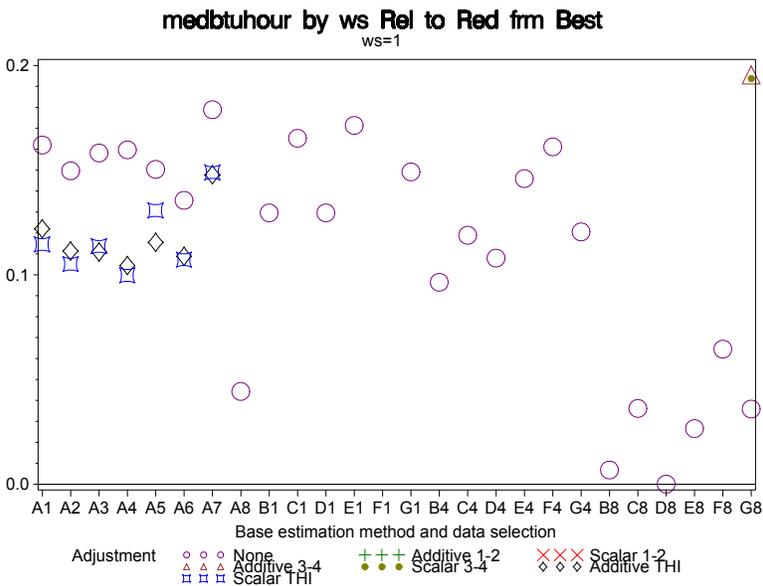
# B

## PERFORMANCE RELATIVE TO CURTAILMENT AMOUNT

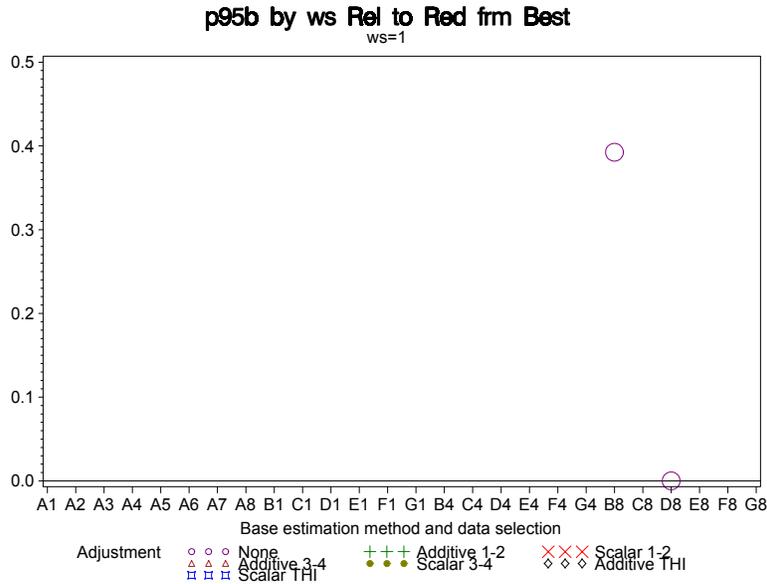
**Figure B-1**  
**Median Relative Hourly Error**  
**Summer Curtailed Weather-Sensitive Low-Variability Accounts**



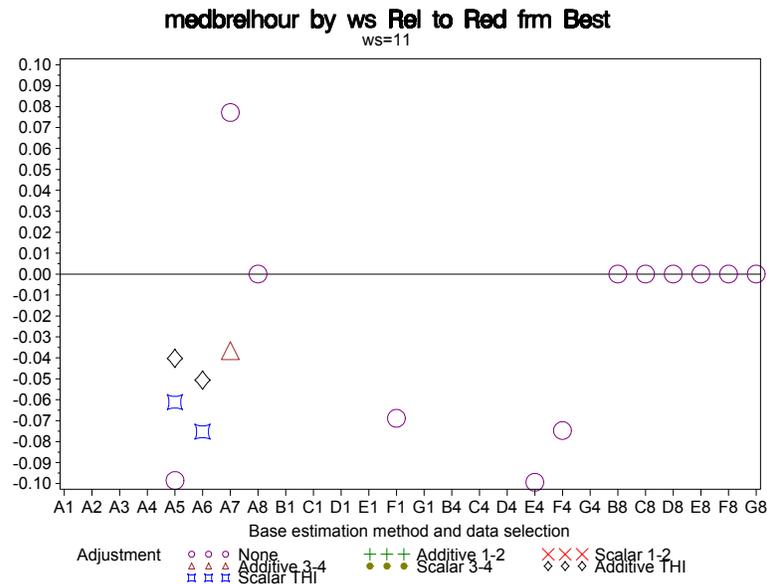
**Figure B-2**  
**Median Account Theil's U**  
**Summer Curtailed Weather-Sensitive Low-Variability Accounts**



