SCE Comments

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Southern California Edison (SCE) files these comments in response to the April 26, 2016 CAISO Stakeholder Call and the associated presentation materials the CAISO has shared. SCE supports the CAISO's efforts to work collaboratively with stakeholders to clarify the "pre-dispatch" requirements for resources that cannot be dispatched post-contingency to meet reliability planning requirements. SCE's comments focus on two areas: 1) general comments on the presentation and the CAISO efforts; and 2) clarifications on the "Method 1" approach that will be performed by the Participating Transmission Owners (PTOs).

General Comments

SCE suggests a few clarifications for the study plan and materials. The CAISO should clarify that this study focuses on DR resources that are not capable of being dispatched post-contingency due to their notification (response) time, while recognizing that there are DR resources that are capable of such dispatch (i.e. not all DR is "slow-response" DR). Furthermore, while this stakeholder process has been kicked off within the Transmission Planning Process (TPP), the CAISO should work closely with the California Public Utilities Commission (CPUC) to coordinate with the Resource Adequacy (RA) proceeding, and ensure that the Load Serving Entities (LSEs) have a consistent set of regulatory requirements for Resource Adequacy and Transmission Planning purposes.

Method 1 Clarifications

For the benefit of the stakeholders in this process, SCE hereby provides additional details on the proposed study steps under the "Method 1" approach. As discussed on the call, the PTOs would first perform the analysis, and share it with the CAISO and the stakeholders. The CAISO would then have the option to verify these results by performing the "Method 2" approach.

In the attached presentation, additional details and initial results from the three IOUs are provided. The proposed methodology starts with the one-in-ten load forecast target, and scales historical loads to the target level. Several levels of Demand Response (DR) are assumed, and the expected resulting dispatch frequency is recorded. The methodology looks at various possible levels (MW) of DR, and calculates the

associated requirements, where a higher volume of DR implies a more frequent use, and therefore a more stringent set of requirements.

The study will be performed for all the Local Capacity Areas and Sub-Areas, and it may indicate different regional requirements due to differing load shapes and DR penetration. This information can then be used to inform the Transmission Planning Process as well as the DR program design.

SCE appreciates the opportunity to provide comments, and looks forward to working collaboratively with the stakeholders in completing this study and clarifying the pre-dispatch requirements for "slow" DR resources.

Determination of "Pre-Dispatch" Requirements for DR to Meet Local Capacity Needs

Draft Methodology

April 2016

Agenda

- Review Proposed Methodology
 - Background
 - Proposed approach
- SCE Example (Rector Sub Area)
- PG&E Example (Sierra Sub Area)
- Next Steps

2016 CAISO LOCAL CAPACITY TECHNICAL ANALYSIS

- Published April 30, 2015
- Objectives Identify specific CAISO areas that have limited import capability & determine minimum generation (MW) necessary to mitigate local reliability problems

SCE	LOAD	EFFECTIVENESS	2016	PRETRIESEPY	
LOCAL AREAS	POCKET	FACTORS	LCR (MW)	CONTINUENCE	VIDEATION
LA Davia	Defined	Donuidad	8,887	Lugo - Victorville 500kV & Sylmar - Gould 230kV (Eat C)	not specified
LA Basin	Derneg	Provided	7,575	Redondo Unit #7 & Sylmar - Gould 250kV (Eat B)	thermal overload
El Nédo			508	La Fresa - Hirson 230kV & La Fresa - Redondo #1 & #2 230kV	voltage collapse
Western LA Sasin			4,472	Serrano - Villa Park #2.230kV & Serrano - Lewis 230kV	thermal overload
West of Devers			488	San Bernardino - Etiwanda 230kV & San Bernardino - Vista 230kV	voltage collapse
Valley-Devers			1,722	Palo Verde - Colorado River 500kV & Valley SC - Serrano 500kV	thermal overload
Valley			n/a	Meeting Valley-Devers LCR sufficient to meet this area.	
Eastern LA Basin		Provided	n/a	Meeting West of Devers and Valley-Devers LCR sufficient to meet this area.	
No Conclusion to a	Configured.	Descrided	2,395	Lugo - Victorville 500kV & Sylmar - Pardee #1 or #2 250kV (Eat C)	thermal overload
sig creek/ventura	Derned	Provided	2,141	Ormond Beach Unit #2 & Sylmar - Pardee #1 or #2 230kV (Cat 8)	thermal overload
Rector		Provided	492	Eastwood & Rector - Vestal 230kV	thermal overload
Vestal		Provided	739	Eastwood & Magurden - Vestal 250kV	thermal overload
S. Clara			247	Pardee - S. Clara 230kV & Moorpark - S. Clara #1.8.2 230kV	voltage collapse
Moorpark			462	Pardee - Moorpark #1 230kV & Pardee - Moorpark #2 & #5 230kV	voltage collapse