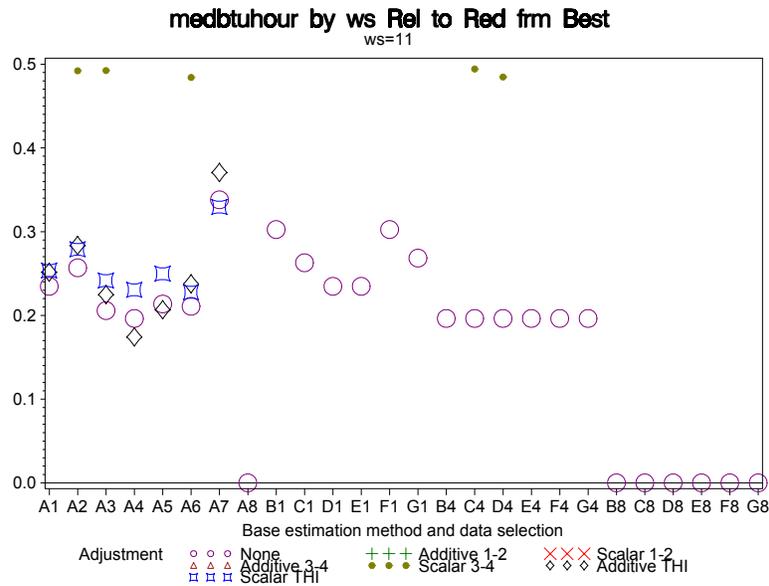
**Figure B-3**  
**95<sup>th</sup> Percentile Account Theil's U**  
**Summer Curtailed Weather-Sensitive Low-Variability Accounts**



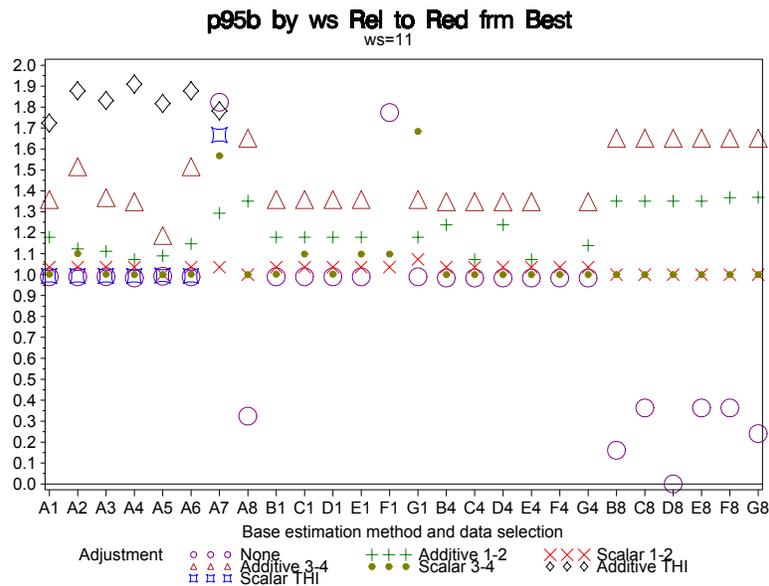
**Figure B-4**  
**Median Relative Hourly Error**  
**Summer Curtailed Weather-Sensitive High-Variability Accounts**



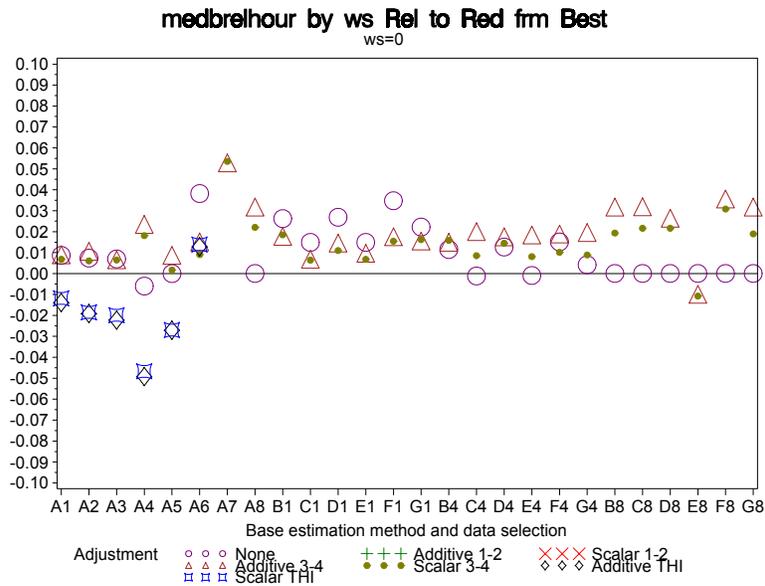
**Figure B-5**  
**Median Account Theil's U**  
**Summer Curtailed Weather-Sensitive High-Variability Accounts**



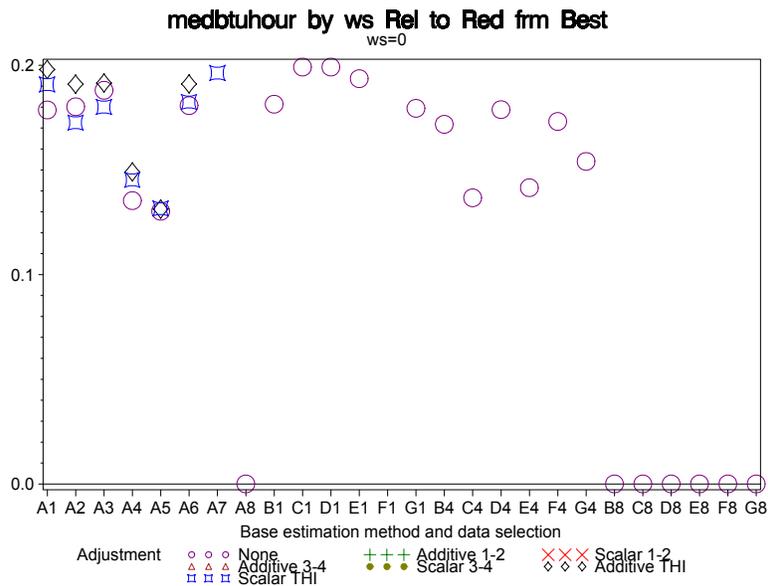
**Figure B-6**  
**95<sup>th</sup> Percentile Account Theil's U**  
**Summer Curtailed Weather-Sensitive High-Variability Accounts**



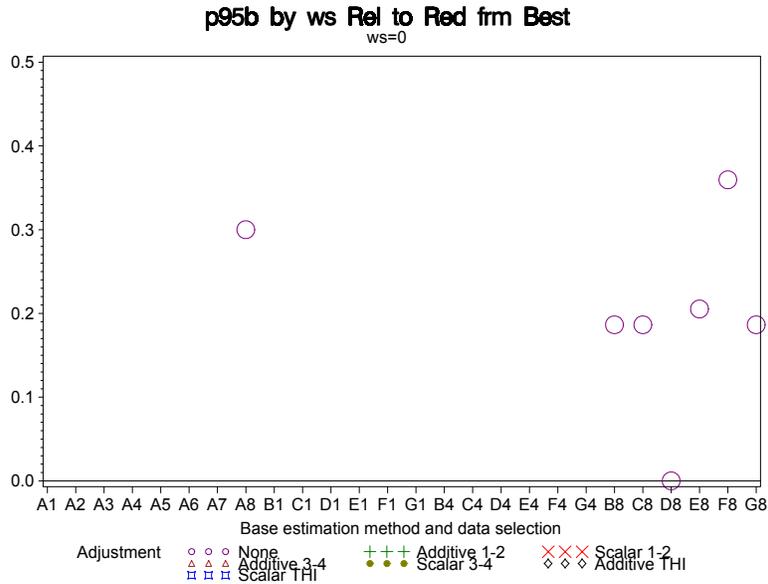
**Figure B-7**  
**Median Relative Hourly Error**  
**Summer Curtailed Non-Weather-Sensitive Low-Variability Accounts**



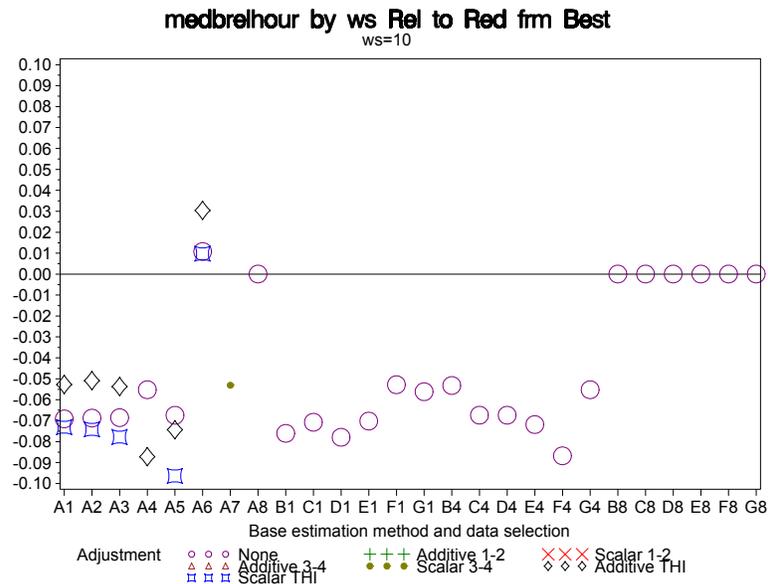
**Figure B-8**  
**Median Account Theil's U**  
**Summer Curtailed Non-Weather-Sensitive Low-Variability Accounts**



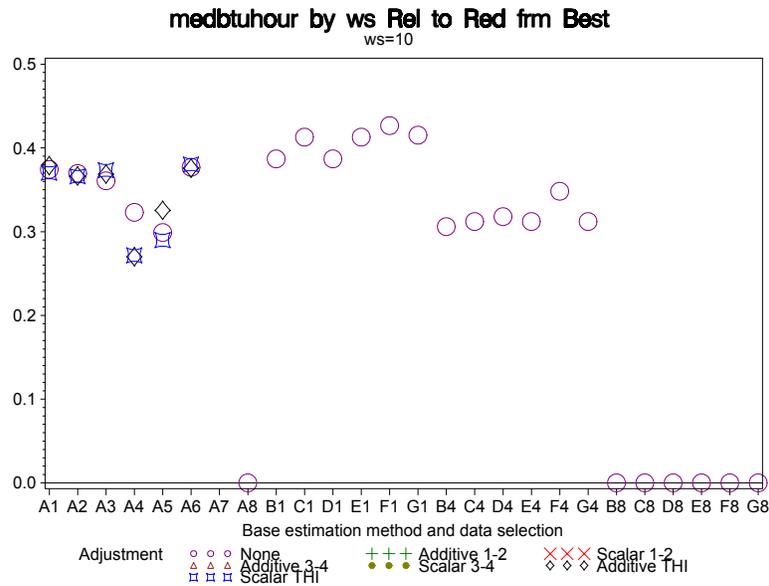
**Figure B-9**  
**95<sup>th</sup> Percentile Account Theil's U**  
**Summer Curtailed Non-Weather-Sensitive Low-Variability Accounts**