Base Assumptions

- Probability of peak load forecast, contingency type (e.g. N-1, N-1-1, N-1-2) and system performance violation fully incorporated into CAISO's analysis
- Local RA showing assumes peak load and contingency will occur and sufficient LCR resources must be available during peak load
- Assume sufficient resources to meet LCR and that DR is last to be used with pre-dispatch DR first type to be utilized
- Scale recorded hourly load shapes of load pocket to forecasted peak load

Forecasted peak load in Load pocket DR

Served by local resources after critical contingency

Served by remote resources via transmission system after critical contingency



EXAMPLE

CAISO 2016 LOCAL CAPACITY TECHNICAL ANALYSIS (April 30, 2015)

Aedror Sub-orea The most critical contingency for the Rector sub-area is the loss of one of the Rector-Vestal 280 MV lines with the Eastwood unit out of service, which would thermally overload the remaining Rector-Vestal 280 MV line. This limiting contingency establishes a CR of 492 MW (includes SMW of DF generation) in 200 Bas the minimum capacity necessary for millable load serving capability within this sub-area

Gen Bus	Gen Name	Gen ID	MW Eff Fetr (h)	No. Construction
24370	KAWAGEN	1	51	Generation
24306	8 CRK1-1	1	45	9.0
24306	B CRK1-1	2	45	- 0-20
24307	B CRK1-2	a	45	Andrew Mark
24307	B CRK1-2	4	45	X
24319	EASTWOOD .	1	45	(Ch.
24323	PORTAL	1	45	
24308	8 CRK2-1	1	45	
24308	B CRK2-1	2	45	1 2
24309	B CRK2-2	a	45	
24309	B CRK2-2	4	45	H
24310	B CRK2-3	5	45	There
24310	B CRK2-3	6	45	
24315	B CRK B	81	45	New Street Stree
24315	B CRK B	- 58	45	D Oberland
24311	B CRKB-1	1	45	
24311	B CR83-1	2	45	7
24312	B CR83-2	a	45	Quere.
24312	B CR83-2	4	45	N. W.
24313	B CRK3-3	5	45	A.S.
24317	MAMOTH16	1	45	
24318	MAMOTH26	2	45	- 10 M / 10 M
24314	B CRK 4	41	43	Community .
24914	S CRK 4	42	43	
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Analysis Steps

- LCR of 492 MW required based on forecasted peak load to guard against a thermal overload triggered by critical contingency.
- 2. Since SCE builds CAISO's LCR cases, 2016 peak load modeled at Rector is known.
- Get recorded hourly flows for 2011 2015 (most recent five years) through Rector A-Banks and subtract KAWGEN production (local gen).
- 4. Scale recorded load curve up to modeled load to examine peak periods.
- 5. Examine DR at 10, 20, 50 & 100 MW levels.