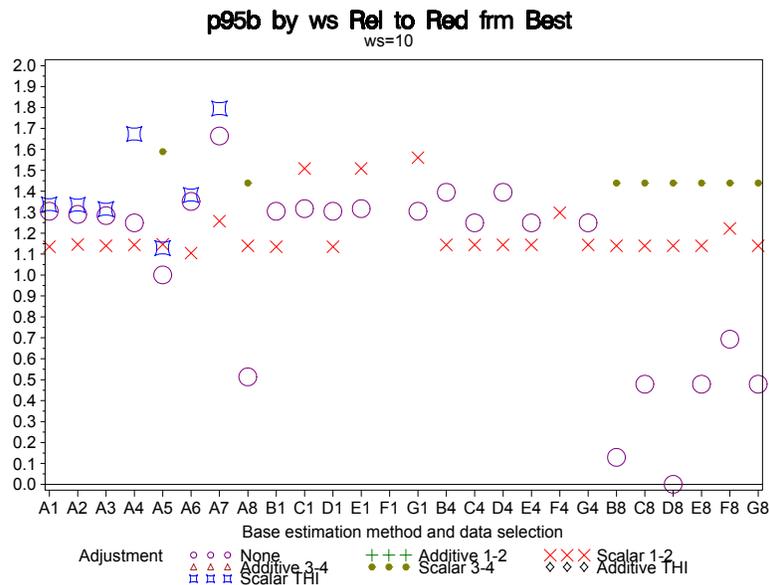
**Figure B-10**  
**Median Relative Hourly Error**  
**Summer Curtailed Non-Weather-Sensitive High-Variability Accounts**



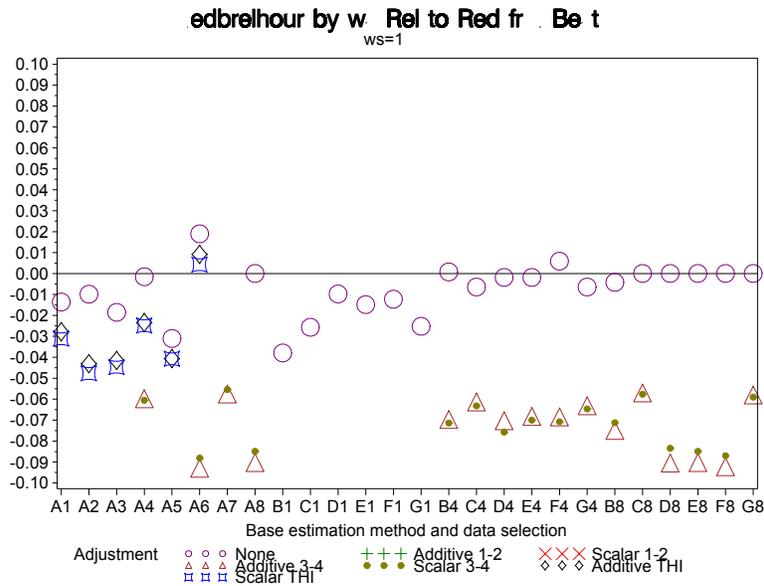
**Figure B-11**  
**Median Account Theil's U**  
**Summer Curtailed Non-Weather-Sensitive High-Variability Accounts**



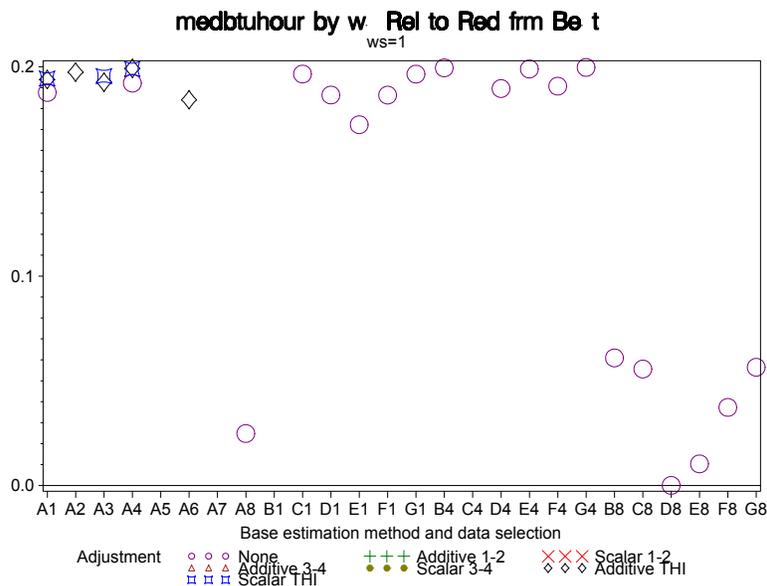
**Figure B-12**  
**95<sup>th</sup> Percentile Account Theil's U**  
**Summer Curtailed Non-Weather-Sensitive High-Variability Accounts**