												5.		-							
2016 Forec	asted Peak	847																			
Recorded I	Peak	678				737				719				719				712			
Scaling Fac	tor	1.25				1.15				1.18				1.18				1.19			
			20	11			20	12			20	13			20	14			20	15	
DR Ar	nount		20	11 Hour	5		20	12 Hour	5		20	13 Hour	5		20	14 Hour	5		20	15 Hour	5
DR Ar MW /%	nount of Peak	Days	20 Max	11 Hours Avg	s Total	Days	20 Max	12 Hour Avg	rs Total	Days	20 Max	13 Hour Avg	s Total	Days	20 Max	14 Hour Avg	s Total	Days	20 Max	15 Hour Avg	rs To
DR Ar MW /% 10	nount of Peak 1.2%	Days 1	20 Max 1	11 Hours Avg 1	s Total 1	Days	20 Max 2	12 Hour Avg 2	rs Total 2	Days	20 Max 1	13 Hour Avg 1	s Total 1	Days	20 Max 1	14 Hour Avg 1	s Total 1	Days	20 Max 1	15 Hour Avg 1	rs Tot
DR Ar MW / % 10 20	nount of Peak 1.2% 2.4%	Days 1	20 Max 1 1	11 Hours Avg 1 1	s Total 1	Days	20 Max 2 2	12 Hour Avg 2 2	rs Total 2 5	Days	20 Max 1 3	13 Hour Avg 1 2	s Total 1 6	Days 1 2	20 Max 1 3	14 Hour Avg 1 3	s Total 1 5	Days	20 Max 1 2	15 Hour Avg 1 2	rs Tot 1
DR Ar MW /% 10 20 50	nount of Peak 1.2% 2.4% 5.9%	Days 1 1 3	20 Max 1 1 5	11 Hours Avg 1 1 3	s Total 1 9	Days	20 Max 2 6	12 Hour Avg 2 2 5	s Total 2 5 27	Days 1 3 12	20 Max 1 3 7	13 Hour Avg 1 2 3	s Total 1 6 36	Days 1 2 13	20 Max 1 3 6	14 Hour Avg 1 3 3	s Total 1 5 44	Days	20 Max 1 2 6	15 Hour Avg 1 2 4	To To 1

PG&E Example - Analysis Steps

- Get recorded hourly load for 2014 2015 in Sierra area.
- 2. Scale recorded load curve up to modeled load to examine peak periods.
- Examine DR at 23 (existing), 47, 94 & 188 MW levels.

2016 1-in-10 Peak Foreca	st (MW) 1171.48								
Recorded Year Recorded Peak (MW) Scaling Factor	2014 1151 34 1.02		2015 1183.43 0.99						
Resource Deficiency (Ne	eded DR Amount)		201	15			20	14	
Resource Deficiency (Ne	eded DR Amount)	Deys	201	15 Hours		Days	20	Hours	
Resource Deficiency (Ne MW/% of P	eded DR Amount) ?eak	Days	201 Max	5 Hours Avg.	Total	Days	20 Max	Hours Avg.	1
Resource Deficiency (Ne MW/% of F 22.98	eded DR Amount) Peak	Deys 1	201 Max 3	Hours Avg. 3	Total 3	Days	20 Max 2	Hours Avg. 2	,
Resource Deficiency (Ne NW/% of P 22.98 47	eded DR Amount) Peak 2.0% 4.0%	Deys 1 1	201 Max 3 3	Hours Avg. 3 3	Total 3 3	Days 1 3	20 Max 2 3	Hours Avg. 2 2	
Resource Deficiency (Ne NWV/% of F 22.98 47 94	eded DR Amount) Peak 2.0% 4.0% 8.0%	Deys 1 1 4	201 Max 3 3 5	5 Hours Avg. 3 3 3	Total 3 3 12	Days 1 3 4	20 Max 2 3 5	Hours Avg. 2 2 4	

Discussion / Next Steps

- Methodology is LCR area specific: wide area requirements (e.g. LA Basin and Big Creek / Ventura) may be different from sub-areas
 - SCE & PG&E will need to expand the study to other sub-areas
 - Results may or may not be similar across areas
- DR Requirements dependent on DR quantity
 - Counting rules / requirements change as level of DR increases in a given area