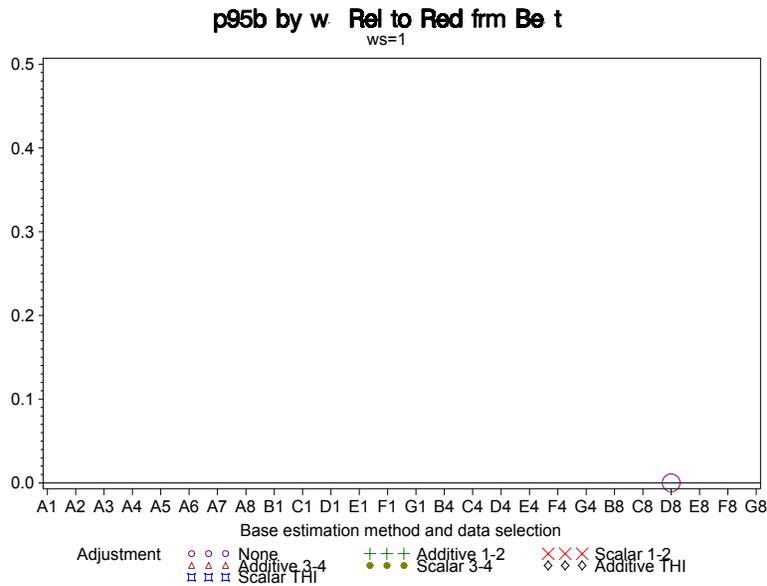
**Figure B-13**  
**Median Relative Hourly Error**  
**Nonsummer Curtailed Weather-Sensitive Low-Variability Accounts**



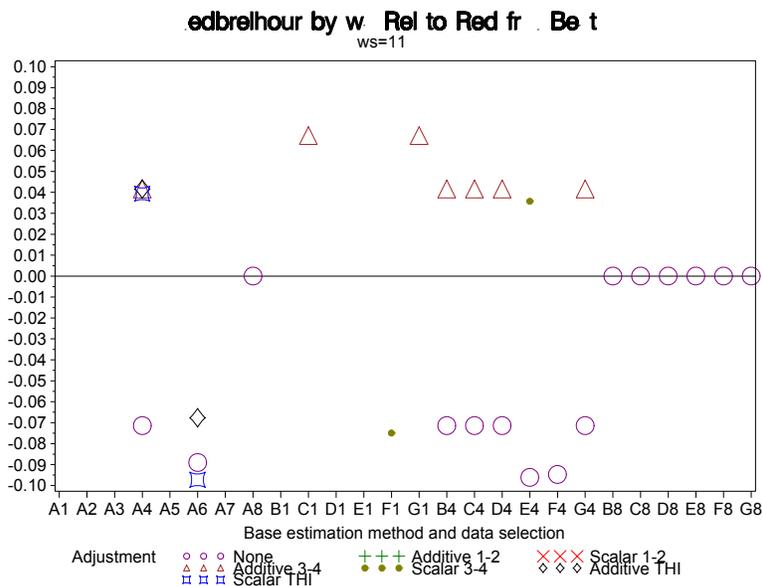
**Figure B-14**  
**Median Account Theil's U**  
**Nonsummer Curtailed Weather-Sensitive Low-Variability Accounts**



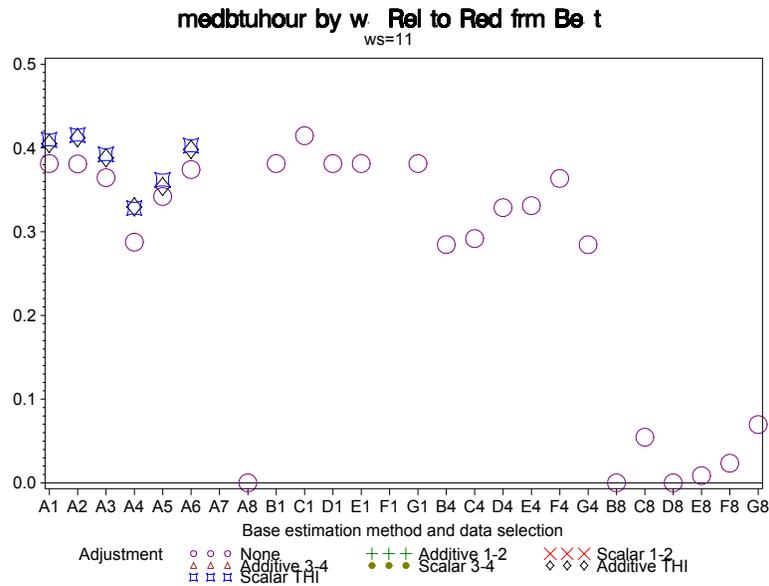
**Figure B-15**  
**95<sup>th</sup> Percentile Account Theil's U**  
**Nonsummer Curtailed Weather-Sensitive Low-Variability Accounts**



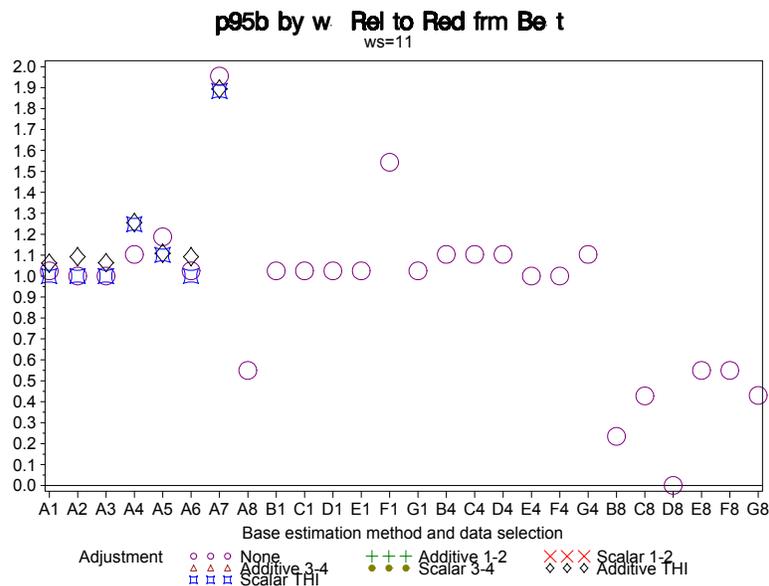
**Figure B-16**  
**Median Relative Hourly Error**  
**Nonsummer Curtailed Weather-Sensitive High-Variability Accounts**



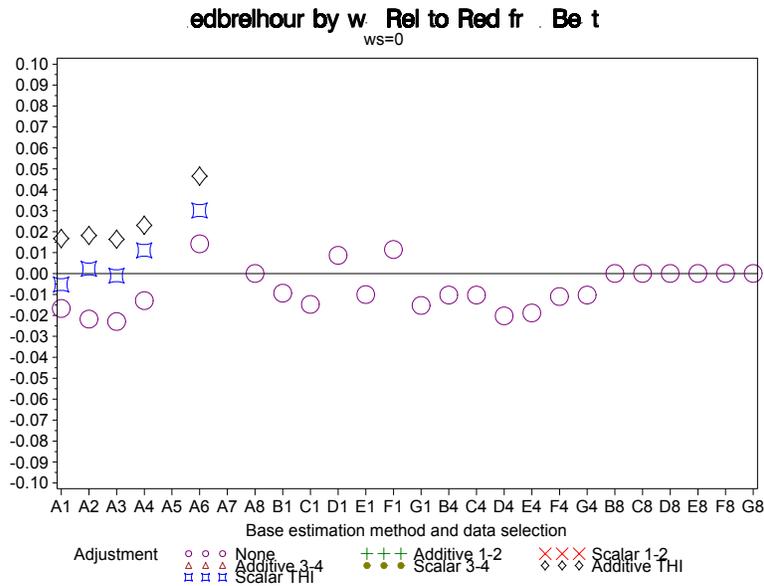
**Figure B-17**  
**Median Account Theil's U**  
**Nonsummer Curtailed Weather-Sensitive High-Variability Accounts**



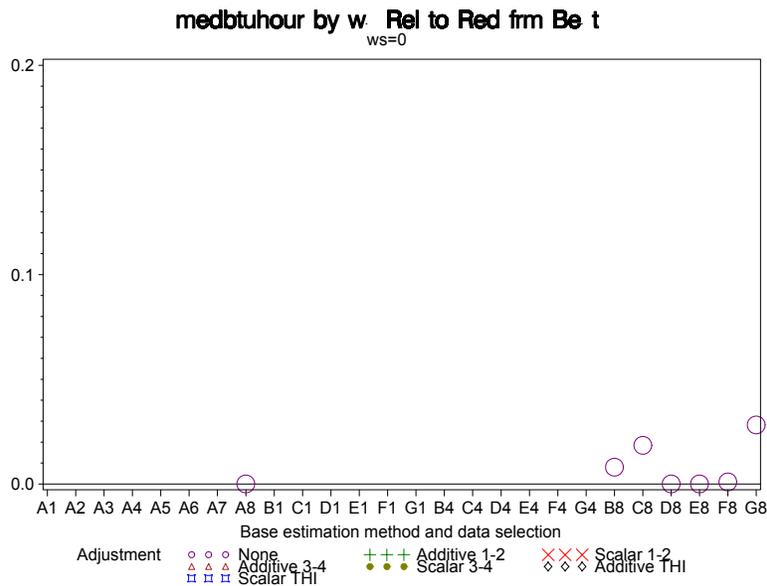
**Figure B-18**  
**95<sup>th</sup> Percentile Account Theil's U**  
**Nonsummer Curtailed Weather-Sensitive High-Variability Accounts**



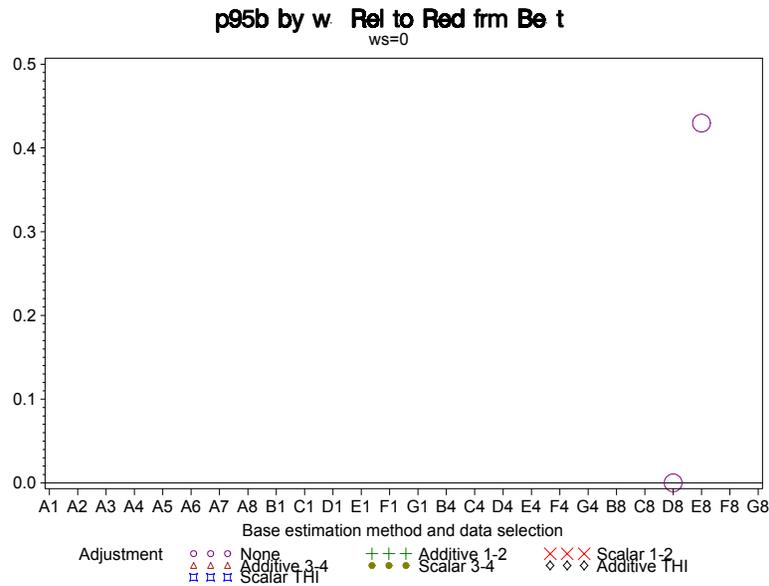
**Figure B-19**  
**Median Relative Hourly Error**  
**Nonsummer Curtailed Non-Weather-Sensitive Low-Variability Accounts**



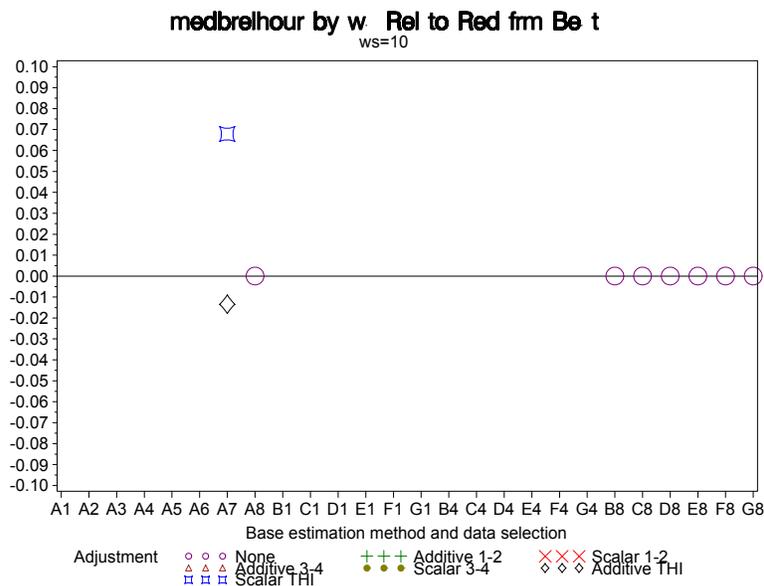
**Figure B-20**  
**Median Account Theil's U**  
**Nonsummer Curtailed Non-Weather-Sensitive Low-Variability Accounts**



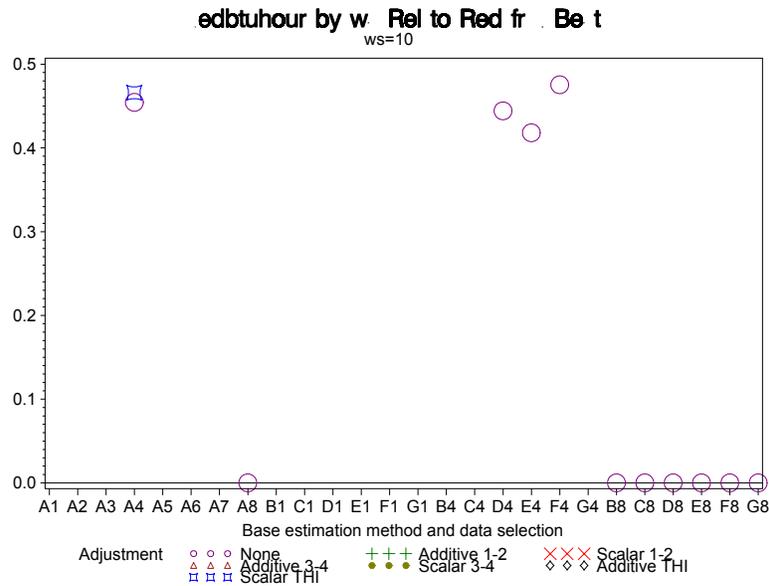
**Figure B-21**  
**95<sup>th</sup> Percentile Account Theil's U**  
**Nonsummer Curtailed Non-Weather-Sensitive Low-Variability Accounts**



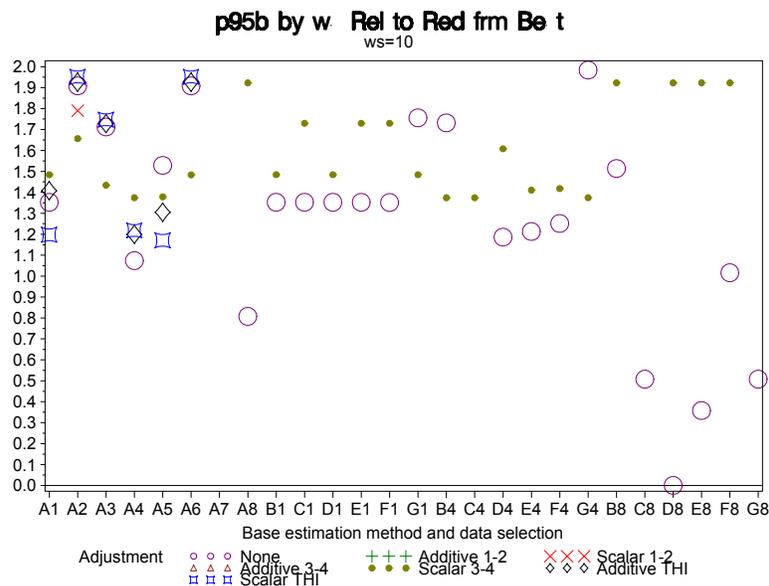
**Figure B-22**  
**Median Relative Hourly Error**  
**Nonsummer Curtailed Non-Weather-Sensitive High-Variability Accounts**

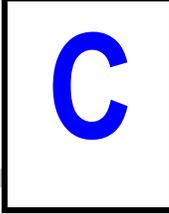


**Figure B-23**  
**Median Account Theil's U**  
**Nonsummer Curtailed Non-Weather-Sensitive High-Variability Accounts**



**Figure B-24**  
**95<sup>th</sup> Percentile Account Theil's U**  
**Nonsummer Curtailed Non-Weather-Sensitive High-Variability Accounts**





**Additive adjustment:** An adjustment method by which a fixed amount is added to the provisional baseline load in each interval.

**Adjustment method:** An additive or scalar adjustment to a provisional baseline as the final step in a baseline calculation methodology.

**Averaging:** A baseline estimation method whereby the provisional baseline for each hour (or finer interval) of the day is the simple average, over all days used in the estimation, of the load at that hour.

**Baseline Calculation Methodology:** A set of procedures for calculating a CBL. In this document, a baseline methodology is defined by an estimation method, a set of data selection criteria, and an adjustment method.

**Bias:** Systematic tendency of an estimation to over- or under-state the true value. Technically, the expected value of the difference between the estimate and the true value. In this study, the median relative hourly error is used as the measure of bias.

**CA ISO:** The California ISO.

**CBL:** Customer baseline.

**Control period:** Curtailment period.

**Curtailed account:** In this study, an account that had one or more actual curtailment periods during the time span of the data available for the study.

**Curtailment period:** A period during which DRP participants would have been required or incented to reduce demand.

**Curtailment:** Demand response.

**Customer Baseline (CBL):** In a demand-response program, the load level for a particular customer for each interval of a curtailment period, compared to which demand reduction in each interval is calculated. The customer's demand reduction in each interval is calculated as the difference between the customer's CBL and its metered load.

**Data selection criteria:** The rules and process for selecting the days and intervals that will be included in calculating the CBL.

**Demand Reduction:** Demand response.

**Demand Response (DR):** Reducing demand in response to a curtailment notification or short-term price signal. Also, the magnitude of the reduction, in kW.

**Demand Response Program (DRP):** A program operated by an electric utility, ISO, energy service company, or retail energy supplier to encourage end-use customers to reduce their peak loads on short notice (under two to 24 hours) in exchange for some form of compensation.

**DR:** Demand response.

**Estimation method:** The calculations applied to a set of data to determine the CBL, after the selection of included and excluded data points, and before any adjustment is applied.

**Free Ridership:** Obtaining incentive payments for load reductions that would have taken place without the program.

**Gaming:** Altering behavior to manipulate a baseline to the advantage of the customer.

**High variability:** A characteristic of an account, indicating that the load at a given hour of the day exhibits high variation from one uncontrolled business day to the next.

**Independent System Operator:** The regional electric grid operator, particularly in markets that have been opened to retail electric competition.

**International Performance Measurement and Verification Protocol (IPMVP):** A set of documents providing guidance on methods for quantifying the long-term results of energy efficiency projects. Also, the organization responsible for the continued development of the concept of standardized verification methods, distribution of the documents, and providing guidance and training on the appropriate use of the documents.

**IOU:** Investor-Owned utility.

**IPMVP:** International Performance Measurement and Verification Protocol.

**ISO:** Independent System Operator.

**ISO-NE:** The New England ISO.

**Load type:** In this report, a classification of an account according to whether or not it is weather-sensitive and whether it has high or low variability.

**Low-variability load:** A characteristic of an account, indicating that the load at a given hour of the day exhibits low variation from one uncontrolled business day to the next.

**M&V:** Measurement and verification.

**Measurement and Verification (M&V):** the procedures used to determine savings in programs where compensation is paid based on the achieved savings.

**Nonsummer:** The months October through May.

**Non-weather-sensitive:** A characteristic of an account, indicating that the load variations are not related to weather conditions.

**NYISO:** The New York ISO.

**PJM:** The Pennsylvania, New Jersey, Maryland ISO.

**Protocol:** A set of procedures for calculating savings.

**Relative Root-Mean-Square Error:** In this study, another term for Theil's U.

**Scalar adjustment:** An adjustment method by which the provisional baseline load in each interval is multiplied by a constant or scalar.

**Simple adjustment:** An additive or scalar adjustment, where the additive or scalar is calculated as the difference or ratio of the average provisional baseline to the average actual load for some period prior to the control period. After simple adjustment, the average adjusted baseline matches the average actual load over the hours used to calculate the adjustment amount.

**Summer:** The months June through September.

**Temperature-Humidity Index:** An index based on daily temperature and humidity, as an indicator of the intensity of cooling requirements on a given day.

**Theil's U:** A measure of the typical magnitude of error, relative to the typical actual value, calculated as the ratio of the root-mean-square error to the root-mean-square actual.

**THI:** Temperature-Humidity Index.

**Uncurtailed account:** In this study, an account that had no curtailment periods during the time span of the data available for the study.

**Weather model:** A baseline estimation method using a regression model with weather terms as predictors.

**Weather-based adjustment:** An additive or scalar adjustment, where the additive or scalar is calculated as the difference or ratio of load estimated using control-period weather conditions to load estimated using weather conditions for period used to calculate the provisional baseline. Both load estimates use the same weather-based load model, fitted to data for a time period prior to either period used to produce the load estimates.

**Weather-sensitive:** A characteristic of an account, indicating that the load tends to increase or decrease according to weather conditions such as temperature and humidity.